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(71) Applicant: UBE INDUSTRIES, LTD.  
Ube-shi, Yamaguchi-ken 755 (JP)

(72) Inventors:

- Adachi, Mitsuru,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)
- Sasaki, Hiroto,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)
- Harada, Yasunori,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)
- Sakamoto, Tatsuo,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)
- Sato, Satoru,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)
- Yoshida, Atsushi,  
c/o Ube Industries, Ltd.  
Oaza Kogushi, Ube-shi, Yamaguchi (JP)

(74) Representative: Strehl Schübel-Hopf Groening &  
Partner  
Maximilianstrasse 54  
80538 München (DE)

### (54) Method and apparatus for shaping semisolid metals

(57) The improved method and apparatus for the semisolid forming of alloys to enable shaped parts having a fine-grained, spherical thixotropic structures to be produced in a convenient, easy and inexpensive manner without relying upon the conventional mechanical or electromagnetic agitation. In the method, a liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is fed into an insulated vessel having a heat insulating effect, held in said insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, thereby crystallizing fine primary crystals in the alloy solution, and the alloy is fed into a forming mold, where it is shaped under pressure.

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## Description

### Background of the Invention

5 This invention relates to a method of shaping semisolid metals. More particularly, the invention relates to a method of shaping semisolid metals, in which liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is fed into an insulated vessel having heat insulating effect, holding the alloy for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, thereby generating  
10 fine primary crystals in the alloy solution and the alloy is shaped under pressure. The invention also relates to an apparatus for implementing this method.

Various methods for shaping semisolid metals are known in the art. A thixo-casting process is drawing researcher's attention these days since it involves a fewer molding defects and segregations, produces uniform metallographic structures and features longer mold lives but shorter molding cycles than the existing casting techniques. The billets used in  
15 this molding method (A) are characterized by spheroidized structures obtained by either performing mechanical or electromagnetic agitation in temperature ranges that produce semisolid metals or by taking advantage of recrystallization of worked metals. On the other hand, raw materials cast by the existing methods may be molded in a semisolid state. There are three examples of this approach; the first two concern magnesium alloys that will easily produce an equiaxed microstructure and Zr is added to induce the formation of finer crystals [method (B)] or a carbonaceous refiner is added  
20 for the same purpose [method (C)]; the third approach concerns aluminum alloy and a master alloy comprising an Al-5% Ti-1% B system is added as a refiner in amounts ranging from 2 - 10 times the conventional amount [method (D)]. The raw materials prepared by these methods are heated to temperature ranges that produce semisolid metals and the resulting primary crystals are spheroidized before molding. It is also known that alloys within a solubility limit are heated fairly rapidly up to a temperature near the solidus line and, thereafter, in order to ensure a uniform temperature profile  
25 through the raw material while avoiding local melting, the alloy is slowly heated to an appropriate temperature beyond the solidus line so that the material becomes sufficiently soft to be molded [method (E)].

These methods in which billets are molded after they are heated to temperatures that produce semisolid metals are in sharp contrast with a rheo-casting process (F), in which molten metals containing spherical primary crystals are produced continuously and molded as such without being solidified to billets.

30 However, the above-described conventional methods have their own problems. method (A) is cumbersome and the production cost is high irrespective of whether the agitation or recrystallization technique is utilized. When applied to magnesium alloys, method (B) is economically disadvantageous since Zr is an expensive element and speaking of method (C), in order to ensure that carbonaceous refiners will exhibit their function to the fullest extent, the addition of Be as an oxidation control element has to be reduced to a level as low as about 7 ppm but then the alloy is prone to  
35 burn by oxidation during the heat treatment just prior to molding and this is inconvenient in operations.

In the case of aluminum alloys, about 500  $\mu\text{m}$  is the size that can be achieved by the mere addition of refiners and it is not easy to obtain crystal grains finer than 100  $\mu\text{m}$ . To solve this problem, increased amounts of refiners are added in method (D) but this is industrially difficult to implement because the added refiners are prone to settle on the bottom of the furnace; furthermore, the method is costly. Method (E) is a thixo-casting process which is characterized by heating the raw material slowly after the temperature has exceeded the solidus line such that the raw material is uniformly  
40 heated and spheroidized. In fact, however, an ordinary dendritic microstructure will not transform to a thixotropic structure (in which the primary dendrites have been spheroidized). What is more, thixo-casting methods (A) - (E) have a common problem in that they are more costly than the existing casting methods because in order to perform molding in the semisolid state, the liquid phase must first be solidified to prepare a billet, which is heated again to a temperature range that produces a semisolid metal. In contrast, method (F) which continuously generates and supplies a molten metal containing spherical primary crystals is more advantageous than the thixocasting approach from the viewpoint of cost and energy but, on the other hand, the machine to be installed for producing a metal material consisting of a spherical structure and a liquid phase requires cumbersome procedures to assure effective operative association with the casting machine to yield the final product.

50 The present invention has been accomplished under these circumstances and has as an object providing a method that does not use billets or any cumbersome procedures but which ensures convenience and ease in the production of semisolid metals having fine primary crystals and shaping them under pressure.

Another object of the invention is to provide an apparatus that can implement this method.

### 55 Summary of the Invention

The first object of the invention can be attained by the method of shaping a semisolid metal recited in claim 1, in which a liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is fed into an insulated

vessel having a heat insulating effect, held in said insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, thereby crystallizing primary crystals in the alloy solution, and the alloy is fed into a forming mold, where it is shaped under pressure.

According to claim 2, the crystal nuclei mentioned in claim 1 are generated by contacting the molten alloy with a surface of a jig at a temperature lower than the melting point of said alloy which has been held superheated to less than 300°C above the liquidus temperature.

According to claim 3, the jig mentioned in claim 2 is a metallic or nonmetallic jig, or a metallic jig having a surface coated with nonmetallic materials or semiconductors, or a metallic jig compounded of nonmetallic materials or semiconductor, with said jig being adapted to be coolable from either inside or outside.

According to claim 4, the crystal nuclei mentioned in claim 1 or 2 are generated by applying vibrations to the molten metal in contact with either the jig or the insulated vessel or both.

According to claim 5, the alloy mentioned in claim 1 or 2 is an aluminum alloy of a composition within a maximum solubility limit or a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit.

According to claim 6, the alloy mentioned in claim 1 or 2 is a magnesium alloy of a composition within a maximum solubility limit.

According to claim 7, the aluminum alloy mentioned in claim 5 has 0.001% - 0.01% B and 0.005% - 0.3% Ti added thereto.

According to claim 8, the magnesium alloy mentioned in claim 6 is one having 0.005% - 0.1% Sr added thereto, or one having 0.01% - 1.5% Si and 0.005% - 0.1% Sr added thereto, or one having 0.05% - 0.30% Ca added thereto.

According to claim 9, a molten aluminum alloy held superheated to less than 100°C above the liquidus temperature is directly poured into an insulated vessel without using a jig.

According to claim 10, a molten magnesium alloy held superheated to less than 100°C above the liquidus temperature is directly poured into an insulated vessel without using a jig.

According to claim 11, liquid alloy having crystal nuclei that has been superheated by a degree ( $X^{\circ}\text{C}$ ) of less than 10°C above the liquidus line is held in an insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to a molding temperature where a specified fraction liquid is established, such that the cooling from the initial temperature at which said alloy is held in said insulated vessel to its liquidus temperature is completed within a time shorter than the time Y (in minutes) calculated by the relation  $Y=10-X$  and that the period of cooling from said initial temperature to a temperature 5°C lower than said liquidus temperature is not longer than 15 minutes, whereby fine primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.

According to claim 12, a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is held within an insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, such that the period of cooling from the initial temperature at which said alloy is held in said insulated vessel to a temperature 5°C lower than its liquidus temperature is not longer than 15 minutes, whereby fine primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.

According to claim 13, the crystal nuclei mentioned in claim 11 or 12 are generated by holding a molten alloy superheated to less than 300°C above the liquidus temperature and contacting the melt with a surface of a jig at a lower temperature than its melting point.

The second object of the invention can be attained by the apparatus recited in claim 14 which is for producing a semisolid forming metal having fine primary crystals dispersed in a liquid phase, said apparatus comprising a nucleus generating section that causes a molten metal to contact a cooling jig to generate crystal nuclei in the solution and a crystal generating section having an insulated vessel in which the metal obtained in said nucleus generating section is held as it is cooled to a molding temperature at which said metal is partially solid, partially liquid.

According to claim 15, the cooling jig in the nucleus generating section mentioned in claim 14 is either an inclined flat plate that has an internal channel for a cooling medium and that has a pair of weirs provided on the top surface parallel to the flow of the melt, or a cylindrical or semicylindrical tube.

According to claim 16, liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid having crystal nuclei at a temperature not lower than a molding temperature is poured into a vessel so that it is cooled to a temperature at which a fraction solid appropriate for shaping is established, said vessel being adapted to be heatable or coolable from either inside or outside, being made of a material having a thermal conductivity of at least 1.0 kcal/hr · m · °C (at room temperature) and being held at a temperature not higher than the liquidus temperature of said alloy prior to its pouring, and said alloy is poured into said vessel in such a manner that fine, nondendritic primary crystals are crystallized in said alloy solution and that said alloy is cooled rapidly enough to be provided with a uniform temperature profile in said vessel, and said alloy, after being cooled, is fed into a forming mold, where it is shaped under pressure.

According to claim 17, the step of cooling the alloy mentioned in claim 16 is performed with the top and bottom portions of the vessel being heated by a greater degree than the middle portion or heat-retained with a heat-retaining mate-

rial having a thermal conductivity of less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  or with either the top or bottom portion of the vessel being heated while the remainder is heat-retained.

According to claim 18, the step of cooling the alloy mentioned in claim 16 is performed with the vessel holding said alloy being accommodated in an outer vessel that is capable of accommodating said alloy holding vessel and that has a smaller thermal conductivity than said holding vessel, or that has a thermal conductivity equal to or greater than that of said holding vessel and which has a higher initial temperature than said holding vessel, or that is spaced from said holding vessel by a gas-filled gap, at a sufficiently rapid cooling rate to provide a uniform temperature profile through the alloy in said holding vessel no later than the start of the shaping step.

According to claim 19, there is provided a method of managing the temperature of a semisolid metal slurry for use in molding equipment in which a molten metal containing a large number of crystal nuclei is poured into a vessel, where it is cooled to produce a semisolid metal slurry containing both a solid and a liquid phase in specified amounts, said slurry being subsequently fed into a molding machine for shaping under pressure, which method is characterized in that the vessel for holding said molten metal is temperature-managed such as to establish a preset desired temperature prior to the pouring of said molten metal and such that said molten metal is cooled at an intended rate after said molten metal is poured into said vessel.

According to claim 20, there is provided an apparatus for managing the temperature of a semisolid metal slurry to be used in molding equipment in which a molten metal containing a large number of crystal nuclei is poured from a melt holding furnace into a vessel, where it is cooled to produce a semisolid metal slurry containing both a solid and a liquid phase in specified amounts and in which said slurry is directly fed into a molding machine for shaping under pressure, which apparatus is further characterized by comprising the vessel for holding said molten metal, a vessel temperature control section for managing the temperature of said vessel, a semisolid metal cooling section for managing the temperature of the as-poured molten metal such that it is cooled at an intended rate, and a vessel transport mechanism comprising basically a robot for gripping, moving and transporting said vessel and a conveyor for carrying, moving and transporting said vessel.

According to claim 21, the vessel temperature control section mentioned in claim 20 comprises a vessel cooling furnace for cooling the vessel in an ambient temperature not higher than a target temperature for the vessel and a vessel heat-retaining furnace for holding the vessel at an ambient temperature equal to said target temperature.

According to claim 22, the semisolid metal cooling section mentioned in claim 20 comprises a semisolid metal cooling furnace and a semisolid metal annealing furnace for managing the temperature in itself to be higher than the temperature in said semisolid metal cooling furnace.

According to claim 23, the semisolid metal cooling furnace in the semisolid metal cooling section mentioned in claim 22 is such that the area around the vessel carried on the conveyor device moving to pass through said furnace is partitioned into three regions, the upper, middle and lower parts, by means of two pairs of heat insulating plate, one pair consisting of an upper right and an upper left plate and the other pair consisting of a lower right and a lower left plate, with a heater being installed in both said upper and lower parts for heating said two parts at a higher temperature than hot air to be supplied to said central part.

According to claim 24, a preheating furnace is installed at a stage prior to the semisolid metal cooling furnace in claim 22 to ensure that both a plinth having a lower thermal conductivity than the vessel and which carries said vessel before it is directed to said semisolid metal cooling furnace and a lid having a lower thermal conductivity than said vessel and which is to be placed to cover it after it accommodates said molten metal are preheated by being moved to pass through said preheating furnace in advance.

According to claim 25, the semisolid metal cooling furnace is equipped with a control unit with which the temperature or the velocity of hot air to be supplied into said semisolid metal cooling furnace is controlled to vary with the lapse of time.

According to claim 26, the semisolid metal cooling furnace mentioned in claim 22 comprises an array of housings each accommodating the vessel as it contains the molten metal and being equipped with an openable cover and hot air feed/exhaust pipes, as well as a mechanism by which a receptacle for carrying said vessel is rotated about a vertical shaft.

According to claim 27, a vibrator for vibrating the receptacle mentioned in claim 26 is provided for each housing.

According to claim 28, the semisolid metal cooling furnace for treating the molten metal as poured into a vessel having a thermal conductivity of at least  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  is supplied with hot air having a temperature in the range from  $150^\circ\text{C}$  to  $350^\circ\text{C}$  for aluminum alloys and from  $200^\circ\text{C}$  to  $450^\circ\text{C}$  for magnesium alloys.

According to claim 29, the semisolid metal cooling furnace for treating the molten metal as poured into a vessel having a thermal conductivity of less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  is supplied with hot air having a temperature in range from  $50^\circ\text{C}$  to  $200^\circ\text{C}$  for aluminum alloys and from  $100^\circ\text{C}$  to  $250^\circ\text{C}$  for magnesium alloys.

According to claim 30, the molten metal as poured into the insulated vessel in claim 1 or 2 is isolated from the ambient atmosphere by closing the top surface of said vessel with an insulating lid having a heat insulating effect as long as said molten metal is held within said vessel until the molding temperature is reached.

According to claim 31, the alloy in claim 1 or 2 is specified to a zinc alloy.

According to claim 32, the alloy in claim 1 or 2 is specified to a hypereutectic Al-Si alloy having 0.005% - 0.03% P added thereto or a hypereutectic Al-Si alloy containing 0.005% - 0.03% P having either 0.005% - 0.03% Sr or 0.001% - 0.01% Na or both added thereto.

According to claim 33, the alloy in claim 1 or 2 is specified to a hypoeutectic Al-Mg alloy containing Mg in an amount not exceeding a maximum solubility limit and which has 0.3% - 2.5% Si added thereto.

According to claim 34, the pressure forming in claim 1 or 2 is accomplished with the alloy being inserted into a container on an extruding machine.

According to claim 35, the extruding machine is of either a horizontal or a vertical type or of such a horizontal type in which the container changes position from being vertical to horizontal and the method of extrusion is either direct or indirect.

According to claim 36, the crystal nuclei in claim 1 are generated by a method in which two or more liquid alloys having different melting points that are held superheated to less than 50°C above the liquidus temperature are mixed either directly within the insulated vessel having a heat insulating effect or along a trough in a path into the insulated vessel, such that the temperature of the metal as mixed is either just above or below the liquidus temperature.

According to claim 37, the two or more metals to be mixed in claim 36 are preliminarily contacted with respective jigs each having a cooling zone such as to produce metals of different melting points that have crystal nuclei and which have attained temperatures just either above or below the liquidus temperature.

According to claim 38, the top surface of the semisolid metal that is held within the insulated vessel and which is to be fed into the forming mold in claim 1 is removed by means of either a metallic or nonmetallic jig during a period from just after the pouring into said vessel but before the molding temperature is reached and, thereafter, said semisolid metal is inserted into an injection sleeve.

According to claim 39, the outer vessel in claim 18 is heated either from inside or outside or by induction heating, with such heating being performed only or before or after the insertion of the holding vessel into the outer vessel or continued throughout the period not only before but also after the insertion.

According to claim 40, the aluminum alloy in claim 9 is replaced by a zinc alloy.

With these methods and apparatus of the invention, either liquid or partially solid, partially liquid alloys having crystal nuclei (as exemplified by molten Al and Mg alloys) are charged into an insulated vessel having a heat insulating effect and held there for a period from 5 seconds to 60 minutes as they are cooled to a molding temperature, whereby fine and spherical primary crystals are generated in the solution and the resulting semisolid alloy is fed into a mold, where it is pressure formed to produce a shaped part having a homogeneous microstructure.

#### Brief Description of the Drawings

Fig. 1 is a diagram showing a process sequence for the semisolid forming of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit;

Fig. 2 is a diagram showing a process sequence for the semisolid forming of a magnesium or aluminum alloy having a composition within a maximum solubility limit;

Fig. 3 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step;

Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 3;

Fig. 5 is an equilibrium phase diagram for an Al-Si alloy as a typical aluminum alloy system;

Fig. 6 is an equilibrium phase diagram for a Mg-Al alloy as a typical magnesium alloy system;

Fig. 7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention;

Fig. 8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art;

Fig. 9 is a diagram showing a process sequence for the semisolid forming of hypoeutectic aluminum alloys having a composition at or above a maximum solubility limit according to examples of the invention (as recited in claims 11 - 13 and 18);

Fig. 10 is a diagram showing a process sequence for the semisolid forming of magnesium or aluminum alloys having a composition within a maximum solubility limit according to examples of the invention (as recited in claims 11 - 13 and 18);

Fig. 11 is an equilibrium phase diagram for Al-Si alloys as a typical aluminum alloy system according to the invention (as recited in claims 11 - 13 and 18);

Fig. 12 is an equilibrium phase diagram for Mg-Al alloys as a typical magnesium alloy system according to the invention (as recited in claims 11 - 13 and 18);

Fig. 13 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention (as recited in claims 11 - 13);

Fig. 14 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claims 11 - 13);

Fig. 15 is a graph showing how the holding time affects the crystal grain size of a prior art alloy (AZ91);

Fig. 16 is a graph showing how the holding time affects the crystal grain size of a prior art alloy (AC4CH);

Fig. 17 is a graph showing how the degree of superheating of the prior art alloy AZ91 (above the liquidus line) and the holding time (from the initial temperature within an insulated vessel to the liquidus temperature) affect the crystal grain size of the alloy;

Fig. 18 is a graph showing how the degree of superheating of the prior art alloy AC4H (above the liquidus line) and the holding time (from the initial temperature within the insulated vessel to the liquidus temperature) affect the crystal grain size of the alloy;

Fig. 19 is a graph showing how the holding time (from the initial temperature within the insulated vessel to the liquidus temperature minus 5°C) affects the crystal grain size of the prior art alloy AZ91;

Fig. 20 is a graph showing how the holding time (from the initial temperature within the insulated vessel to the liquidus temperature minus 5°C) affects the crystal grain size of the prior art alloy AC4CH;

Fig. 21 is a side view of an apparatus for producing a semisolid forming metal according to an example of the invention (as recited in claims 14 and 15);

Fig. 22 is a perspective view of a cooling jig as part of the nucleus generating section of the apparatus shown in Fig. 21;

Fig. 23 shows in cross section two types of a cooling jig as part of the nucleus generating section of an apparatus for producing a semisolid forming metal according to another example of the invention (as recited in claims 14 and 15);

Fig. 24 is a sectional side view of a cooling jig as part of the nucleus generating section of an apparatus for producing a semisolid forming metal according to yet another example of the invention (as recited in claims 14 and 15);

Fig. 25 is a plan view showing the general layout of an apparatus for producing a semisolid forming metal according to another example of the invention (as recited in claims 14 and 15);

Fig. 26 is a longitudinal section A-A of Fig. 25;

Fig. 27 is a longitudinal section B-B of Fig. 25;

Fig. 28 is a longitudinal section of an insulated vessel in the examples of the invention (as recited in claims 14 and 15);

Fig. 29 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step (as recited in claims 16 and 17);

Fig. 30 compares two graphs plotting the temperature changes in the metal being cooled within a vessel during step 3 shown in Fig. 29;

Fig. 31 illustrates four methods of managing the temperature within a vessel according to the invention (as recited in claims 16 and 17);

Fig. 32 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step according to the invention (as recited in claim 18);

Fig. 33 compares the temperature profiles through two semisolid metals, one being held within a vessel according to an example of the invention (as recited in claim 18) and the other treated by the prior art;

Fig. 34 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claim 18);

Fig. 35 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to an example of the invention (as recited in claim 18);

Fig. 36 is a plan view showing the general layout of molding equipment (its first embodiment) according to an example of the invention recited in claims 19 - 23;

Fig. 37 is a plan view of a temperature management unit (its first embodiment) according to an example of the invention recited in claims 19 - 23;

Fig. 38 is a graph showing the specific positions of temperature measurement within a vessel according to an example of the invention (as recited in claims 19 - 23);

Fig. 39 is a graph showing the temperature history of cooling within the vessel according to an example of the invention (as recited in claims 19 - 23);

Fig. 40 is a graph showing the temperature history of cooling within the vessel according to another example of the invention (as recited in claims 19 - 23);

Fig. 41 is a graph showing the temperature history of cooling within the vessel according to another example of the invention (as recited in claims 19 - 23);

Fig. 42 is a longitudinal section of a semisolid metal cooling furnace according to another example of the invention (as recited in claims 19 - 23);

Fig. 43 is a plan view of a temperature management unit (its second embodiment) according to other examples of the invention (as recited in claims 19 - 29);

Fig. 44 is a longitudinal section A-A of Fig. 43;

Fig. 45 shows the temperature profiles in the vessel fitted with heat insulators according to an example of the invention (as recited in claims 19 - 29) as compared with the temperature profile in the absence of such heat insulators;

Fig. 46 is a plan view of a temperature management unit (its third embodiment) according to another example of the invention (as recited in claims 19 - 29);

Fig. 47 shows schematically the composition of a temperature controller (its first embodiment) for a semisolid metal cooling furnace according to an example of the invention (as recited in claims 19 - 29);

Fig. 48 shows schematically the composition of a temperature controller (its second embodiment) for a semisolid metal cooling furnace according to another example of the invention (as recited in claims 19 - 29);

Fig. 49 is a longitudinal section of a vessel rotating unit according to an example of the invention (as recited in claims 19 - 29);

Fig. 50 is a plan view showing the general layout of molding equipment according to an example of the invention (as recited in claims 24 - 29);

Fig. 51 is a longitudinal sectional view showing in detail the position of temperature measurement within the holding vessel in the example shown in Fig. 50;

Fig. 52 is a graph showing the temperature history of cooling within the holding vessel in the example shown in Fig. 50;

Fig. 53 is a longitudinal section of a semisolid metal cooling furnace (equipped with a vessel vibrator) according to the third embodiment of the invention recited in claims 24 - 29;

Fig. 54 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step according to the invention (as recited in claim 30);

Fig. 55 is a diagram showing a process sequence for the semisolid forming of a zinc alloy of a hypoeutectic composition according to the invention (as recited in claim 31);

Fig. 56 is an equilibrium phase diagram for a binary Zn-Al alloy as a typical zinc alloy system according to the invention (as recited in claim 31);

Fig. 57 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention (as recited in claim 31);

Fig. 58 is a diagrammatic representation of micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claim 31);

Fig. 59 is a diagram showing a process sequence for the semisolid forming of a hypereutectic Al-Si alloy according to an example of the invention (as recited in claim 32);

Fig. 60 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step according to the example shown in Fig. 59;

Fig. 61 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 60;

Fig. 62 is an equilibrium phase diagram for a binary Al-Si alloy according to another example of the invention (as recited in claim 32);

Fig. 63 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention recited in claim 32;

Fig. 64 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claim 31);

Fig. 65 is an equilibrium phase diagram for a binary Al-Mg alloy according to the invention (as recited in claim 33);

Fig. 66 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to an example of the invention (as recited in claim 33);

Fig. 67 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claim 33);

Fig. 68 shows process flow starting with the generation of spherical primary crystals and ending with the molding step according to an example of the invention (as recited in claims 34 and 35);

Fig. 69 shows two process sequences for the semisolid forming of a hypoeutectic aluminum alloy according to an example of the invention (as recited in claims 36 and 37);

Fig. 70 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step according to the example shown in Fig. 69;

Fig. 71 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 70;

Fig. 72 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the example shown in Fig. 69;

Fig. 73 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art (for comparison with the invention recited in claims 36 and 37); and

Fig. 74 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step according to an example of the invention (as recited in claim 38).

Detailed Description of the Invention

A liquid alloy having crystal nuclei at a temperature not lower than the liquidus line or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature, as exemplified by a molten aluminum or magnesium alloy, is fed into an insulated vessel having a heat insulating effect, and the alloys are held in that vessel for a period from 5 seconds to 60 minutes as they are cooled to the molding temperature, thereby generating fine and spheroidized primary crystals in the alloy solution and the resulting semisolid alloy is fed into a mold, where it is pressure formed into a shaped part having a homogeneous microstructure.

Example 1

An example of the invention (as recited in claims 1 - 10) will now be described in detail with reference to accompanying Figs. 1-8, in which: Fig. 1 is a diagram showing a process sequence for the semisolid forming of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit; Fig. 2 is a diagram showing a process sequence for the semisolid forming of a magnesium or aluminum alloy having a composition within a maximum solubility limit; Fig. 3 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 3; Fig. 5 is an equilibrium phase diagram for an Al-Si alloy as a typical aluminum alloy system; Fig. 6 is an equilibrium phase diagram for a Mg-Al alloy as a typical magnesium alloy system; Fig. 7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig. 8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs. 1, 2, 5 and 6 the first step of the process according to the invention comprises:

- (1) superheating the melt of a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit or a magnesium or aluminum alloy of a composition within a maximum solubility limit, holding the melt superheated to less than 300°C above the liquidus temperature and contacting the melt with a surface of a jig at a lower temperature than its melting point so as to generate crystal nuclei in the alloy solution; or alternatively,
- (2) superheating the melt of an aluminum or magnesium alloy containing an element for promoting the generation of crystal nuclei, holding the melt superheated to less than 100°C above the liquidus temperature.

The cooled molten alloy prepared in (1) is poured into an insulated vessel having a heat insulating effect and, in the case of (2), the melt is directly poured into the insulated vessel without being cooled with a jig. The melt is held within the insulated vessel for a period from 5 seconds to 60 minutes at a temperature not higher than the liquidus temperature but higher than the eutectic or solidus temperature, whereby a large number of fine spherical primary crystals are generated in the alloy, which is then shaped at a specified fraction liquid.

The term "a specified fraction liquid" means a relative proportion of the liquid phase which is suitable for pressure forming. In high-pressure casting operations such as die casting and squeeze casting, the fraction liquid ranges from 20% to 90%, preferably from 30% to 70%. If the fraction liquid is less than 30%, the formability of the raw material is poor; above 70%, the raw material is so soft that it is not only difficult to handle but also less likely to produce a homogeneous microstructure. In extruding and forging operations, the fraction liquid ranges from 0.1% to 70%, preferably from 0.1% to 50%, beyond which an inhomogeneous structure can potentially occur.

The "insulated vessel" as used in the invention is a metallic or nonmetallic vessel, or a metallic vessel having a surface coated with nonmetallic materials or semiconductors, or a metallic vessel compounded of nonmetallic materials or semiconductor, which vessels are adapted to be either heatable or coolable from either inside or outside.

According to the invention, semisolid metal forming will proceed by the following specific procedure. In step (1) of the process shown in Figs. 3 and 4, a complete liquid form of metal M is contained in a ladle 10. In step (2), the metal is treated by either one of the following methods to produce an alloy having a large number of crystal nuclei which is of a composition just below the liquidus line: (a) the low-temperature melt (which may optionally contain an element that is added to promote the generation of crystal nuclei) is cooled with a jig 20 to generate crystal nuclei and the melt is then poured into a ceramic vessel 30 having a heat insulating effect; or (b) the low-temperature melt of a composition just above the melting point which contains an element to promote the generation of a fine structure is directly poured into the insulated vessel (or a ceramics-coated metallic vessel 30A) having a heat insulating effect. In subsequent step (3) the alloy is held partially molten within the insulated vessel 30 (or 30A). In the meantime, very fine, isotropic dendritic primary crystals result from the introduced crystal nuclei [step (3)-a] and grow into spherical primary crystals as the fraction solid increases with the decreasing temperature of the melt [steps (3)-b and (3)-c]. Metal M thus obtained at a specified fraction liquid is inserted into a die casting injection sleeve 40 [step (3)-d] and thereafter pressure formed within a mold cavity 50a on a die casting machine to produce a shaped part [step (4)].

The semisolid metal forming process of the invention shown in Figs. 1 - 4 has obvious differences from the conventional thixocasting and rheocasting methods. In the invention method, the dendritic primary crystals that have been



crystallized within a temperature range for the semisolid state are not ground into spherical grains by mechanical or electromagnetic agitation as in the prior art but the large number of primary crystals that have been crystallized and grown from the introduced crystal nuclei with the decreasing temperature in the range for the semisolid state are spheroidized continuously by the heat of the alloy itself (which may optionally be supplied with external heat and held at a desired temperature). In addition, the semisolid metal forming method of the invention is very convenient since it does not involve the step of partially melting billets by reheating in the thixocasting process.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in Fig. 3, namely, the step of pouring the molten metal on to the cooling jig 20, the step of generating and spheroidizing primary crystals and the forming step, are set forth below more specifically. Also discussed below is the criticality of the numerical limitations set forth in claims 2 and 7 - 10.

If the casting temperature is at least 300°C higher than the melting point or if the surface temperature of jig 20 is not lower than the melting point, the following phenomena will occur; (1) only a few crystal nuclei are generated; (2) the temperature of the melt M as poured into the insulated vessel having a heat insulating effect is higher than the liquidus temperature and, hence, the proportion of the remaining crystal nuclei is low enough to produce large primary crystals.

To avoid these problems, the casting temperature to be employed in the invention is controlled to be such that the degree of superheating above the liquidus line is less than 300°C whereas the surface temperature of jig 20 is controlled to be lower than the melting point of alloy M. Primary crystals of an even finer size can be produced by ensuring that the degree of superheating above the liquidus line is less than 100°C and by adjusting the surface temperature of jig 20 to be at least 50°C lower than the melting point of alloy M. The melt M can be contacted with jig 20 by one of two methods: the melt M is moved on the surface of jig 20 (the melt is caused to flow down the inclined jig), or the jig moves through the melt. The "jig" as used herein means any device that provides a cooling action on the melt as it flows down. The jig may be replaced by the tubular pipe on a molten metal supply unit. Insulated vessel 30 for holding the melt the temperature of which has dropped to just below the liquidus line shall have a heat insulating effect in order to ensure that the primary crystals generated will spheroidize and have the desired fraction liquid after the passage of a specified time. The constituent material of the insulated vessel is in no way limited and those which have a heat-retaining property and which wet with the melt only poorly are preferred. If a gas-permeable ceramic container is to be used as the insulated vessel 30 for holding magnesium alloys which are prone to oxidize and burn, the exterior to the vessel is preferably filled with a specified atmosphere (e.g. an inert or vacuum atmosphere). For preventing oxidation, it is desired that Be or Ca is preliminarily added to the molten metal. The shape of the insulated vessel 30 is by no means limited to a tubular form and any other shapes that are suitable for the subsequent forming process may be adopted. The molten metal need not be poured into the insulated vessel but it may optionally be charged directly into a ceramic injection sleeve. If the holding time within the insulated vessel 30 is less than 5 seconds, it is not easy to attain the temperature for the desired fraction liquid and it is also difficult to generate spherical primary crystals. If the holding time exceeds 60 minutes, the spherical primary crystals and eutectic structure generated are so coarse that deterioration in mechanical properties will occur. Hence, the holding time within the insulated vessel is controlled to lie between 5 seconds and 60 minutes. If the fraction liquid in the alloy which is about to be shaped by high-pressure casting processes is less than 20%, the resistance to deformation during the shaping is so high that it is not easy to produce shaped parts of good quality. If the fraction liquid exceeds 90%, shaped parts having a homogeneous structure cannot be obtained. Therefore, as already mentioned, the fraction liquid in the alloy to be shaped is preferably controlled to lie between 20% and 90%. By adjusting the effective fraction liquid to range from 30% to 70%, shaped parts having a more homogeneous structure and higher quality can be easily obtained by pressure forming. If, in the case of shaping Al-Si alloy systems having a near eutectic composition, it is necessary to generate eutectic Si within the insulated vessel while reducing the fraction liquid to 80% or below, Na or Sr may be added as an Si modifying element and this is advantageous for refining the eutectic Si grains, thereby providing improved ductility. The means of pressure forming are in no way limited to high-pressure casting processes typified by squeeze casting and die casting and various other methods of pressure forming may be adopted, such as extruding and casting operations.

The constituent material of the jig 20 with which the melt M is to be contacted is not limited to any particular types as long as it is capable of lowering the temperature of the melt. A jig 20 that is made of a highly heat-conductive metal such as copper, a copper alloy, aluminum or an aluminum alloy and which is controlled to provide a cooling effect for maintaining temperatures below a specified level is particularly preferred since it allows for the generation of many crystal nuclei. In this connection, it should be mentioned that coating the cooling surface of the jig 20 with a nonmetallic material is effective for the purpose of ensuring that solid lumps of metal will not adhere to the jig 20 when it is contacted by the melt M. The coating method may be either mechanical or chemical or physical.

A semisolid alloy containing a large number of crystal nuclei and which has a temperature not higher than the liquidus line can be obtained by contacting the melt M with the jig 20. If desired, (1) in order to generate more crystal nuclei so as to produce a homogeneous structure comprising fine spherical grains or (2) to ensure that a semisolid alloy containing a large number of crystal nuclei and which has a temperature not higher than the liquidus line is produced from a melt that has been superheated to less than 100°C above the liquidus line and which is not contacted with any jig, various elements may be added to the melt, as exemplified by Ti and B for the case where the melt is an aluminum alloy,

and Sr, Si and Ca for the case where the melt is a magnesium alloy. If the Ti addition is less than 0.005%, the intended refining effect is not attained; beyond 0.30%, a coarse Ti compound will form to cause deterioration in ductility. Hence, the Ti addition is controlled to lie between 0.005% and 0.30%. Boron (B) cooperates with Ti to promote the refining of crystal grains but its refining effect is small if the addition is less than 0.001%; on the other hand, the effect of B is saturated at 0.02% and no further improvement is expected beyond 0.02%. Hence, the B addition is controlled to lie between 0.001% and 0.02%. If the Sr addition is less than 0.005%, the intended refining effect is not attained; on the other hand, the effect of Sr is saturated at 0.1% and no further improvement is expected beyond 0.1%. Hence, the Sr addition is controlled to lie between 0.005% and 0.1%. If 0.01% - 1.5% of Si is added in combination with 0.005% - 0.1% of Sr, even finer crystal grains will be formed than when Sr is added alone. If the Ca addition is less than 0.05%, the intended refining effect is not attained; on the other hand, the effect of Ca is saturated at 0.30% and no further improvement is expected beyond 0.30%. Hence, the Ca addition is controlled to lie between 0.05% and 0.30%.

If the fine spherical primary crystals are to be obtained without employing jig 20, the degree of superheating above the liquidus line is set to be less than 100°C and this is to ensure that the molten alloy poured into the insulated vessel 30 having a heat insulating effect is brought to either a liquid state having crystal nuclei or a partially solid, partially liquid state having crystal nuclei at a temperature not lower than the molding temperature. If the melt poured into the insulated vessel 30 is unduly hot, so much time will be taken for the temperature of the melt to decrease to establish a specified fraction liquid that the operating efficiency becomes low. Another inconvenience is that the poured melt M is oxidized or burnt at the surface.

Table 1 shows the conditions of various samples of semisolid metal to be shaped, as well as the qualities of shaped parts. As shown in Fig. 3, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed, 1.5 m/s; mold cavity dimensions, 100 x 150 x 10; mold temperature, 230°C.

Table 1 (continued on next page)

		Conditions of the semisolid metal to be shaped						
	No.	Alloy	Casting temperature (°C)	Cooling jig	Temperature of the cooling (°C)	Temperature of the metal within vessel (°C)	Holding time (min)	Fraction of liquid just before shaping (%)
Comparative Sample	1	AC4CH	625	Used	622	618	5	60
	2	AC4CH	950	Used	30	730	20	60
	3	AC4CH	680	Used	30	622	65	15
	4	AC4CH-0.15%Ti-0.005%B	630	Used	30	613	0.04	95
	5	AC4CH	630	Used	30	610	2	60
	6	AC4CH-0.15%Ti-0.005%B	630	Used	30	611	1	92
	7	AC4CH	630	Not used	-	620	5	60
	8	AC4CH-0.15%Ti-0.005%B	630	Used	30	612	6.5	55
Invention Sample	9	AC4CH	630	Used	30	611	12	45
	10	AC4CH-0.15%Ti-0.005%B	630	Used	400	614	5.5	60
	11	AC4CH-0.15%Ti-0.010%B	850	Used	25	613	6	60
	12	AC4CH-0.15%Ti-0.015%B	630	Not Used	-	620	15	35
	13	AC7A	660	Used	30	632	5.7	50
	14	7075	650	Used	30	620	1.5	80
	15	AZ91	620	Used	30	590	4.2	55
	16	AZ91-0.4%Si-0.01%Sr	620	Used	30	590	4.3	55
	17	AZ91-0.15%Ca	620	Not used	30	590	4.5	55
	18	AC4CH-0.15%Ti-0.015%B	630	Not used	-	620	5	60

AC4CH: Al-7%Si-0.35%Mg m.p. 620°C

7075: Al-4.5%Zn-1.1%Mg m.p. 640°C

\*1 Dendritic primary crystals

\*2 Spherical primary crystals (with dendritic primary crystals)

External appearance: O, good; Δ, fair; X, poor

Internal segregations: O, a few; X, many

Amount of unspherical primary crystals: O, small; X, large

Eutectic size: O, fine; X, coarse

AZ91: Mg-9%Al-0.7%Zn m.p. 595°C

AC7A: Al-5%Mg-0.4%Mn m.p. 635°C

Table 1 (continued)

	No.	Alloy	Quality of shaped part				Remarks
			Inter- nal Segre- gation	Primary crystal size ( $\mu$ m)	Amount of un- spherical primary crystal	Eutec- tic size	Exter- nal appear- ance
Comparative Sample	1	AC4CH	x	280	x	o	High jig temperature
	2	AC4CH	x	450	x	o	High casting temperature
	3	AC4CH	o	180	o	x	Long holding time
	4	AC4CH-0.15%Ti-0.005%B	x	*1		o	Short holding time, high fraction liquid
	5	AC4CH	x	*2		o	Metallic container was us- ed at ordinary temperature.
Inven- tion Sample	6	AC4CH-0.15%Ti-0.005%B	x	*2		o	Short holding time, high fraction liquid
	7	AC4CH	x	290	x	o	No grain refiner was used.
	8	AC4CH-0.15%Ti-0.005%B	o	55	o	o	
	9	AC4CH	o	70	o	o	
	10	AC4CH-0.15%Ti-0.005%B	o	85	o	o	
	11	AC4CH-0.15%Ti-0.010%B	o	75	o	o	
	12	AC4CH-0.15%Ti-0.015%B	o	115	o	o	Water-cooled cooling jig was used.
	13	AC7A	o	80	o	o	No jig was used.
	14	7075	o	90	o	o	
	15	AZ91	o	85	o	o	
	16	AZ91-0.4%Si-0.01%Sr	o	75	o	o	
	17	AZ91-0.15%Ca	o	120	o	o	No jig was used. Vibrations(100Hz) were applied at amplitude of 0.1mm.
	18	AC4CH-0.15%Ti-0.015%B	o	95	o	o	

In Comparative Sample 1, the temperature of jig 20 with which the melt M was contacted was so high that the number of crystal nuclei generated was insufficient to produce fine spherical primary crystals; instead coarse unspherical primary crystals formed as shown in Fig. 7. In Comparative Sample 2, the casting temperature was so high that very few crystal nuclei remained within the ceramic vessel 30, yielding the same result as with Comparative Sample 1. In

Comparative Sample 3, the holding time was so long that the fraction liquid in the metal to be shaped was low, yielding a shaped part of poor appearance. In addition, the size of primary crystals was undesirably large. In Comparative Sample 4, the holding time within the ceramic vessel 30 was short whereas the fraction liquid in the metal to be shaped was high; hence, only dendritic primary crystals formed. In addition, the high fraction liquid caused many segregations of components within the shaped part. With Comparative Sample 5 the insulated vessel 30 was a metallic container having a small heat insulating effect, so the dendritic solidified layer forming on the inner surface of the vessel 30 would enter the spherical primary crystals generated in the central part of the vessel, thus yielding an inhomogeneous structure involving segregations. In Comparative Sample 6, the fraction liquid in the metal to be shaped was so high that the result was the same as with Comparative Sample 4. With Comparative Sample 7, the jig 20 was not used; the starting alloy did not contain any grain refiners, so the number of crystal nuclei generated was small enough to yield the same result as with Comparative Sample 1.

In each of Invention Samples 8 - 17, a homogeneous microstructure comprising fine ( $<150\mu\text{m}$ ) spherical primary crystals was obtained to enable the production of a shaped part having good appearance.

## Example 2

An example of the invention (as recited in claims 11 - 13) will now be described in detail with reference to accompanying drawings. As shown in Figs. 9 - 12, the invention recited in claims 11 - 13 is such that:

- (1) the melt of a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit or a magnesium or aluminum alloy of a composition within a maximum solubility limit which are held superheated less than  $300^{\circ}\text{C}$  above the liquidus temperature is contacted with a surface of a jig having a lower temperature than the melting point of the alloy so as to generate crystal nuclei in the alloy solution which is then poured into an insulated vessel; or
- (2) the melt of an aluminum or magnesium alloy that is held superheated to less than  $100^{\circ}\text{C}$  above the liquidus temperature is directly poured into an insulated vessel without using any jig, thereby generating crystal nuclei in the liquid alloy.

Subsequently, the liquid alloy having crystal nuclei that has been superheated by a degree ( $X^{\circ}\text{C}$ ) of less than  $10^{\circ}\text{C}$  above the liquidus temperature is held in the insulated vessel for a period from 5 seconds to 60 minutes as said alloy is cooled to a molding temperature that is higher than the eutectic or solidus temperature and where a specified fraction liquid is established, such that the cooling to the liquidus temperature of said alloy is completed within a time shorter than the time Y (in minutes) calculated by the relation  $Y=10-X$  and that the period of cooling from the initial temperature at which said alloy is held in the insulated vessel to a temperature  $5^{\circ}\text{C}$  lower than the liquidus temperature is not longer than 15 minutes, whereby fine spherical primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.

Alternatively, a partially solid, partially liquid alloy (at a temperature not lower than a molding temperature higher than the eutectic or solidus temperature) is held within the insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, such that the period of cooling from the initial temperature at which said alloy is held within the insulated vessel to a temperature  $5^{\circ}\text{C}$  lower than the liquidus temperature of said alloy is not longer than 150 minutes, whereby fine spherical primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.

The specific procedure of semisolid metal forming to be performed in Example 2 is essentially the same as described in Example 1.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in see Fig. 3, namely, the step of pouring the molten metal on to the ceramic jig 20, the step of generating and spheroidizing primary crystals and the forming step, are set forth below more specifically. Also discussed below is the criticality of the numerical limitations set forth in claims 11 - 13.

If the alloy to be held within the insulated vessel 30 is superheated such that its initial temperature is at least  $10^{\circ}\text{C}$  above the liquidus line, only unspherical primary crystals of a size of  $300\mu\text{m}$  and larger will form and fine, spherical primary crystals cannot be obtained no matter what conditions are used to cool the alloy to the molding temperature where a specified fraction liquid is established with a view to introducing crystal nuclei into the melt. To avoid this problem, the initial temperature of the alloy held within the insulated vessel 30 is controlled to be less than  $10^{\circ}\text{C}$  above the liquidus line.

If the alloy to be held within the insulated vessel 30 is superheated such that its initial temperature is less than  $10^{\circ}\text{C}$  above the liquidus line, the alloy must be cooled to the liquidus temperature within a shorter time than the period calculated by the relation  $Y=10-X$ , where Y is the time (in minutes) taken for the alloy temperature to drop to the liquidus temperature and X is the degree of superheating (in  $^{\circ}\text{C}$ ). Otherwise, unspherical primary crystals of a size of  $300\mu\text{m}$  and larger will form as is the case where the degree of superheating is  $10^{\circ}\text{C}$  or more above the liquidus line. To avoid

this problem, the alloy is cooled to the liquidus temperature within a shorter time than the period calculated by the relation  $Y=10-X$ .

Even if the alloy is cooled from the initial temperature to the liquidus temperature within a shorter time than the period determined by the relation  $Y=10-X$ , unspherical primary crystals of a size of  $300\mu\text{m}$  and larger will form or the size of spherical crystals to be obtained tends to be larger than  $200\mu\text{m}$  if the cooling from the initial temperature to the temperature  $5^\circ\text{C}$  lower than the liquidus temperature is completed within 15 minutes. Therefore, the period of cooling from the initial temperature to the temperature  $5^\circ\text{C}$  lower than the liquidus temperature should not be longer than 15 minutes.

Speaking now of the case where the alloy to be held within the insulated vessel 30 is in a partially solid, partially liquid state having an initial temperature lower than the liquidus temperature, the cooling from the initial temperature to the temperature  $5^\circ\text{C}$  lower than the liquidus temperature must be completed within 15 minutes; otherwise, unspherical primary crystals of a size of  $300\mu\text{m}$  and larger will form or the size of spherical crystals to be obtained tends to be larger than  $200\mu\text{m}$ . Therefore, the period of cooling from the initial temperature to the temperature  $5^\circ\text{C}$  lower than the liquidus temperature should not be longer than 15 minutes.

Figs. 15 and 16 show how the holding time affects the crystal grain sizes of AZ91 and AC4CH which respectively are typical magnesium and aluminum alloys. The "holding time" is the time for which the metal as poured into the insulated vessel is held until the molding temperature is reached. The "molding temperature" is a typical value at which about 50% fraction liquid is established and it is  $570^\circ\text{C}$  for AZ91 and  $585^\circ\text{C}$  for AC4CH. Obviously, the dependency of the crystal grain size on the holding time differs with the alloy type but in both cases the grain size tends to be greater than  $200\mu\text{m}$  if the holding time exceeds 60 minutes. On the other hand, primary crystals finer than  $200\mu\text{m}$  are prone to occur in the present invention. Figs. 17 and 18 show how the degree by which the AZ91 and AC4CH within the holding vessel are superheated above the liquidus temperature and the holding time from the initial temperature within the insulated vessel to the liquidus temperature will affect the crystal grain sizes of the respective alloys.

In the area of each graph where the degree of superheating ( $^\circ\text{C}$ ) and the holding time (min) are below the line connecting two points (10, 0) and (0, 10), fine ( $<200\mu\text{m}$ ) primary crystals are generated in accordance with the invention as shown diagrammatically in Fig. 13. In the area above the line, coarse ( $>300\mu\text{m}$ ) unspherical primary crystals occur as shown diagrammatically in Fig. 14. Even finer and more homogeneous primary crystals are obtained under the conditions for the holding time and the degree of superheating that are represented by area (C) in Fig. 17 and 18 [the region bound by points (0,6), (5,5) and (6,0) in Fig. 17 and the region bound by points (0,7), (5,5) and (5,0) in Fig. 18]. Figs. 19 and 20 show how the holding time (from the initial temperature within the insulated vessel to the liquidus temperature minus  $5^\circ\text{C}$ ) affects the crystal grain sizes of AZ91 and AC4CH, respectively. Obviously, the crystal grain size increases with the holding time and if the latter exceeds 15 minutes, there is a marked tendency for the crystal grain size to exceed  $200\mu\text{m}$  and coarse unspherical primary crystals occur. In the present invention where the holding time is less than 15 minutes, there is a marked tendency for the primary crystals to be generated in small sizes less than  $200\mu\text{m}$ .

### Example 3

An example of the invention (as recited in claims 14 and 15) will now be described in detail with reference to the accompanying Figs. 3, 7, 8 and 21 - 28, in which: Fig. 21 is a side view of an apparatus 100 for producing a semisolid forming metal; Fig. 22 is a perspective view of a cooling jig 1 as part of the nucleus generating section 12 of the apparatus 100; Fig. 23 shows in cross section two other cooling jigs 1A and 1B; Fig. 24 is a sectional side view of another cooling jig 1C which is funnel-shaped; Fig. 25 is a plan view showing the general layout of another apparatus 100A for producing a semisolid forming metal; Fig. 26 is a longitudinal section A - A of Fig. 25; Fig. 27 is a longitudinal section B - B of Fig. 25; Fig. 28 is a longitudinal section of an insulated vessel 22; Fig. 3 shows a process flow illustrating the method of producing a semisolid forming metal; Fig. 7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig. 8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part produced by a prior art process in which the molten metal is directly poured into the insulated vessel for cooling without passing through the nucleus generating section.

As shown in Fig. 21, the apparatus 100 for producing semisolid forming metal consists of the nucleus generating section 12 and a crystal generating section 18. The nucleus generating section 12 consists of the cooling jig 1 having a pair of weirs 2 provided to project from the right and left sides of the top surface of an inclined flat copper plate, stands 3 for supporting the jig 1 in an inclined position, and cooling pipes 4 (an inlet pipe 42 and an outlet pipe 4b) which are connected to a passage through which a cooling medium (usually water) is to be supplied into the cooling jig 1. The crystal generating section 18 serves to generate fine crystals by ensuring that the molten metal obtained in the nucleus generating section 12 is held as it is cooled to a molding temperature where it becomes partially solid, partially liquid. The crystal generating section 18 is constituted of the insulated vessel 22 which serves as a container of the molten metal M pouring down the cooling jig 1. As shown in Fig. 28, the insulated vessel 22 may optionally be accommodated within a metallic container 24 and equipped with a bolted cover plate 25 to ensure rigidity. As will be mentioned herein-

after, a pair of hooks 24a made of a round steel bar are provided to project from the lateral side of the metallic container 24 in order to assure convenience in transport.

If a flat metallic (e.g. Cu) plate is to be used as the cooling jig 1, the molten metal can potentially stick to the cooling plate; to prevent this problem, it is desirable to reduce the wettability of the plate by applying a nonmetallic (e.g. BN) coating material onto its surface. Weirs 2 are provided to control the flow of the molten metal as it descends the top surface of the cooling jig 1.

Fig. 23 shows the case where cooling jig 1A in the form of a cylindrical tube or cooling jig 1B in the form of a semicylindrical tube 1B is used as the cooling jig. As in the case of the cooling jig 1 in the form of a flat copper plate, both cooling jigs 1A and 1B are equipped with a cooling medium channel 5 and cooling pipes 4 (inlet pipe 4a and outlet pipe 4b).

A funnel-shaped tube may be used as the cooling jig as shown in Fig. 24. The cooling jig 1C may be stationary while the molten metal M is poured so that it drips into the underlying insulated vessel 22. Alternatively, in order to provide an enhanced cooling effect, the cooling jig 1C may be rotationally journaled on a thrust bearing 1b on a pedestal 1a such that the molten metal is poured into the jig as it is rotated at slow speed by means of a reduction motor 1f which transmits the rotating power via spur gears 1e and 1d.

To obtain a semisolid forming metal with the thus constructed apparatus 100, a molten alloy held superheated to less than 300°C above the liquidus temperature is poured on to the upper end of the cooling jig 1 (or 1A, 1B or 1C) in the nucleus generating section 12 so that the alloy flows down the jig. During the flowing of the alloy, the surface temperature of the cooling jig 1 is held to be lower than the melting point of the alloy. The molten alloy which has flowed down the cooling jig 1 (or 1A, 1B or 1C) is gently received by the insulated vessel 22, in which it is held for a period from 5 seconds to 60 minutes in such a condition that its temperature is not higher than the liquidus temperature but higher than the eutectic or solidus temperature, whereby a large number of fine spherical primary crystals are generated to ensure that the alloy can be shaped at a specified fraction liquid.

The specific procedure of semisolid metal forming to be performed in Example 3 is essentially the same as described in Example 1.

As already mentioned, the holding time within the insulated vessel 22 varies widely from 5 seconds to 60 minutes depending on the time taken for the alloy to be cooled to the molding temperature. If the holding time is as long as 10 - 60 minutes, the productivity is very low on an apparatus in which one nucleus generating section 12 (cooling jig 1) is combined with one crystal generating section 18 (insulated vessel 22).

In order to solve this problem, the present inventors have devised an apparatus that shortens the interval between successive cooling cycles so as to enhance the efficiency of the production of semisolid forming metals. Shown by 100A in Fig. 25, the apparatus comprises a turntable 60 that is capable of suspending a plurality of insulated vessels 22 on the circumference and which is free to rotate horizontally about a central shaft 62. Each of the insulated vessels 22 is accommodated within a metallic container 24 which, as shown in Fig. 28, is fitted with a pair of hooks 24a that are each formed of a round steel bar and which are welded to project from the lateral side of the container 24. The turntable 60 is provided with semicircular cutouts in the circumference that are spaced apart at generally equal intervals and which have a greater diameter than the metallic container 24; at the same time, the turntable 60 has as many hook receptacles 30a as the insulated vessels 22 and each receptacle 30a is in the form of a semicircular pipe that extends horizontally from the circumference of the turntable 60 so that the hooks 24a will rest on the receptacle to suspend the metallic container 24 which is integral with the insulated vessel 24 as shown in Fig. 28.

Each of the insulated vessels 22 suspended on the turntable 60 is charged with the molten metal via the cooling jig 1 on the left side (see Fig. 25) and carried by the slowly rotating turntable until it reaches the diametrically opposite position (as a result of 180° turn) after the passage of a predetermined cooling period. In this diametrically opposite position (i.e. on the right side of the turntable), a hydraulic cylinder or other means 26 for vertically moving the insulated vessel 22 is provided below the position where the insulated vessel is suspended (see Fig. 26). The hydraulic cylinder 26 serves to push up the bottom of the insulated vessel 22 so that it is transferred to an injection sleeve 40 at the subsequent stage, which is then supplied with the partially solidified metal from within the insulated vessel.

If the molten metal flowing down the cooling jig 1 is directly poured into the erect insulated vessel 22, air will be entrapped to potentially cause casting defects. To avoid this problem, it is desirable to incline the insulated vessel 22 by a specified angle such that the molten metal will gently pour into the insulated vessel along its sidewall (see Fig. 27). To this end, a hydraulic cylinder or some other depressing means 28 is provided below the cooling jig 1; as shown, the hydraulic cylinder 28 has a piston rod 28a fitted at the terminal end with a rotatable depressing plate 28b supported on a pin.

The thus constructed apparatus 100A for producing semisolid forming metals is capable of feeding the molten metal into the injection sleeve by continuous treatment in a plurality of insulated vessels 22 and compared to the apparatus using a single unit of insulated vessels 22, the interval between successive cooling cycles is substantially reduced to ensure against the drop in productivity.

Thus, the apparatus 100 and 100A according to the invention are capable of producing semisolid metals that are suitable for use in semisolid forming, that have fine primary crystals dispersed within a liquid phase and that are free

from the contamination by nonmetallic inclusions. In addition, due to the holding of the molten metal within the insulated vessel for cooling purposes, the semisolid metal obtained is difficult to be oxidized at the surface and has a very uniform temperature profile in its interior; hence, with almost all alloys, there is no need to use a high-frequency furnace for heating molding materials although this has been necessary in the conventional semisolid forming technology.

If desired, a robot or a dedicated machine may be used to grip the insulated vessel 22 and when the metal within the vessel has attained a specified molding temperature, it may be inserted into the injection sleeve 40 in a die casting machine (which may be a squeeze casting machine), with the top end directed to the side facing the injection tip, such as to accomplish semisolid forming. In this way, one can produce castings or high quality that have fine, spherical primary crystals as shown in Fig. 7. In fact, however, only coarse dendrites with slightly round corners as shown in Fig. 8 can be obtained by simply pouring the molten metal into the insulated vessel 22 without passing through the nucleus generating section 12. The semisolid metals produced with the apparatus of the invention may be shaped by pressure forming methods other than die casting; alternatively, they may be inserted into a sand or metallic mold gently without applying pressure.

In the example described above, the flat copper plate having internal cooling means is used as the nucleus generating means but this is not the sole case of the invention and any other means may be employed as long as it is capable of generating crystal nuclei that will not redissolve in the liquid phase. As example of this alternative nucleus generating means is described below.

The flat copper plate without weirs 2 may be replaced by the tubular cooling jig 1A or semicylindrical cooling jig 1B as shown in Fig. 23. Alternatively, the molten metal may be poured into the conical cooling jig 1C as it is rotated by drive means and after crystal nuclei have been generated in the metal, the latter is withdrawn from the bottom the cooling jig 1C to be poured into the insulated vessel 22. The constituent material of the cooling jig 1 is by no means limited to metals and it may be of any type as long as it is capable of cooling the molten alloy within a specified time while producing crystal nuclei in the alloy.

In the example described above, the insulated ceramic vessel is used as the crystal generating means and in a practical version of the example, the rotating turntable 60 which is capable of arranging a plurality of insulated vessels 22 is used. However, this is not the sole method of arranging and fixing the insulated vessels 22 and they may be linearly or otherwise arranged. To fix the insulated vessel 22, it may be positioned at a specified site as typically shown in Fig. 28, wherein the insulated vessel 22 is placed within the metallic container 24 having a slightly larger inside diameter and the bottom of the container 24 is pushed up by the hydraulic cylinder 26 as required.

In the above description of the invention, the cooling jig consists of the nucleus generating section and the crystal generation section but, if desired, the two steps may be integrated. For instance, the molten metal within the insulated vessel 22 may be treated with the cooling jig and/or a melt surface vibrating jig to ensure that both nuclei and crystals will be generated.

#### Example 4

An example of the invention (as recited in claims 16 and 17) will now be described with reference to accompanying Figs. 1, 2, 4 - 8 and 29 - 31, in which: Fig. 1 is a diagram showing a process sequence for the semisolid forming of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit; Fig. 2 is a diagram showing a process sequence for the semisolid forming of a magnesium or aluminum alloy having a composition within a maximum solubility limit; Fig. 29 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 29; Fig. 30 compares two graphs plotting the temperature changes in the metal being cooled within a vessel during step 3 shown in Fig. 29; Fig. 31 illustrates four methods of managing the temperature within a vessel according to the invention; Fig. 5 is an equilibrium phase diagram for an Al-Si alloy as a typical aluminum alloy system; Fig. 6 is an equilibrium phase diagram for a Mg-Al alloy as a typical magnesium alloy system; Fig. 7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig. 8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs 1, 2, 5 and 6, the invention recited in claims 16 and 17 is based on claims 2, 9 and 10 and it is such that:

- (1) the melt of a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit or the melt of a magnesium alloy of a composition within a maximum solubility limit is held superheated to less than 300°C above the liquidus temperature and then contacted with a surface of the jig 20 having a lower temperature than the melting point of either alloy and the resulting alloy is poured into a vessel 30; or
- (2) the melt of an aluminum or magnesium alloy that is held superheated to less than 100°C above the liquidus temperature as it contains an element to promote the generation of crystal nuclei is directly poured into the vessel 30 without using the jig 20. The vessel 30 of a specified wall thickness is adapted to be heatable or coolable from either



inside or outside, is made of a material having a thermal conductivity of at least  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  (at room temperature) and is held at a temperature not higher than the liquidus temperature of said alloy prior to its pouring, and the melt is subsequently cooled to a temperature at which a fraction solid appropriate for shaping is established, such that while the alloy is poured into the vessel 30, its top and bottom portions are heated by a greater degree than the middle portion or that the top or bottom portion is heat-retained with a heat-retaining material having a thermal conductivity of less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  or that the top portion of the vessel is heated by a greater degree than the middle portion while the bottom portion is heat-retained or that the top portion is heat-retained while the bottom portion is heated by a greater degree than the middle portion, whereby nondendritic fine primary crystals are crystallized in the alloy solution while, at the same time, the alloy is cooled at a sufficiently rapid rate to provide a uniform temperature profile through the alloy in the vessel 30, with the cooled alloy being subsequently supplied into a forming mold 50, where it is pressure formed to a shape.

Four methods of managing the temperature of the vessel 30 and that of the alloy within the vessel 30 are collectively shown in Fig. 31, wherein (a) - (d) correspond to the methods of temperature management set forth in claim 17.

The wall thickness of the vessel 30 is desirably such that after pouring of the molten metal, no dendritic primary crystals will result from the metal in contact with the inner surface of the vessel and yet no solidified layer will remain in the vessel at the stage where the semisolid metal has been discharged from within the vessel just before shaping. The exact value of the wall thickness of the vessel is appropriately determined in consideration of the alloy type and the weight of the alloy in the vessel 30.

The term "fraction solid appropriate for shaping" means a relative proportion of the solid phase which is suitable for pressure forming. In high-pressure casting operations such as die casting and squeeze casting, the fraction solid ranges from 10% to 80%, preferably from 30% to 70%. If the fraction solid is more than 70%, the formability of the raw material is poor; below 30%, the raw material is so soft that it is not only difficult to handle but also less likely to produce a homogeneous structure. In extruding and forging operations, the fraction solid ranges from 30% to 99.9%, preferably from 50% to 99.9%; if the fraction solid is less than 50%, an inhomogeneous structure can potentially occur.

The "temperature not higher than the liquidus temperature" means such a temperature that even if the temperature of the metal within the vessel is rapidly lowered to the level equal to the molding temperature, no dendritic primary crystals will result from the melt in contact with the inner surface of the vessel and yet no solidified layer will remain in the vessel at the stage where the semisolid metal is discharged from within the vessel just before shaping. The exact value of the "temperature not higher than the liquidus temperature" varies with the alloy type and the weight of the alloy within the vessel.

The "vessel" as used in the invention is a metallic or nonmetallic vessel, or a metallic vessel having a surface coated with nonmetallic materials or semiconductors, or a metallic vessel compounded of nonmetallic materials or semiconductors. Coating the surface of the metallic vessel with a nonmetallic material is effective in preventing the sticking of the metal. To heat the vessel, its interior or exterior may be heated with an electric heater; alternatively, induction heating with high-frequency waves may be employed if the vessel is electrically conductive.

The specific procedure of semisolid metal forming to be performed in Example 4 is essentially the same as described in Example 1.

Vessel 30 is used to hold the molten metal until it is cooled to a specified fraction solid after its temperature has dropped just below the liquidus line. If the thermal conductivity of the vessel 30 is less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  at room temperature, it has such a good heat insulating effect that an unduly prolonged time will be required for the molten metal M in the vessel 30 to be cooled to the temperature where a specified fraction solid is established, thereby reducing the operational efficiency. In addition, the generated spherical primary crystals become coarse to deteriorate the formability of the alloy. It should, however, be mentioned that if the vessel contains a comparatively small quantity of the melt, the holding time necessary to achieve the intended cooling becomes short even if the thermal conductivity of the vessel is less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  at room temperature. If the temperature of the vessel 30 is higher than the liquidus temperature, the molten metal M as poured into the vessel is higher than the liquidus temperature, so that only a few crystal nuclei will remain in the liquid phase to produce large primary crystals. If the top and bottom portions of the vessel are neither heated nor heat-retained as the molten metal M is cooled until the fraction solid in the metal reaches the value appropriate for shaping, dendritic primary crystals may occur at the site in the top or bottom portion of the vessel that is contacted by the metal M or a solidified layer will grow at that site, thereby creating a nonuniform temperature profile through the metal in the vessel which makes the subsequent shaping operation difficult to accomplish on account of the remaining solidified layer within the vessel. To avoid these difficulties, it is preferred to heat the top or bottom portion of the vessel by a greater degree than the middle portion while the bottom or top portion is heat-retained during the cooling process after the pouring of the metal; if necessary, the top or bottom portion of the vessel may be heated not only during the cooling process following the pouring of the metal but also prior to its pouring and this is another preferred practice in the invention.

The constituent material of the vessel 30 is in no way limited except on the thermal conductivity and those which are poorly wettable with the molten metal are preferred.

Table 2 shows the conditions of various samples of semisolid metal to be shaped, as well as the qualities of shaped parts. As shown in Fig. 29, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed, 1.0 m/s; casting weight (including biscuits), 30 kg; mold temperature, 230°C.

Table 2 (continued on next page)

No.	Alloy	Casting temperature (°C)	Cooling jig	Temperature of the cooling jig (°C)	Thermal conductivity of holding vessel (kcal/hr·m·°C)	Temperature of the holding vessel *1			Heating or Heat-retaining of the holding vessel		
						Upper part	Middle part	Lower part	Upper part	Middle part	Lower part
1	AC4CH	640	Used	25	0.3	100	100	100	No treatment	No treatment	No treatment
2	AC4CH	640	Used	25	0.3	200	100	300	No treatment	No treatment	No treatment
3	AC4CH	640	Used	25	14	100	100	100	No treatment	No treatment	No treatment
4	AC4CH	640	Used	25	14	25	25	25	No treatment	No treatment	No treatment
5	AC4CH	950	Used	25	14	100	100	100	No treatment	No treatment	No treatment
6	AC4CH	640	Used	625	14	100	100	100	No treatment	No treatment	No treatment
7	AC4CH	640	Used	25	14	200	100	250	Heat-retained	No treatment	Heated
8	AC4CH	640	Used	25	14	500	400	500	Heat-retained	No treatment	Heated
9	AC4CH	640	Used	25	14	200	100	200	Heat-retained	No treatment	Heated
10	AC4CH	670	Used	25	14	250	250	250	Heated	No treatment	Heated
11	AC4CH	640	Used	25	14	300	200	300	Heat-retained	No treatment	Heat-retained
12	AC4CH	660	Used	25	14	200	200	200	Heated	No treatment	Heat-retained
13	AC4CH	640	Not used	-	14	200	100	200	Heat-retained	No treatment	Heated
14	AC4CH	640	Used	25	14	300	200	300	Heat-retained	No treatment	Heated

Table 2 (continued)

	No.	Alloy	Quality of shaped part				Time to molding temperature *2 (min)	Remarks
			Amount of unspherical primary crystal	Primary crystal size (μm)	Solidified layer within vessel	Structural homogeneity		
Comparative Sample	1	AC4CH	○	150	×	○	30	Small thermal conductivity; the vessel was neither heated nor heat-retained.
	2	AC4CH	○	150	○	○	34	Small thermal conductivity
	3	AC4CH	○	80	×	×	12	The vessel was neither heated nor heat-retained.
	4	AC4CH	×	90	×	×	6	The vessel was neither heated nor heat-retained; its wall thickness was 20mm.
	5	AC4CH	×	500	×	×	22	High casting temperature
	6	AC4CH	×	450	×	×	12	High jig temperature
	7	AC4CH	△	100	○	×	3 *3	Low fraction solid (8%)
Invention Sample	8	AC4CH	○	100	○	○	17	
	9	AC4CH	○	85	○	○	10	
	10	AC4CH	○	90	○	○	11	
	11	AC4CH	○	90	○	○	13	
	12	AC4CH	○	90	○	○	13	
	13	AC4CH	○	170	○	○	14	No cooling jig was used.
	14	AC4CH	○	80	○	○	9	

\*1 : Temperature of the vessel before pouring of the metal

\*2 : Molding temperature at 50% fraction solid (excepting \*3)

\*3 : Molding temperature at 8% fraction solid

Wall thickness of the holding vessel: 5mm (but 20mm with No.4)

Amount of unspherical primary crystals: ○, small; ×, large

Structural homogeneity: ×, many segregations; ○, a few segregations

Solidified layer within vessel: ○, absent; ×, present

AC4CH ; Al-7%Si-0.35%Mg m.p. 615°C  
A291 ; Mg-9%Al-0.7%Zn m.p. 595°C

In Comparative Sample 1, the thermal conductivity of the holding vessel was small and, in addition, the vessel was heated or heat-retained inappropriately after the pouring of the metal so that the holding time to the shaping tempera-

ture was unduly long; what is more, the formation of a solidified layer within the vessel prevented the discharge of the semisolid metal, thus making it impossible to perform shaping. In Comparative Sample 2, the thermal conductivity of the holding vessel was so small that the holding time to the shaping temperature was unduly prolonged. In Comparative Sample 3, the holding vessel was heated or heat-retained inappropriately after the pouring of the metal so that a solidified layer formed within the vessel to prevent the discharge of the semisolid metal, thus making it impossible to start the shaping step. In Comparative Sample 4, the wall thickness of the holding vessel was unduly great and, in addition, the vessel was heated or heat-retained inappropriately after the pouring of the metal so that unspherical primary crystals were generated; what is more, the formation of a solidified layer within the vessel prevented the discharge of the semisolid metal, thus making it impossible to perform shaping. In Comparative Sample 5, the casting temperature was so high that very few crystal nuclei remained within the vessel to yield only coarse unspherical primary crystals as shown in Fig. 8. In Comparative Sample 6, the cooling jig had such a high temperature that the number of crystal nuclei formed was insufficient to produce fine spherical primary crystals and, instead, only coarse unspherical primary grains formed as in Comparative Sample 5. In Comparative Sample 7, the fraction solid in the metal was so small that many segregations occurred within the shaped part.

In Invention Samples 8 - 14, the metal in the vessel 30 was rapidly cooled with its temperature profile being maintained sufficiently uniform that semisolid metals having nondendritic fine primary crystals were produced in a convenient and easy way. Such alloys were then fed into a forming mold and pressure formed to produce shaped parts of a homogeneous structure having fine ( $<200\mu\text{m}$ ) spherical primary crystals.

## Example 5

An example of the invention (as recited in claim 18) will now be described with reference to the accompanying Figs. 4, 9, 10 and 32 - 35, in which: Fig. 9 is a diagram showing a process sequence for the semisolid forming of hypoeutectic aluminum alloys having a composition at or above a maximum solubility limit; Fig. 10 is a diagram showing a process sequence for the semisolid forming of magnesium or aluminum alloys having a composition within a maximum solubility limit; Fig. 32 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 32; Fig. 33 compares the temperature profiles through two semisolid metals, one being held within a vessel in step (3) shown in Fig. 32 and the other being treated by the prior art without using any outer vessel; Fig. 34 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art; and Fig. 35 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention.

As shown in Figs. 9, 10 and 32, the invention recited in claim 18 is such that the melt of a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit or the melt of a magnesium or aluminum alloy of a composition within a maximum solubility limit is held superheated to less than  $300^{\circ}\text{C}$  above the liquidus temperature, contacted with a surface of the jig 20 at a lower temperature than the melting point of either alloy, and poured into a holding vessel 29 of a specified wall thickness that is made of a material having a thermal conductivity of at least  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^{\circ}\text{C}$  (at room temperature) and that is preliminarily held at a temperature not higher than the liquidus temperature of either alloy, and the melt is subsequently cooled, with a heat insulating lid 32 placed on top of the holding vessel, down to a temperature at which a fraction solid appropriate for shaping is established, characterized in that during the cooling of the alloy, the outer surface of said holding vessel is heated or heat-retained with an outer vessel 31 capable of accommodating said holding vessel, whereby nondendritic fine spherical primary crystals are crystallized in the alloy within said holding vessel while the cooling rate is controlled to be rapid enough to provide a uniform temperature profile through the alloy in said holding vessel no later than the start of the forming step and, thereafter, the cooled alloy is fed into a mold where it is subjected to pressure forming.

The wall thickness of the holding vessel 29 is desirably such that after pouring of the molten metal, no dendritic primary crystals will result from the metal in contact with the inner surface of the vessel and yet no solidified layer will remain in the vessel at the stage where the semisolid metal has been discharged from within the vessel just before shaping. The exact value of the wall thickness of the vessel is appropriately determined in consideration of the alloy type and the weight of the alloy in the holding vessel 29.

The term "fraction solid appropriate for shaping" means a relative proportion of the solid phase which is suitable for pressure forming. In high-pressure casting operations such as die casting and squeeze casting, the fraction solid ranges from 10% to 80%, preferably from 30% to 70%. If the fraction solid is more than 70%, the formability of the raw material is poor; below 30%, the raw material is so soft that it is not only difficult to handle but also less likely to produce a homogeneous structure. In extruding and forging operations, the fraction solid ranges from 30% to 99.9%, preferably from 50% to 99.9%; if the fraction solid is less than 50%, an inhomogeneous structure can potentially occur.

The "temperature not higher than the liquidus temperature" means such a temperature that even if the temperature of the alloy within the holding vessel is rapidly lowered to the level equal to the molding temperature, no dendritic primary crystals will result from the melt in contact with the inner surface of the holding vessel and yet no solidified layer

will remain in the vessel at the stage where the semisolid alloy has been discharged from within the vessel just before shaping. The "temperature not higher than the liquidus temperature" is also such that the alloy containing crystal nuclei can be poured into the holding vessel 29 without losing the crystal nuclei. The exact value of this temperature differs with the alloy type and the weight of the alloy within the holding vessel.

5 The "holding vessel" as used in the invention is a metallic or nonmetallic vessel, or a metallic vessel having a surface coated with nonmetallic materials or semiconductors, or a metallic vessel compounded of nonmetallic materials or semiconductors. Coating the surface of the metallic vessel with a nonmetallic material is effective in preventing the sticking of the metal.

10 The "outer vessel" as used in the invention serves to ensure that the alloy in the holding vessel will be cooled within a specified time. To this end, the outer vessel, must have the ability to cool the, holding vessel 29 rapidly in addition to a capability for heat-retaining or heating said vessel. To meet this requirement, the temperature of the outer vessel 31 should be lowered to the level equal to the molding temperature within a specified time.

15 In order to provide a more uniform temperature profile through the alloy within the holding vessel 29, the outer vessel 31 may be provided with a temperature profile by, for example, heating the top and bottom portions of the outer vessel 31 in a high-frequency heating furnace by a greater degree than the middle portion. In the case where the outer vessel 31 starts to be heated before the holding vessel 29 is inserted and continues to be heated until after its insertion, the heating of the outer vessel 31 may be interrupted temporarily if it is necessary for adjusting the temperature of the alloy within the holding vessel 29.

20 The inside diameter of the outer vessel 31 is made sufficiently larger than the outside diameter of the holding vessel 29 to provide a clearance between the outer vessel 31 and the holding vessel 29 accommodated in it. To insure the clearance, a plurality of projections are provided along the outer circumference of the holding vessel 29 and/or the inner circumference of the outer vessel 31. Alternatively, the clearance may be insured by replacing the projections with recesses formed in either the outer circumference of the holding vessel or the inner circumference of the outer vessel.

25 The gap between the holding vessel 29 and the outer vessel 31 is typically filled with air but various other gases may be substituted such as inert gases, carbon dioxide and  $\text{SF}_6$ .

30 According to the invention, semisolid metal forming will proceed by the following specific procedure. In step (1) of the process shown in Figs. 32 and 4, a complete liquid form of metal M is contained in a ladle 10. In step (2), the low-temperature melt (which may optionally contain an element that is added to promote the generation of crystal nuclei) is cooled with a jig 20 to generate crystal nuclei; in step (3)-0, the melt is poured into a vessel 30 that is preliminarily held at a specified temperature not higher than the liquidus temperature, thereby yielding an alloy containing a large number of crystal nuclei at a temperature either just below or above the liquidus line.

35 Alternatively, the cooling jig 20 may be dispensed with and the low-temperature melt of a composition just above the melting point and which contains an element added to promote the generation of a fine structure may be directly poured into the holding vessel 29 which is preliminarily maintained at a temperature not higher than the liquidus temperature.

40 In subsequent step (3), the holding vessel 29 is accommodated within the outer vessel 31 lined with a heat insulator 33 on the bottom and then fitted with a lid. Thereafter, the alloy in the holding vessel is held in a semisolid condition with its temperature being lowered, whereby fine particulate (nondendritic) primary crystals are generated from the introduced crystal nuclei. In order to ensure that the temperature in the holding vessel 29 is lowered under the temperature conditions specified in Figs. 9 and 10, the outer vessel 31 is temperature managed such as by internal or external heating or by induction heating, with the heating being performed only before or after the insertion of the holding vessel 29 or for a continued period starting prior to the insertion of the holding vessel and ending after its insertion.

Metal M thus obtained at a specified fraction solid is inserted into a die casting injection sleeve 70 and thereafter pressure formed within a mold cavity 50a on a die casting machine to produce a shaped part.

45 The casting, spheroidizing and molding conditions that are respectively set for the steps shown in (see Fig. 9), namely, the step of pouring the molten metal on to the cooling jig, the step of generating and spheroidizing primary crystals and the forming step, are set forth below more specifically. Also discussed below is the criticality of the numerical limitations set forth in claim 18.

50 The holding vessel 29 is used to hold the molten metal until it is cooled to a specified fraction solid after its temperature has dropped just below the liquidus line. If the thermal conductivity of the vessel 29 is less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  (at room temperature), it has such a good heat insulating effect that an unduly prolonged time is required for the molten metal M in the holding vessel 29 to be cooled to the temperature where a specified fraction solid is established, thereby reducing the operational efficiency. In addition, the generated spherical primary crystals become coarse to deteriorate the formability of the alloy.

55 It should, however, be mentioned that if the holding vessel contains a comparatively small quantity of the melt, the holding time necessary to achieve the intended cooling becomes short even if the thermal conductivity of the vessel is less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  at room temperature. If the temperature of the holding vessel 29 is higher than the liquidus temperature, the molten metal M as poured into the vessel is higher than the liquidus line, so that only a few crystal nuclei will remain in the liquid phase to produce large primary crystals. In order to endure a more uniform temperature

profile through the alloy within the holding vessel 29 by means of the outer vessel 31 while the molten metal M is cooled to a temperature where the fraction solid appropriate for shaping is established, either one of the following conditions should be satisfied: the top of the holding vessel 29 should be fitted with a lid; an adequate clearance should be provided between the holding vessel 29 and the outer vessel 31; a heat insulator should be provided in the area where the bottom of the holding vessel 29 contacts the outer vessel 31; or projections or recesses should be provided on either the holding vessel 29 or the outer vessel 31.

In the example under discussion, the crystal nuclei were generated by the method of the invention recited in claims 2, 9 and 10.

Table 3 shows the conditions of the holding vessel, the alloy within the holding vessel, and the outer vessel, as well as the qualities of shaped parts. As shown in Fig. 32, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed; 1.0m/s; casting weight (including biscuits), 2 kg; mold temperature, 250°C.

Table 3 (continued on next page)

	No.	Alloy	Temperature of cooling plate (°C)	Initial temperature of holding vessel (°C)	Constituent material of holding vessel	Initial temperature of the alloy within holding vessel (°C)	Constituent material of outer vessel	Method of heating the outer vessel
Invention Sample	1	AZ91	20	250	SUS	601	SUS	B
	2	AZ91	20	450	SUS	601	Graphite	C
	3	AZ91	100	250	SUS	599	Graphite	C
	4	AZ91	20	250	SUS	597	Graphite	C
	5	AZ91	20	250	SUS	600	SUS	A
	6	AZ91	20	250	SUS	601	SUS	B
	7	AZ91	*5	100	SUS	599	Graphite	C
	8	AC4CH	20	450	SiN	616	Graphite	B
Comparative Sample	9	AC4CH	20	250	SUS	615	Graphite	C
	10	AZ91	20	200	SUS	601	*6	-
	11	AC4CH	20	250	SUS	615	*6	-
	12	AZ91	20	250	SUS	599	Graphite	A
	13	AC4CH	20	250	SUS	720 *7	Graphite	C
	14	AC4CH	20	250	SUS	615	Graphite	C
	15	AZ91	20	650	SUS	604	Graphite	C

(Notes)

\*1 m.p. AZ91: 598°C AC4CH: 618°C

\*2 A. The outer vessel was heated from inside with an electric heater.

B. The outer vessel was heated from outside with an electric heater.

C. The outer vessel was heated by induction heating.

\*3 A. Only before insertion of the holding vessel.

B. Only after insertion of the holding vessel.

C. From before insertion of the holding vessel until after its insertion.

\*4 Molding temperature was 570°C for AZ91 and 585°C for AC4CH, except that it was 610°C for No.14.

\*5 No cooling plate was used.

Table 3 (continued)

	No.	Alloy	Temperature of the outer vessel just before insertion of the holding vessel (°C)	When the outer vessel was heated	Holding time to molding temperature (min)	Size of primary crystal grains in molding material (μm)	Temperature profile through the metal with- in vessel
Inven- tion Sample	1	AZ91	480	C	5.0	80	○
	2	AZ91	480	A	6.1	100	○
	3	AZ91	610	A	9.4	97	○
	4	AZ91	540	A	5.8	93	○
	5	AZ91	20	B	5.5	83	○
	6	AZ91	600	C	50.0	175	○
	7	AZ91	480	A	6.5	145	○
	8	AC4CH	500	A	8.5	90	○
	9	AC4CH	300	A	4.5	81	○
	10	AZ91	-	-	1.5	70	x
Compara- tive Sample	11	AC4CH	-	-	2.5	60	x
	12	AZ91	650	C	70.1	220	○
	13	AC4CH	500	A	8.5	600	○
	14	AC4CH	300	A	0.04	40	x
	15	AZ91	480	A	6.5	3,000	x

\*6 No outer vessel was used.

\*7 Molten metal was poured on to the cooling plate at 950°C.

\*8 Not all primary crystals were spherical.

\*9 ○, Good (with temperature difference within 5°C between maximum and minimum values)

x, Poor (with temperature difference more than 5°C between maximum and minimum values)

\*10 Alloy weight, ca. 2kg

With Comparative Samples 10 and 11 which did not use the outer vessel, the temperature of the alloy within the holding vessel dropped so rapidly that fine primary crystals formed but, on the other hand, the temperature profile through the semisolid alloy in the holding vessel was poor as shown in the graph on left side of Fig. 33. With Comparative Sample 12, the semisolid metal holding time within the holding vessel was sufficiently long to provide a good tem-



perature profile through the metal in the holding vessel but, on the other hand, unduly large primary crystals formed. With Comparative Sample 13, the casting temperature was so high that the alloy as poured into the holding vessel acquired a sufficiently high temperature to either substantially preclude the generation of crystal nuclei or cause rapid disappearance of crystal nuclei, thereby yielding unduly large primary crystals. With Comparative Sample 14, the frac-  
 5 tion liquid in the semisolid metal was high whereas the holding time was short, thereby providing only a poor tempera-  
 ture profile through the semisolid alloy within the holding vessel.

In Invention Samples 1 - 9, the metal in the vessel was rapidly cooled with its temperature profile being maintained sufficiently uniform that semisolid metals having nondendritic fine primary crystals were produced in a convenient and easy way. Such alloys were then fed into a mold and pressure formed to produce shaped parts of a homogeneous  
 10 structure having fine ( $<200\mu\text{m}$ ) spherical primary crystals.

#### Example 6

Examples of the invention (as recited in claims 19 - 23) will now be described in detail with reference to accompa-  
 15 nying drawings 36 - 49 and 53, in which: Fig. 36 is a plan view showing the general layout of molding equipment (its first  
 embodiment) according to an example of the invention; Fig. 37 is a plan view of a temperature management unit (its  
 first embodiment) according to the example of the invention; Fig. 38 is a graph showing the specific positions of tem-  
 perature measurement within a vessel according to an example of the invention; Figs. 39, 40 and 41 are graphs show-  
 ing the temperature history of cooling within the vessel under different conditions; Fig. 42 is a longitudinal section of a  
 20 semisolid metal cooling furnace according to another example of the invention; Fig. 43 is a plan view of a temperature  
 management unit (its second embodiment) according to yet another example of the invention; Fig. 44 is a longitudinal  
 section A - A of Fig. 43; Fig. 45 shows the temperature profiles in the vessel fitted with heat insulators according to an  
 example of the invention; Fig. 46 is a plan view of a temperature management unit (its third embodiment) according to  
 another example of the invention; Fig. 47 shows schematically the composition of a temperature controller for a semi-  
 25 solid metal cooling furnace (its first embodiment) according to an example of the invention; Fig. 48 shows schematically  
 the composition of a temperature controller (its second embodiment) for a semisolid metal cooling furnace according to  
 another example of the invention; Fig. 49 is a longitudinal section of a vessel rotating unit according to an example of the  
 invention; and Fig. 53 is a longitudinal section of a semisolid metal cooling furnace as it is equipped with a vessel vibra-  
 tor according to another example of the invention.

30 As Fig. 36 shows, the molding equipment generally indicated by 300 consists of a melt holding furnace 14 for feed-  
 ing the molten metal as a molding material (containing a large number of crystal nuclei), a molding machine 200, and  
 a temperature management unit 104 for managing the temperature of the melt until it is fed to the molding machine 200.  
 The molten metal held within the furnace 14 contains a large number of crystal nuclei.

As also shown in Fig. 36, the temperature management unit 104 consists of a semisolid metal cooling section 110  
 35 and a vessel temperature control section 140; the semisolid metal cooling section 110 is composed of a semisolid metal  
 cooling furnace 120 and a semisolid metal slowly cooling furnace 130 which are connected in a generally rectangular  
 arrangement by means of a transport mechanism such as a conveyor 170 whereas the vessel temperature control sec-  
 tion 140 is composed of a vessel cooling furnace 150 and a vessel heat-retaining furnace 160. The temperature man-  
 agement unit 104 is also equipped with a robot 180 which grips the vessel 102 and transports it to one of the specified  
 40 positions A - F (to be described below).

The temperature management unit 104 is operated as follows. An empty vessel 102 is first located in the heating  
 vessel pickup position A. The robot 180 then transfers the vessel 102 to the position B, where the vessel is charged with  
 a prescribed amount of the molten metal from the melt holding furnace 14. Thereafter, the robot 180 transports the ves-  
 sel 102 to the filled vessel rest position C; subsequently, the vessel is cooled as it is carried by the conveyor 170 to pass  
 45 through the semisolid metal cooling furnace 120 in a specified period of time. The vessel 102 leaving the furnace 120  
 reaches the slurry vessel rest position D, from which it is immediately transferred to the sleeve position E by the robot  
 180 if the injection sleeve 202 in the molding machine 200 is ready to accept the molten metal; at position E, the slurry  
 of semisolid metal in the vessel is poured into the injection sleeve 202. If the injection sleeve 202 is not ready to accept-  
 the molten metal when the vessel 102 has reached the slurry vessel rest position D (i. e., if the molding machine is oper-  
 50 ating to perform pressure forming), the slurry of semisolid metal within the vessel will progressively solidify upon cooling  
 while it is waiting for acceptance in the position D, thereby making it impossible for all the slurry to be discharged from  
 the vessel or the crystal nuclei in the slurry will disappear to cause deterioration in the quality of the shaped part. In  
 order to avoid these problems, the vessel 102 is forwarded to the semisolid metal slowly cooling furnace 130, where it  
 waits for the molding machine 200 to become completely ready for the acceptance of the molten metal while ensuring  
 55 against its rapid cooling.

The vessel 102 from which the slurry of semisolid metal having satisfactory properties has been emptied into the  
 injection sleeve 202 is then transferred to the empty vessel rest position F by means of the robot 180, carried by the  
 conveyor 170 into the vessel cooling furnace 150, where it is cooled for a specified time, passed through the vessel

heat-retaining furnace 160 as it is held at a suitable temperature, and is thereafter returned to the heating vessel pick up position A.

A specific embodiment of the temperature management unit 104 is shown in Fig.37. In this first embodiment, aluminum alloys are to be treated at a comparatively small scale with the molten metal being poured in an amount of no more than 10 kg; the system configuration is such that the molding cycle on the molding machine 200 is about 75 seconds and the time of passage through the semisolid metal cooling furnace 120 and the vessel temperature controller 140 (i. e., consisting of the vessel cooling furnace 150 and the vessel heat-retaining furnace 160) is 600 seconds in total. If the total passage time is longer than 600 seconds, the overall equipment becomes impractically bulky and the volume of the slurry in process which results from machine troubles and which has to be discarded is increased and these are by no means preferred or the purpose of constructing commercial production facilities. Considering these points and in order to achieve consistent temperature management for a small quantity of slurry having good properties, the vessel 102 is made of an  $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$  composite having a small thermal conductivity ( $0.3 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$ ). As a result, a slurry of semisolid metal having satisfactory properties can be obtained if only the temperature of the vessel 102 is retained by circulation of hot air the temperature of which is set at a constant value of  $120^\circ\text{C}$ .

The system shown in Fig. 37 has the following differences from the system of Fig.36. Since the vessel 102 is made of the  $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$  composite, it has a sufficiently small thermal conductivity that one only need supply the interior of the semisolid metal cooling furnace 120 (which is set at a temperature of  $200^\circ\text{C}$ ) with a circulating hot air flow of a constant temperature from a hot air generating furnace 122. In addition, one only need equip the semisolid metal slowly cooling furnace 130 (which is set at a temperature of  $550^\circ\text{C}$ ) and the vessel heat-retaining furnace 160 (which is set at a temperature of  $100^\circ\text{C}$ ) with heaters 132 and 162, respectively. With these provisions, the temperature in the vessel 102 can be managed correctly to ensure that slurries of semisolid metal having satisfactory properties can be produced in a short time while assuring fairly consistent temperature management. The temperature in the vessel is optimally at  $70^\circ\text{C}$ ; to ensure that the temperature in the vessel is consistently managed at the optimal  $70^\circ\text{C}$ , adequate heat removal must be effected in the vessel cooling furnace 150; otherwise, the temperature in the vessel 102 becomes undesirably high. To deal with this problem, the vessel cooling furnace 150 is fitted with a blower 152 and a blow nozzle 152a such that a fast air flow is blown at room temperature to achieve forced cooling.

For system assessment on the management of the temperature in the vessel 102, a sheathed thermocouple was set up in the vessel and temperature data were taken under various conditions. Fig. 38 shows five different positions (A) - (E) of temperature measurement in the vessel 102, into which the 1.0- mm thick sheathed thermocouple was inserted.

Fig.39 shows the temperature history of cooling under condition I, i. e., the vessel temperature control section 140 was not divided into the vessel cooling furnace 150 and the vessel heat-retaining furnace 160 and a hot air flow having the target temperature of  $70^\circ\text{C}$  was circulated within the monolithic vessel temperature control section 140 at a velocity of about 5 m/sec. With this approach, the temperature in the vessel dropped to only about  $200^\circ\text{C}$  which was far from the target value.

Fig.40 shows the temperature history of cooling under condition II, i. e., a hot air flow having a temperature of  $70^\circ\text{C}$  was circulated at a higher velocity of about 30 m/sec. This approach was effective in further reducing the temperature in the vessel but not to the desired level of  $70^\circ\text{C}$ .

Fig.41 shows the temperature history of cooling under condition III, i. e., the vessel temperature control section 140 was divided into the vessel cooling furnace 150 and the vessel heat-retaining furnace 160, with an air flow at ordinary temperature being circulated within the cooling furnace 150 at a velocity of 30 m/sec whereas the atmosphere in the vessel heat-retaining furnace 160 had its temperature raised to  $70^\circ\text{C}$  by means of an electric heater. It was only with this system that the temperature in the vessel could be managed to be stable at the intended  $70^\circ\text{C}$ .

If, in the case of treating aluminum alloys at a large scale, the vessel 102 is made of ceramics having thermal conductivities of no more than  $1 \text{ kcal/m} \cdot \text{hr} \cdot ^\circ\text{C}$ , the time to cool the slurry of semisolid metal becomes impractically long. Therefore, in the second embodiment of the temperature management unit 104 which is adapted for handling comparatively large volumes of aluminum alloys such that the molten alloy is poured in an amount of 20 kg or more, the vessel 102 is made of SUS304 (see Fig.43) rather than the ceramics which are used with the first embodiment shown in Fig.37 and which require a prolonged cooling time. The resulting differences between the first embodiment of the temperature management unit 104 (Fig.37) and the second embodiment are as follows.

In order to ensure smooth recovery of the slurry from the vessel 102, its inner surfaces have to be coated with a water-soluble (which is desirable for ensuring against gas evolution) spray of a lubricant and, to this end, a spray position (spray equipment) is provided between the vessel cooling furnace 150 and the vessel heat-retaining furnace 160. Accordingly, the vessel 102 emerging from the vessel cooling furnace 150 must be kept at a sufficient temperature ( $200^\circ\text{C}$ ) to allow for the deposition of the spray solution; to meet this requirement, hot air at  $200^\circ\text{C}$  is applied against the vessel through a blow nozzle. As the result of the application of the water-soluble spray, the vessel 102 experiences a local temperature drop. In order to ensure that the vessel 102 has a uniform temperature of  $200^\circ\text{C}$  throughout, a hot air flow at  $200^\circ\text{C}$  is circulated within the vessel heat-retaining furnace 160 while it is agitated by a rotating fan to ensure uniformity in the temperature of the vessel 102.

The vessel 102 which is made of SUS304 allows thermal diffusion through it, so even if the semisolid metal cooling furnace 120 is of the design shown in Fig.42, no sharp border line can be drawn between the high-temperature range of the vessel (consisting of its top and bottom portions) and the low-temperature range (the middle portion of the vessel). To deal with this problem, a preheating furnace 190 is provided as accessory equipment on a lateral side of the semisolid metal cooling furnace 120 and, as shown in Fig.44, a lid 102a made of a ceramic material ( $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$  composite) and a plinth 102b are used to heat-retain the top and bottom of the vessel 102 while it is heated in the preheating furnace 190 before it is charged into the semisolid metal cooling furnace 120.

The interior of the semisolid metal cooling furnace 120 is supplied with hot air from the hot air generating furnace via two sets of blow nozzles 124, one being in the upper position and the other in the lower position. The supplied hot air is circulated within the cooling furnace 120 with its temperature and velocity being  $220^\circ\text{C}$  and  $5\text{ m/sec}$  at the entrance and  $180^\circ\text{C}$  and  $20\text{ m/sec}$  at the exit, whereby the semisolid metal is cooled comparatively slowly in the initial cooling period but cooled rapidly in the latter period.

Thus, the present invention provides a method of temperature management in which the step of managing the temperature in the vessel 102 at an appropriate level before it is supplied with the molten metal is distinctly separated from the step of managing the temperature in the vessel 102 in such a way that the as poured molten metal can be cooled at a desired appropriate rate; the invention also provides the apparatus for temperature management 104 which is capable of automatic performance of these steps in an efficient and continuous manner. Also proposed by the invention is a system configuration that implements the respective steps by means of the vessel temperature control section 140 and the semisolid metal cooling section 110.

In a specific embodiment, the vessel temperature control section 140 is composed of the vessel cooling furnace 150 capable of forced cooling with a circulating hot air flow that provides an appropriate cooling capacity by controlling the temperature and velocity of the air passing through the furnace and the vessel heat-retaining furnace 160 which controls the temperature of the atmosphere to lie at the target value in the vessel 102 and which maintains the vessel 102 at said temperature of the atmosphere. It should be noted here that the temperature to which the vessel cooling furnace 150 and the vessel heat-retaining furnace 160 should be controlled differs between aluminum and magnesium alloys. In the case of aluminum alloys, the interior of the vessel cooling furnace 150 is controlled to lie between room temperature and  $300^\circ\text{C}$  whereas the interior of the vessel heat-retaining furnace 160 is controlled to lie between  $50^\circ\text{C}$  and  $350^\circ\text{C}$ ; in the case of magnesium alloys, the interior of the vessel cooling furnace 150 is controlled to lie between room temperature and  $350^\circ\text{C}$  whereas the interior of the vessel heat-retaining furnace 160 is controlled to lie between  $200^\circ\text{C}$  and  $450^\circ\text{C}$ .

The semisolid metal cooling section 110 is composed of the semisolid metal cooling furnace 120 which is adapted to circulate hot air at an appropriate temperature such as to accomplish cooling within the shortest possible time that produces the slurry of semisolid metal with satisfactory properties and the semisolid metal slowly cooling furnace 130 which is designed to maintain the slurry of semisolid metal for 2 - 5 minutes in a temperature range appropriate for shaping such as to be adaptive for the specific molding cycle on the molding machine 200. Again, the temperature to which the semisolid metal cooling furnace 120 should be controlled differs between aluminum and magnesium alloys. In the case of aluminum alloys, the temperature should be controlled to lie between  $150^\circ\text{C}$  and  $350^\circ\text{C}$  and in the case of magnesium alloys, the temperature should be controlled to lie between  $200^\circ\text{C}$  and  $450^\circ\text{C}$ . On the other hand, the interior of the semisolid metal slowly cooling furnace 130 should be controlled to be at  $500^\circ\text{C}$  and above in both cases.

If the injection sleeve 202 on the molding machine 200 is ready to accept the molten metal just at time when the vessel 102 holding the metal has left the semisolid metal cooling furnace 120, the metal is immediately fed (poured) into the molding machine 200 without being directed into the semisolid metal slowly cooling furnace 130. Conversely, if the injection sleeve 202 is not ready to accept the molten metal since the molding machine 200 is operating, the vessel 102 leaving the semisolid metal cooling furnace 120 is transferred to the semisolid metal slowly cooling furnace 130.

As shown in Figs.37 and 42, the semisolid metal cooling furnace 120 has the vessel 102 carried on the conveyor 170 via a heat insulating plate 120c and the inner surfaces on the sidewall of the furnace 120 is partitioned by an upper and a lower heat insulating plate 120b in the middle portion of its height, with hot air (set at an appropriate temperature of  $120^\circ\text{C}$ ) being circulated through the partitioned area to establish a low-temperature region; at the same time, the inner surfaces of both top and bottom portions of the furnace 120 are heated with electric heaters 120a (set at a temperature of  $500^\circ\text{C}$ ) to establish a high-temperature (ca.  $500^\circ\text{C}$ ) region, thereby ensuring that a uniform temperature is provided throughout the molten metal in the vessel 102.

A first version of the heating system in the semisolid metal cooling furnace 120 according to the invention is such that either the temperature or the velocity of the circulating hot air is controlled to vary appropriately with the lapse of time or, alternatively, both the temperature and the velocity of the hot air are controlled to vary simultaneously with the lapse of time.

The first specific embodiment of the heating system is as shown in Fig.47 and comprises a hot air line for supplying a hot air flow into the semisolid metal cooling furnace 120, an air line from which an air flow at ordinary temperature emerges to combine with the hot air to lower its temperature, a damper for controlling the quantity of the air flowing through the air line, and a damper opening controller.

The second specific embodiment of the heating system is as shown in Fig.48 and comprises a temperature sensor installed within the semisolid metal cooling furnace 120, a hot air line for supplying a hot air flow into the furnace, an air line that combines with the hot air line, an automatic damper installed on the air line, and a damper opening controller that performs feed back control on the damper opening on the basis of the data obtained by measurement with the temperature sensor. The opening of the automatic damper is controlled on the basis of the data for the temperature in the furnace and the hot air is mixed with an appropriate amount of air and fed into the furnace, whereby the temperature and the velocity of the circulating hot air are controlled such that the molten metal will be cooled at a desired rate.

#### Example 7

An example of the invention (as recited in claims 24 - 29) will now be described specifically with reference to accompanying Figs. 43 - 53, in which: Fig.50 is a plan view showing the general layout of molding equipment; Fig. 43 is a plan view of the temperature management unit (its first embodiment); Fig.51 is a longitudinal sectional view showing in detail the position of temperature measurement within the holding vessel; Fig. 52 is a graph showing the temperature history of cooling within the holding vessel; Fig. 44 is a longitudinal section A - A of Fig.43; Fig.46 is a plan view of the temperature management unit (its second embodiment) according to another example of the invention; Fig. 45 shows the temperature profiles in the vessel fitted with heat insulators as compared with the temperature profile in the absence of such heat insulators; Fig.47 shows schematically the composition of the temperature control unit (its first embodiment) for a semisolid metal cooling furnace; Fig.48 shows schematically the composition of the temperature control unit (its second embodiment) for a semisolid metal cooling furnace according to another example of the invention; Fig.49 is a longitudinal section of the semisolid metal cooling furnace according to the second embodiment in which it is equipped with a vessel rotating mechanism; and Fig.53 is a longitudinal section of the semisolid metal cooling furnace according to the third embodiment in which it is equipped with a vessel vibrating mechanism.

As shown in Fig.50, the molding equipment generally indicated by 104 consists of a melt holding furnace 10 for feeding the molten metal as a molding material, a molding machine 200 and a temperature management unit 100 for managing the temperature of the melt until it is fed to the molding machine 200.

As also shown in Fig.50, the temperature management unit generally indicated by 104 consists of a semisolid metal cooling section 110 and a vessel temperature control section 140; the semisolid metal cooling section 110 is composed of a semisolid metal cooling furnace 120 and a semisolid metal slowly cooling furnace 130 which are connected in a generally rectangular arrangement by means of a transport mechanism such as a conveyor 170 whereas the vessel temperature control section 140 is composed of a vessel cooling furnace 150 and a vessel heat-retaining vessel 160. The temperature management unit 100 is also equipped with a robot 180 which grips the vessel 102 and transports it to one of the specified positions A - F (to be described below). The vessel 102 moves in the direction of arrows.

In the first embodiment of the temperature management unit 104, the preheating furnace 190 is provided near and parallel to the semisolid metal cooling furnace as shown in Figs.43 and 44. The purpose of the preheating furnace 190 is to ensure that both the plinth 102b placed under the melt containing vessel 102 and the lid 102a placed on top of the vessel 102 are preliminarily heated to a higher temperature than the hot air to be passed through the semisolid metal cooling furnace 120 such that uniformity will be assured for the temperature of the melt within the vessel as it is cooled in the semisolid metal cooling furnace 120. To this end, both the lid 102a and the plinth 102b which are carried on the conveyor 170 will be heated by the hot air being injected through the blow nozzle 192 as they move together with the conveyor 170 (see Fig. 44).

The temperature management unit 104 is operated as follows. An empty vessel 102 is first located in the heating vessel pickup position A. The robot 180 then transfers the vessel 102 to the position B, where the vessel is charged with a prescribed amount of the molten metal from the melt holding furnace 10 (which holds the molten metal containing a large number of crystal nuclei). Thereafter, the robot 180 transports the vessel 102 to the filled vessel rest position C, where it is placed on the plinth 102b and has its top covered with the lid 102a (both the lid 102a and the plinth 102b are preliminarily heated with the preheater 190); subsequently, the vessel is cooled as it is carried by the conveyor 170 to pass through the semisolid metal cooling furnace 120 in a specified period of time. The vessel 102 leaving the furnace 120 reaches the slurry vessel rest position D, from which it is immediately transferred to the sleeve position E by the robot 180 if the injection sleeve 202 in the molding machine 200 is ready to accept the molten metal; at position E, the slurry of semisolid metal in the vessel is poured into the injection sleeve 202. If the injection sleeve 202 is not ready to accept the molten metal when the vessel 202 has reached the slurry vessel rest position D (i. e., if the molding machine is operating to perform pressure forming), the slurry of semisolid metal within the vessel will progressively solidify upon cooling while it is waiting for acceptance in position D, thereby making it impossible for all the slurry to be discharged from the vessel or the crystal nuclei in the slurry will disappear to cause deterioration in the quality of the shaped part. In order to avoid these problems, the vessel 102 is forwarded to the semisolid metal slowly cooling furnace 130, where it waits for the molding machine 200 to become completely ready for the acceptance of the molten metal while ensuring against its rapid cooling.

The vessel 102 from which the slurry of semisolid metal having satisfactory properties has been emptied into the injection sleeve 202 is then transferred to the empty vessel rest position F by means of the robot 180, carried by the conveyor 170 into the vessel cooling furnace 150, where it is cooled for a specified time, passed through the vessel heat-retaining furnace 160 as it is held at a suitable temperature, and is thereafter returned to the heating vessel pickup position A.

A specific embodiment of the temperature management unit 104 is shown in Fig.43. In this first embodiment, aluminum alloys are to be treated on a comparatively large scale with the molten metal being poured in an amount of at least 20 kg; the system configuration is such that the molding cycle on the molding machine 200 is about 150 seconds and the time of passage through the semisolid metal cooling furnace 120 and the vessel temperature control section 140 (i. e. consisting of the vessel cooling furnace 150 and the vessel heat-retaining furnace 160) is 600 seconds in total. If the total passage time is longer than 600 seconds, the overall equipment becomes impractically bulky and the volume of the slurry in process which results from machine troubles and which has to be discarded is increased and these are by no means preferred for the purpose of constructing commercial production facilities.

To satisfy these cycle conditions and yet to produce slurries of good properties, details of the system have been determined as follows. SUS304 was adopted as the constituent material of the vessel (in the case of a comparatively small-scale operation with the molten metal being poured in an amount of no more than 10 kg, materials of small thermal conductivity provide comparative ease in temperature management; however, in a large-scale operation like the case under discussion, the use of ceramics and other materials of small thermal conductivity as the constituent material of the vessel requires an unduly prolonged time to cool the slurry, resulting in the failure to satisfy the cycle time requirement set forth above).

In order to ensure smooth recovery of the slurry from the vessel 102, its inner surfaces had to be coated with a water-soluble (which is desirable for ensuring against gas evolution) spray of a lubricant and, to this end, a spray position was provided between the vessel cooling furnace 150 and the vessel heat-retaining furnace 160. The vessel 102 emerging from the vessel cooling furnace 150 had to be cooled within 5 minutes down to a temperature (200 °C - 250 °C) that would allow for effective deposition of the spray; to meet this requirement, hot air at 100 °C was applied against the vessel through a blow nozzle.

As the result of the application of the water-soluble spray, the vessel 102 experienced a local temperature drop. In order to ensure that the vessel 102 would have a uniform temperature of 180°C - 190 °C throughout to provide a uniform temperature profile through the slurry, the vessel 102 was heated in the vessel heat-retaining furnace 160 in which a hot air flow at 190 °C was circulated by means of a fan.

In order to provide a uniform temperature profile through the slurry in the vessel, preheating furnace 190 was installed as an accessory and the plinth 102b and lid 102a which were each made of a heat insulator ( $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$  composite) were heated at 350 °C before they were set up on the vessel 102; this arrangement allowed the vessel 102 to be inserted into the semisolid metal cooling furnace 120 together with the lid 102a and plinth 102b.

The interior of the semisolid metal cooling furnace 120 was equipped with two sets each of hot air generating furnaces and blow nozzles, through which hot air was supplied to circulate within the furnace 120, with its temperature and velocity being 220°C and 5 m/sec at the entrance and 180 °C and 20 m/sec at the exit, whereby the semisolid metal was cooled comparatively slowly in the initial cooling period but cooled rapidly in the latter period.

For management of the temperature in the vessel 102, a sheathed thermocouple was set in the vessel to take data on the temperature. Detailed discussion will follow based on the thus taken temperature data.

Fig.51 shows the position of temperature measurement in the vessel 102. As shown enlarged on the right-hand illustration, a hole was made in the outer surface of the sidewall of the vessel to a depth at one half the wall thickness and thermocouple was inserted into the hole and spotwelded.

Fig.52 shows the temperature history of cooling of the vessel 102. The vessel temperature control section 140 was divided into the vessel cooling furnace 150 and the vessel heat-retaining furnace 160 and, as already mentioned above, the vessel cooling furnace 150 was so adapted that "hot air at 100 °C was applied against the vessel through the blow nozzles" whereas the vessel heat-retaining vessel 160 was designed to "permit circulation of hot air at 190 °C."

The system under discussion requires that the " spray should be deposited" within a limited time period while "a uniform temperature (180°C - 190 °C) should be established throughout the vessel 102". To meet these requirements, the vessel temperature control section 140 was divided into the vessel cooling furnace 150 and the vessel heat-retaining furnace 160 and optimal temperature management was performed in each furnace.

The second embodiment of the temperature management unit 100 shown in Fig. 46 was chiefly intended for the treatment of magnesium alloys. As typically shown in Fig.49, the temperature management unit 100 comprises a plurality of linearly arranged housings 120A in a generally cubic shape, each being fitted with a top cover 120B that could be opened or closed by means of an air cylinder 120C. Hot air could be forced into the housings 120A. With the cover 120B open, the melt containing vessel 102 was placed on the plinth 102b at the bottom of each housing 120A and a lid 102a fixed to the inside surface of the cover 120B was fitted over the top of the vessel 102 so that it would ensure a heat insulating effect during the cooling of the vessel 102. The vessel was adapted for transfer into or out of the housing 120A by manipulation of the robot 180.

Thus, the semisolid metal cooling furnace 120 according to the first embodiment shown in Fig.44 is of a continuous type in which the vessel 102 is carried by the conveyor 170 while the furnace is operating and, in contrast, the semisolid metal cooling furnace 120 according to the second embodiment shown in Fig.46 is of a batch system.

As also shown in Fig.49, the plinth 102b seated on the bottom of the housing 120A is coupled to a rotational drive mechanism consisting of a motor 121a, a chain 121b, a sprocket 121c, a bearing 121d, etc. and this drive mechanism allows the vessel 102 to rotate freely during its cooling operation.

Another embodiment of the semisolid metal cooling furnace 120 is shown in Fig.53; it is fitted with not only a vibrator 121f that is actuated with an ultrasonic oscillator 121e but also a water-cooled booster 121g and this arrangement will provide effective vibrations to the vessel 102.

Fig.45 shows the temperature profiles obtained by fitting the top and bottom of the vessel with the lid 102a and the plinth 102b which were each made of a heat insulator ( $\text{Al}_2\text{O}_3 \cdot \text{SiO}_2$  composite). Obviously, the use of the heat insulator produced uniform temperature profiles as compared with the case of using no such heat insulators. The uniformity in temperature profile was further improved by preheating the insulator.

We next discuss the "high-viscosity region". The alloy to be treated in the case at issue is AC4C which has a eutectic temperature of  $577^\circ\text{C}$ . Within a narrow temperature range centered at this eutectic point, the fraction solid increases sharply from 56 % to 100 % and the viscosity will inturn rises noticeably. Hence, the region of 56 % to 100 % fraction solid may well be considered as the "high-density region". When no heat insulator was used, both the top and bottom portions of the vessel were entirely covered with the "high-density region" and in a case like this, the desired slurry would not form smoothly. In contrast, the mere use of the heat insulator resulted in a significant decrease in the "high-density region", which barely remained at the corners. Obviously, the "high-density region" totally disappeared when the heat insulator was heated. In the case under discussion, the heat insulator had to be heated but with smaller vessel sizes, there was no particular need to heat the heat insulator.

Magnesium alloys involve difficulty in temperature management since they have small latent heat and will cool rapidly. To deal with this problem, the semisolid metal cooling furnace 120 according to the second embodiment shown in Fig. 46 have the following differences from the first embodiment shown in Fig.43.

First, silicon nitride was used as the constituent material of the vessel but it was difficult to obtain a uniform temperature profile through the slurry in the vessel. Under the circumstances, the semisolid metal cooling furnace 120 for handling vessels having a diameter of more than 100 mm had to be equipped with a vessel rotating mechanism as indicated by 120X in Fig.49 or a vessel vibrator as indicated by 120Y in Fig.53. (With vessels having diameters ranging from 50 mm to less than 100 mm, neither the vessel rotating mechanism nor the vessel vibrator had to be installed. With vessel diameters of 100 mm - 200 mm, a vessel vibrator as indicated by 120Y in Fig. 53 was necessary and with vessel diameters of more than 200 mm, a vessel rotating mechanism capable of more vigorous agitation as indicated by 120X in Fig. 49 had to be employed.)

It was also necessary to perform the temperature management in such a manner as to be flexible with time; to meet this need, a furnace temperature controller as indicated by 120Z in Fig. 47 or 48 was installed. (With vessel diameters of less than 100 mm, the rate of cooling the slurry was so sensitive to the variations in the temperature within the furnace that it was necessary to control the temperature in the furnace by the mechanism shown in Fig.47. With vessel diameters of less than 70 mm, not only the furnace temperature controller but also a feedback control system as shown in Fig. 48 was necessary.)

In order to permit the addition of these capabilities, the semisolid metal cooling furnace 120 was designed as a batch system of the type shown in Fig.46 and the timing for the transfer of the vessel into and out of the furnace 120 was controlled by the robot 180.

Thus, the present invention provides a method of temperature management in which the step of managing the temperature in the vessel 102 at an appropriate level before it is supplied with the molten metal is distinctly separated from the step of managing the temperature in the vessel 102 in such a way that the as poured molten metal can be cooled at a desired appropriate rate; the invention also provides the apparatus for temperature management 104 which is capable of automatic performance of these steps in an efficient and continuous manner. Also proposed by the invention is a system configuration that implements the respective steps by means of the vessel temperature control section 140 and the semisolid metal cooling section 110.

In a specific embodiment, the vessel temperature control section 140 is composed of the vessel cooling furnace 150 capable of forced cooling with a circulating hot air flow that provides an appropriate cooling capacity by controlling the temperature and velocity of the air passing through the furnace and the vessel heat-retaining furnace 160 which controls the temperature of the atmosphere to lie at the target value in the vessel 102 and which maintains the vessel 102 at said temperature of the atmosphere. It should be noted here that the temperature to which the vessel cooling furnace 150 and the vessel heat-retaining furnace 160 should be controlled differs between aluminum and magnesium alloys. In the case of aluminum alloys, the interior of the vessel cooling furnace 150 is controlled to lie between room temperature and  $300^\circ\text{C}$  whereas the interior of the vessel heat-retaining furnace 160 is controlled to lie between  $50^\circ\text{C}$  and  $350^\circ\text{C}$ ; in the case of magnesium alloys, the interior of the vessel cooling furnace 150 is controlled to lie between

room temperature and 350°C whereas the interior of the vessel heat-retaining vessel 160 is controlled to lie between 200 °C and 450 °C.

The semisolid metal cooling section 110 is composed of the semisolid metal cooling furnace 120 which is adapted to circulate hot air at an appropriate temperature such as to accomplish cooling within the shortest possible time that produces the slurry of semisolid metal with satisfactory properties and the semisolid metal slowly cooling furnace 130 which is designed to maintain the slurry of semisolid metal for 2 - 5 minutes in a temperature range appropriate for shaping such as to be adaptive for the specific molding cycle on the molding machine 200. Again, the temperature to which the semisolid metal cooling furnace 120 should be controlled differs between aluminum and magnesium alloys. In the case of aluminum alloys, the temperature should be controlled to lie between 150 °C and 350 °C and in the case of magnesium alloys, the temperature should be controlled to lie between 200 °C and 450 °C. On the other hand, the interior of the semisolid metal slowly cooling furnace 130 should be controlled to be at 500 °C and above in both cases.

If the injection sleeve 202 on the molding machine 200 is ready to accept the molten metal just at the time when the vessel 102 holding the metal has left the semisolid metal cooling furnace 120, the metal is immediately fed (poured) into the molding machine 200 without being directed into the semisolid metal slowly cooling furnace 130. Conversely, if the injection sleeve 202 is not ready to accept the molten metal since the molding machine 200 is operating, the vessel 102 leaving the semisolid metal cooling furnace 120 is transferred to the semisolid metal annealing furnace 130.

A first version of the heating system in the semisolid metal cooling furnace 120 according to the invention is such that either the temperature or the velocity of the circulating hot air is controlled to vary appropriately with the lapse of time or, alternatively, both the temperature and the velocity of the hot air are controlled to vary simultaneously with the lapse of time.

The first specific embodiment of the heating system (furnace temperature control unit 120Z) is as shown in Fig.47 and comprises a hot air line for supplying a hot air flow into the semisolid metal cooling furnace 120, an air line from which an air flow at ordinary temperature emerges to combine with the hot air to lower its temperature, a damper for controlling the quantity of the air flowing through the air line, and a damper opening controller.

The second specific embodiment of the heating system (furnace temperature control unit 120Z) is as shown in Fig.48 and comprises a temperature sensor installed within the semisolid metal cooling furnace 120, a hot air line for supplying a hot air flow into the furnace, an air line that combines with the hot air line, an automatic damper installed on the air line, and a damper opening controller that performs feedback control on the damper opening on the basis of the data obtained by measurement with the temperature sensor. The opening of the automatic damper is controlled on the basis of the data for the temperature in the furnace and the hot air is mixed with an appropriate amount of air and fed into the furnace, whereby the temperature and the velocity of the circulating hot air are controlled such that the molten metal will be cooled at a desired rate.

#### Example 8

An example of the invention (as recited in claim 30) will now be described specifically with reference to accompanying drawings. The example was implemented by the same method as in Example 1, except that Fig.3 was replaced by Fig.54 and the top surface of the insulated vessel 30 (or 30A) was fitted with a heat insulating lid 42 (or a ceramics coated metallic lid 42A). Thus, Figs.1, 2, 54 and 4 - 7 concern Example 8, in which: Fig.1 is a diagram showing a process sequence for the semisolid forming of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit; Fig.2 is a diagram showing a process sequence for the semisolid forming of a magnesium or aluminum alloy having a composition within a maximum solubility limit; Fig. 54 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig.4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig.54; Fig.5 is an equilibrium phase diagram for an Al-Si alloy as a typical aluminum alloy system; Fig.6 is an equilibrium phase diagram for a Mg-Al alloy as a typical magnesium alloy system; Fig.7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig.8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped according to the prior art.

The insulated vessel 30 for holding the molten metal the temperature of which has dropped to just below the liquidus line shall have a heat insulating effect in order to ensure that the primary crystals generated will spheroidize and have the desired fraction liquid after the passage of a specified time. Problems, however, will occur in certain cases, such as where near-eutectic Al-Si alloys and others that are prone to form skins are to be held, or where the molten metal is so heavy that it has to be held in a semisolid condition for more than 10 minutes, or where the height to diameter ratio of the insulated vessel 30 exceeds 1:2. Although, there is no problem with the internal microstructure of the molten metal, a solidified layer is prone to grow on the surface of the melt and can potentially cover the top of the semisolid metal, thus, making it difficult to insert the metal into the injection sleeve 40. To deal with this situation, the top of the insulated vessel 30 is fitted with the heat insulating lid 42 in order to ensure against solidification from the surface of the molten metal which is being held within the insulated vessel 30, thereby enabling the metal to be cooled while providing uniformity in temperature throughout the metal.



The constituent material of the insulated vessel 30 and the heat-insulating lid 42 is in no way limited to metals and those which have a heat-retaining property and which yet wet with the melt only poorly are preferred. If a gas-permeable ceramic vessel is to be used as the insulated vessel 30 and the heat-insulating lid 42 for holding magnesium alloys which are easy to oxidize and burn, the exterior to the vessel is preferably filled with a specified atmosphere (e. g. an inert or vacuum atmosphere). For preventing oxidation, it is desired that Be or Ca is preliminarily added to the molten metal. The shape of the insulated vessel 30 and the heat-insulating lid 42 is by no means limited to a tubular or cylindrical form and any other shapes that are suitable for the subsequent forming process maybe adopted. The molten metal need not be poured into the insulated vessel 30 but it may optionally be charged directly into the ceramic injection sleeve 40.

Table 4 shows how the presence or absence of the heat insulating lid 42 affected the procedure of making shaped parts. Comparative Samples 19 - 22 refer to the case of holding the molten metal without the insulating lid. In Comparative Sample 19, the insulated vessel 30 held the melt of an alloy that was prone to form a skin and, hence, a solidified layer formed over the semisolid metal, making it impossible to recover the metal from the vessel 30. In Comparative Sample 20, it was attempted to have the semisolid metal inserted into the injection sleeve with the molding temperature lowered; in Comparative Sample 22, the metal was unduly heavy.

Hence, in both cases, the holding time was prolonged and the result was substantially the same as with Comparative Sample 1 shown in Table 1. In Comparative Sample 21, the height-to-diameter ratio of the insulated vessel 30 was greater than 1:2 and, hence, the temperature profile through the semisolid metal was so poor that the result was substantially the same as with Comparative Sample 1 shown in Table 1.

Invention Samples 23 - 26 refer to the case of using the insulated vessel 30 fitted with the heat-insulating lid 42; they showed better results than Comparative Samples 19 - 22 in the recovery of the semisolid metal.



Table 4

	No.	Alloy	Conditions of the semisolid metal to be shaped					Handl- ing of semi- solid metal	Remarks
			Metal weight (kg)	Diamter- to-height ratio of holding vessel	Insula- ting lid	Holding time (min)	Molding temper- ature (°C)	Tempera- ture pro- file just before shaping	
Compara- tive Sample	19	ADC12	2	1/2	Not used	5	571	×	Alloy was prone to form a skin.
	20	AC4CH	2	1/2	Not used	10	580	△	Long holding time
	21	AC4CH	2	1/4	Not used	5	585	△	Holding vessel had large diameter-to-height ratio.
	22	AC4CH	20	1/2	Not used	20	585	×	Heavy metal weight, long holding time
Inven- tion Sample	23	ADC12	2	1/2	Used	5	571	○	Alloy was prone to form a skin.
	24	AC4CH	2	1/2	Used	10	580	○	Long holding time
	25	AC4CH	2	1/4	Used	5	585	○	Holding vessel had large diameter-to-height ratio.
	26	AC4CH	20	1/2	Used	20	585	○	Heavy metal weight, long holding time

\* Cooling jig (30°C) was used to induce the generation of crystal nuclei.

\* Casting temperature was 20°C above the liquidus line.

\* ADC12 : Al-10.6%Si-1.8%Cu-0.8%Fe m.p. 577°C

\* AC4CH : Al-7%Si-0.35%Mg m.p. 615°C

\* Insulated ceramic vessel and lid were chiefly composed of special calcium silicate.

\* Temperature profile just before shaping : ○, uniform; △, slightly nonuniform; ×, nonuniform

\* Handling of semisolid metal: ○, easy; △, somewhat difficult; ×, difficult

## Example 9

An example of the invention (as recited in claim 31) will now be described with reference to accompanying Figs.3, 4 and 55 - 58, in which: Fig. 55 is a diagram showing a process sequence for the semisolid forming of a zinc alloy of a hypoeutectic composition; Fig.3 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig.4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig.3; Fig. 56 is an equilibrium phase diagram for a binary Zn-Al alloy as a typical zinc alloy system; Fig.57 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig.58 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs.55 and 56, the first step of the process according to the invention comprises:

- (1) holding the melt of a hypoeutectic zinc alloy superheated to less than 300°C above the liquidus temperature and contacting the melt with a surface of a jig at a lower temperature than its melting point so as to generate crystal nuclei; or alternatively,
- (2) holding the melt of a zinc alloy superheated to less than 100°C above the liquidus temperature.

The cooled molten alloy prepared in (1) is poured into an insulated vessel having a heat insulating effect and, in the case of (2), the melt is directly poured into the insulated vessel without being cooled with a jig. The melt is held within the insulated vessel for a period from 5 seconds to 60 minutes at a temperature not higher than the liquidus temperature but higher than the eutectic or solidus temperature, whereby a large number of fine spherical primary crystals are generated in the alloy, which is then shaped at a specified liquid fraction.

The term "a specified fraction liquid" means a relative proportion of the liquid phase which is suitable for pressure forming. In high-pressure casting operations such as die casting and squeeze casting, the fraction liquid ranges from 20 % to 90 %, preferably from 30 % to 70 %. If the fraction liquid is less than 30 %, the formability of the raw material is poor; above 70 %, the raw material is so soft that it is not only difficult to handle but also less likely to produce a homogeneous micro-structure. In extruding and forging operations, the fraction liquid ranges from 0.1 % to 70 %, preferably from 0.1 % to 50 %, beyond which an inhomogeneous structure can potentially occur.

The "insulated vessel" as used in the invention is a metallic or nonmetallic vessel, or a metallic vessel having a surface coated with a nonmetallic material or a semiconductor, or a metallic vessel compounded of a nonmetallic material or semiconductor, which vessels are adapted to be either heatable or coolable from either inside or outside.

The specific procedure of semisolid metal forming to be performed in Example 9 is essentially the same as described in Example 1.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in Fig.3, namely, the step of pouring the molten metal on to the cooling jig 20, the step of generating and spheroidizing primary crystals and the forming step are the same as set forth in Example 1. The criticality of the numerical limitations set forth in claims 2 and 9 is also the same as set forth in Example 1.

It should be noted here that zinc alloys are prone to form equiaxed crystals and, hence, provide comparative ease in producing fine spherical primary crystals without using the cooling jig 20. With such zinc alloys, the degree of superheating is adjusted to less than 100 °C above the liquidus line in order to ensure that the alloy poured into the insulated vessel 30 having a heat-insulating effect is rendered either liquid to have crystal nuclei or partially solid, partially liquid to have crystal nuclei at a temperature equal to or higher than the molding temperature. If the temperature of the melt as poured into the insulated vessel 30 is unduly high, the crystal nuclei once generated will dissolve again or coarse primary crystals will form and, in either case, it is impossible to produce the desired semisolid structure. In addition, so much time will be taken for the temperature of the melt to decrease to establish a specified fraction liquid that the operating efficiency becomes low. Another inconvenience is that the poured melt M is oxidized or burnt at the surface.

Table 5 shows the conditions of various samples of semisolid metal to be shaped, as well as the qualities of shaped parts. As shown in Fig. 3, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed, 1.0 m/s; mold temperature, 200 °C. The product shaped parts were flat plates 100 mm wide and 200 mm long, with the thickness varying at 2 mm, 5 mm and 10 mm in the longitudinal direction.

Table 5 (continued on next page)

		Conditions of the semisolid metal to be shaped						
	No.	Alloy Composition	Casting temperature (°C)	Cooling jig	Temperature of the cooling jig (°C)	Temperature of the metal within vessel (°C)	Holding time (min)	Fraction liquid just before shaping (%)
Invention Sample	1	Zn-2.5%Al	430	Used	36	397	6	60
	2	Zn-2.5%Al	429	Used	45	398	9	50
	3	Zn-2.5%Al	440	Used	48	398	12	40
	4	Zn-4%Al	425	Used	38	389	8	50
	5	Zn-2.5%Al	410	Not used	-	400	8	50
	6	Zn-4%Al	400	Not used	-	391	7	50
	7	Zn-2.5%Al	430	Not used	-	407	11	50
Comparative Sample	8	Zn-2.5%Al	680	Used	27	399	9	50
	9	Zn-2.5%Al	440	Used	410	408	10	50
	10	Zn-4%Al	700	Used	34	434	19	50
	11	Zn-2.5%Al	430	Used	37	398	65	15
	12	Zn-2.5%Al	430	Used	42	399	0.03	91
	13	Zn-2.5%Al	430	Used	35	398	1.33	50

Zn-2.5%Al m.p. 400°C

\*1 Dendritic primary crystals

Zn-4%Al m.p. 390°C

\*2 Spherical primary crystals plus dendrites

Segregations : ○, a few; ×, many

Amount of unspherical primary crystals : ○, small; ×, large

External appearance : ○, good; △, fair; ×, poor

Table 5 (continued)

	No.	Alloy Composition	Quality of shaped part				Remarks
			Internal segregation	Primary crystal size ( $\mu\text{m}$ )	Amount of unspherical primary crystal	External appearance	
Invention Sample	1	Zn-2.5%Al	○	135	○	○	
	2	Zn-2.5%Al	○	150	○	○	
	3	Zn-2.5%Al	○	160	○	○	
	4	Zn-4%Al	○	130	○	○	
	5	Zn-2.5%Al	○	190	○	○	
	6	Zn-4%Al	○	175	○	○	
Comparative Sample	7	Zn-2.5%Al	○	135	○	○	Vibrations (100Hz) were applied at amplitude of 0.1mm.
	8	Zn-2.5%Al	○	125	○	○	Water-cooled cooling jig was used.
	9	Zn-2.5%Al	×	410	×	△	High jig temperature
	10	Zn-4%Al	×	660	×	×	High casting temperature
	11	Zn-2.5%Al	○	320	○	×	Long holding time
	12	Zn-2.5%Al	×	*1		△	Short holding time, high fraction liquid
	13	Zn-2.5%Al	×	*2		△	Metallic (non-insulated) vessel was used at ordinary temperature.

In Comparative Sample 9, the temperature of jig 20 with which the melt M was contacted was so high that the number of crystal nuclei generated was insufficient to produce fine spherical primary crystals; instead, coarse unspherical primary crystals formed. In Comparative Sample 10, the casting temperature was so high that very few crystal nuclei remained within the ceramic vessel 30, yielding the same result as with Comparative Sample 9. In Comparative

Sample 11, the holding time was so long that the fraction liquid in the metal to be shaped was low, yielding a shaped part of poor appearance. In addition, the size of primary crystals was undesirably large. In Comparative Sample 12, the holding time within the ceramic vessel 30 was short whereas the fraction liquid in the metal to be shaped was high; hence, many segregations of components occurred within the shaped part as shown in Fig.58. With Comparative Sample 13, the insulated vessel 30 was a metallic container having a very small heat insulating effect, so the dendritic solidified layer forming on the inner surface of the vessel 30 would enter the spherical primary crystals generated in the central part of the vessel, yielding an inhomogeneous structure involving segregations.

In each of Invention Samples 1 - 8, a homogeneous microstructure comprising fine ( $< 200 \mu m$ ) spherical primary crystal was obtained to enable the production of a shaped part having good appearance.

#### Example 10

An example of the invention (as recited in claim 32) will now be described with reference to accompanying Figs.59 - 64, in which: Fig. 59 is a diagram showing a process sequence for the semisolid forming of a hypereutectic Al-Si alloy starting with the preparation of a semisolid metal and ending with the molding step; Fig.60 is a diagram showing a process flow starting with the generation of very fine primary Si crystals and ending with the molding step; Fig.61 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig.60; Fig.62 is an equilibrium phase diagram for a binary Al-Si alloy; Fig. 63 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig.64 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs.59 and 62, the process of the invention starts with superheating the melt of a hypereutectic Al-Si alloy to less than  $300^{\circ}\text{C}$  above the liquidus line. The thus superheated alloy is contacted with a jig at lower temperature than its melting point so as to generate crystal nuclei within the alloy solution; the alloy is then cooled in an insulated vessel until a specified fraction liquid is established, with it being held either at a temperature between the liquidus and eutectic temperatures or at the eutectic temperature for a period from 5 seconds to 60 minutes, thereby generating a large number of fine primary crystals. The hypereutectic Al-Si alloy permits only a small amount of primary crystals to be crystallized and, hence, it has high fraction liquid in a semisolid condition at temperatures exceeding the eutectic point. Therefore, if the desired fraction liquid is low, the alloy which has been heated to its eutectic temperature has to be held at that temperature for a sufficient time to allow for the progress of solidification (eutectic reaction).

According to the invention, semisolid metal forming will proceed by the following specific procedure. In step (1) of the process shown in Figs. 60 and 61, a complete liquid form of metal M is contained in a ladle 10. In step (2), the metal is cooled with a jig 20 to generate crystal nuclei and the melt is then poured into a ceramic vessel 30 (or ceramics-coated vessel 30A) having a heat insulating effect so as to produce an alloy having a large number of crystal nuclei which is of a composition just below the liquidus line. In subsequent step (3), the alloy is held partially molten within the insulated vessel 30 (or 30A). In the meantime, very-fine primary Si crystals result from the introduced crystal nuclei [step (3)-a] and grow into granules together with the surrounding primary  $\alpha$  as the fraction solid increases.

Metal M thus obtained at a specified fraction liquid maybe inserted into a die casting injection sleeve 40 [step (3)-b] and thereafter pressure formed within a mold cavity 50a in a die casting machine to produce a shaped part (step (4)).

The semisolid metal forming process of the invention shown in Figs. 59, 60 and 61 has obvious differences from the conventional thixocasting and rheocasting methods. In the invention method, the primary crystals that have been crystallized within a temperature range for the semisolid state are not ground into spherical grains by mechanical or electromagnetic agitation as in the prior art but the large number of primary crystals that have been crystallized and grown from the introduced crystal nuclei with the decreasing temperature in the range for the semisolid state and with the lapse of the time of holding at the eutectic point are continuously rendered granular by the heat of the alloy itself (which may optionally be supplied with external heat and held at a desired temperature). In addition, the semisolid metal forming method of the invention is very convenient since it does not involve the step of partially melting billets by reheating in the thixocasting process.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in Fig.59, namely, the step of pouring the molten metal on to the cooling jig 20 and the step of generating and spheroidizing primary crystals, are set forth below more specifically. Also discussed below is the criticality of the numerical limitations set forth in claim 32.

If the casting temperature is at least  $300^{\circ}\text{C}$  higher than the melting point or if the surface temperature of jig 20 is not lower than the melting point, the following phenomena will occur:

- (1) only a few crystal nuclei are generated;
- (2) the temperature of the melt M as poured into the insulated vessel having a heat insulating effect is higher than the liquidus temperature and, hence, the proportion of the remaining crystal nuclei is low enough to produce large primary crystals.

To avoid these problems, the casting temperature to be employed in the invention is controlled to be such that the degree of superheating above the liquidus line is less than 300 °C whereas the surface temperature of jig 20 is controlled to be lower than the melting point of alloy M. Primary crystals of an even finer size can be produced by ensuring that the degree of superheating above the liquidus line is less than 100 °C and by adjusting the surface temperature of jig 20 to be at least 50 °C lower than the melting point of alloy M. It should, however, be noted that in the presence of P as a refiner of primary Si crystals, the molten metal should be superheated to at least 30 °C above the liquidus line; if the temperature of the melt is unduly low, the grains of AlP serving as a refiner will agglomerate to become no longer effective.

In order to ensure that the alloy solution at a specified fraction liquid will form a modified eutectic structure after solidification, thereby providing satisfactory mechanical properties, either Sr or Na or both are added. If the P addition is less than 0.005 %, it is not very effective in refining the primary Si crystals; the effect of P is saturated at 0.03 % and no further improvement is expected beyond 0.03 %. Hence, the P addition is controlled to lie between 0.005 % and 0.03 %. If the Sr addition is less than 0.005 %, it is not very effective in modifying the eutectic Si structures; beyond 0.03 %, an Al-Si-Sr compound will crystalize out to cause deterioration in the mechanical properties of the alloy. Hence, the Sr addition is controlled to lie between 0.005 % and 0.03%. If the Na addition is less than 0.001 %, it is not very effective in modifying the eutectic Si structures; beyond 0.01 %, coarse eutectic Si grains will form. Hence, the Na addition is controlled to lie between 0.001 % and 0.01 %.

Table 6 sets forth the conditions for the preparation of semisolid metal samples and the results of evaluation of their metallographic structures by microscopic examination.

Table 6 (continued on next page)

	No.	Alloy composition				Casting temperature (°C)	Cooling jig	Temperature of the cooling jig (°C)	Temperature of the metal within vessel (°C)	Holding time (min)
		Si (%)	Additive							
			P	Sr	Na					
Invention Sample	1	20	No	No	No	750	Used	35	678	7
	2	20	Yes	No	No	750	Used	35	680	7
	3	20	Yes	Yes	No	750	Used	50	683	7
	4	20	Yes	No	Yes	750	Used	40	678	7
	5	20	Yes	Yes	No	730	Used	35	685	10
	6	20	Yes	Yes	No	850	Used	30	682	7
Comparative Sample	7	20	Yes	Yes	No	750	Used	650	715	16
	8	15	Yes	No	No	950	Used	35	730	19
	9	20	Yes	No	Yes	750	Used	40	678	70
	10	20	Yes	No	Yes	750	Used	40	681	0.03
	11	20	Yes	Yes	No	750	Not used	-	710	-

Al-20%Si m.p. 692°C      Al-15%Si m.p. 620°C  
 Segregations: ○, a few; ×, many

Table 6 (continued)

	No.	Alloy composition Additive				Inter-nal segre-gation	Average size of primary crystals ( $\mu\text{m}$ )	Remarks
		Si (%)	P	Sr	Na			
Inven-tion Sample	1	20	No	No	No	O	140	
	2	20	Yes	No	No	O	40	
	3	20	Yes	Yes	No	O	55	
	4	20	Yes	No	Yes	O	60	
	5	20	Yes	Yes	No	O	40	Vibrations (100Hz) were applied at amplitude of 0.1mm.
	6	20	Yes	Yes	No	O	60	Water-cooled cooling jig was used.
Compara-tive Sample	7	20	Yes	Yes	No	X	250	High jig temperature
	8	15	Yes	No	No	X	200	High casting temperature
	9	20	Yes	No	Yes	O	400	Long holding time, low fraction liquid
	10	20	Yes	No	Yes	X	60	Short holding time, high fraction liquid
	11	20	Yes	Yes	No	X	210	Conventional gravity casting was performed.

In Comparative Sample 7, the temperature of jig 20 with which the melt M was contacted was so high that the number of crystal nuclei generated was insufficient to produce fine primary crystals; instead, coarse primary crystals formed. In Comparative Sample 8, the casting temperature was so high that very few crystal nuclei remained within the ceramic vessel 30, yielding the same result as with Comparative Sample 7. In Comparative Sample 9, the holding time



was so long that the fraction liquid in the metal to be shaped was low, making the alloy unsuitable for shaping. In addition, the size of primary crystals was undesirably large. In Comparative Sample 10, the holding time within the ceramic vessel 30 was short whereas the fraction liquid in the metal to be shaped was high; hence, many segregations of components occurred within the shaped part. In Comparative Sample 11, solidification occurred within the insulated vessel and many coarse primary crystals were generated in the form of a rectangular rod (see Fig. 64).

In each of Invention Samples 1 - 6, there was obtained a homogeneous microstructure having fine (< ca. 150 $\mu$ m) granular primary crystals that were adapted for pressure forming.

#### Example 11

An example of the invention (as recited in claim 33) will now be described in detail with reference to Figs. 1, 3, 4 and 65 - 67, in which: Fig. 1 is a diagram showing a process sequence for the semisolid forming of an Al-Mg alloy; Fig. 3 shows a process flow starting with the generation of granular primary crystals and ending with the molding step; Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 3; Fig. 65 is an equilibrium phase diagram for a binary Al-Mg alloy; Fig. 66 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig. 67 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs. 1 and 65, the invention recited in claim 33 is such that:

- (1) the melt of an Al-Mg alloy held superheated to less than 300°C above the liquidus line is contacted with a jig at a lower temperature than its melting point, thereby generating crystal nuclei in the alloy solution, and the molten metal is poured into an insulated vessel having a heat insulating effect; or
- (2) the melt of an Al-Mg alloy that contains an element to promote the generation of crystal nuclei and that is held superheated to less than 100°C above the liquidus temperature is directly poured into the insulated vessel without cooling the melt with a jig.

The poured metal is held within the insulated vessel at a temperature not higher than the liquidus temperature but higher than the eutectic or solidus temperature for a period from 5 seconds to 60 minutes until a specified liquid fraction is established, whereby a large number of fine granular primary crystals are generated to produce a semisolid Al-Mg alloy at the specified fraction liquid.

The specific procedure of semisolid metal forming to be performed in Example 11 is essentially the same as described in Example 1.

Silicon (Si) is added in order to promote the spheroidization of the generated granular primary crystals. If the Si addition is less than 0.3 %, the intended effect in promoting the spheroidization is not expected; adding more than 2.5 % of Si will merely result in deteriorated properties of the alloy and no further improvement in spheroidization is expected. Hence, the Si addition is controlled to lie between 0.3 % and 2.5 %.

It should be noted that the Al-Mg alloy of the invention may incorporate up to 1 % of Mn or up to 0.5 % of Cu with a view to improving its strength.

Table 7 sets forth the conditions for the preparation of semisolid metal samples and the results of evaluation of their metallographic structures by microscopic examination.

Table 7 (continued on next page)

	No.	Alloy composition	Casting temperature (°C)	Cooling jig	Temperature of the cooling jig (°C)	Temperature of the metal within vessel (°C)	Holding time (min)
Invention Sample	1	Al-5%Mg	660	Used	35	634	4
	2	Al-5%Mg	660	Used	45	635	4
	3	Al-5%Mg-2.5%Si	650	Used	35	624	4
	4	Al-10%Mg	630	Used	45	605	4
	5	Al-5%Mg	640	Not used	-	625	4
	6	Al-10%Mg	610	Not used	-	597	3
	7	Al-5%Mg	660	Used	30	635	4
	8	Al-5%Mg	660	Used	27	633	4
Comparative Sample	9	Al-5%Mg	660	Used	650	640	8
	10	Al-10%Mg	950	Used	35	675	14
	11	Al-5%Mg	660	Used	40	635	70
	12	Al-5%Mg	660	Used	40	635	0.03
	13	Al-5%Mg	680	Not used	-	650	-

Al-5%Mg m.p. 631°C

Al-10%Mg m.p. 602°C

\*1 Dendritic primary crystals

\*2 Granular primary crystals plus dendrites

Internal segregations: O, a few; X, many

Table 7 (continued)

	No.	Alloy composition	Internal segregation	Average size of primary crystals ( $\mu\text{m}$ )	Remarks
Invention Sample	1	Al-5%Mg	○	105	
	2	Al-5%Mg	○	75	With the addition of 0.015%Ti and 0.003%B
	3	Al-5%Mg-2.5%Si	○	80	With the addition of 0.015%Ti and 0.003%B; m.p. 626°C
	4	Al-10%Mg	○	95	
	5	Al-5%Mg	○	100	With the addition of 0.1%Ti and 0.01%B
	6	Al-10%M	○	95	With the addition of 0.1%Ti and 0.01%B
	7	Al-5%Mg	○	105	Vibrations (100Hz) were applied at amplitude of 0.1mm.
	8	Al-5%Mg	○	80	Water-cooled cooling jig was used.
Comparative Sample	9	Al-5%Mg	×	450	High jig temperature
	10	Al-10%M	×	500	High casting temperature
	11	Al-5%Mg	○	320	Long holding time
	12	Al-5%Mg	×	70	Short holding time, high fraction liquid
	13	Al-5%Mg	×	500	Metallic (non-insulated) vessel was used at ordinary temperature.

In Comparative Sample 9, the temperature of jig 20 with which the melt M was contacted was so high that the number of crystal nuclei generated was insufficient to produce fine primary crystals; instead, coarse primary crystals formed. In Comparative Sample 10, the casting temperature was so high that very few crystal nuclei remained within

the ceramic vessel 30, yielding the same result as with Comparative Sample 9. In Comparative Sample 11, the holding time was so long that the fraction liquid in the metal to be shaped was low, making the alloy unsuitable for shaping. In addition, the size of primary crystals was undesirably large. In Comparative Sample 12, the holding time within the ceramic vessel 30 was short whereas the fraction liquid in the metal to be shaped was high; hence, only coarse primary crystals formed. In addition, the high fraction liquid caused many segregations of components within the shaped part. In Comparative Sample 13, the hot molten metal was directly poured into the insulated vessel, where it was solidified as such, yielding coarse, dendritic primary crystals (see Fig. 67).

In each of Invention Sample 1 - 8, there was obtained a homogeneous microstructure having fine ( $< \text{ca. } 100 \mu\text{m}$ ) granular primary crystals that were adapted for pressure forming.

#### Example 12

An example of the invention (as recited in claims 34 - 35) will now be described in detail with reference to accompanying Figs. 1, 2, 68 and 4 - 8, in which: Fig. 1 is a diagram showing a process for the semisolid forming of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit; Fig. 2 is a diagram showing a process sequence for the semisolid forming of a magnesium or aluminum alloy having a composition within a maximum solubility limit; Fig. 68 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig. 4 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig. 68; Fig. 5 is an equilibrium phase diagram for an Al-Si alloy as a typical aluminum alloy system; Fig. 6 is an equilibrium phase diagram for a Mg-Al alloy as a typical magnesium alloy system; Fig. 7 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig. 8 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

As shown in Figs. 1, 2, 5 and 6, the invention recited in claims 34 and 35 comprises the following: the melt of a hypoeutectic aluminum alloy having a composition at or above a maximum solubility limit or the melt of a magnesium or aluminum alloy having a composition within a maximum solubility limit is held superheated to less than  $300^\circ\text{C}$  above the liquidus temperature; either melt is contacted with a surface of a jig at a lower temperature than its melting point, thereby generating crystal nuclei in the alloy solution; the melt is then poured into an insulated vessel having a heat insulating effect, in which vessel the melt is held at a temperature not higher than the liquidus line but higher than the eutectic or solidus temperature for a period from 5 seconds to 60 minutes, whereby a large number of fine spherical primary crystals are generated in the melt, which is subsequently shaped at a specified fraction liquid.

The "specified fraction liquid" ranges from 0.1 % to 70 %, preferably from 10 % to 70 %.

The term "insulated vessel" as used herein refers to either a metallic or nonmetallic vessel or a metallic vessel either composited or coated with a nonmetallic material, which vessels are adapted to be heatable or coolable from either inside or outside.

According to the invention, semisolid metal forming will proceed by the following specific procedure. In step (1) of the process shown in Figs. 68 and 4, a complete liquid form of metal M is contained in a ladle 10. In step (2), the metal is cooled with a jig 20 to generate crystal nuclei from the low-temperature melt (which may optionally contain an element that is added to promote the generation of crystal nuclei) and the metal is then poured into a ceramic vessel 30 having a heat insulating effect, thereby producing an alloy of a composition just below the liquidus line which has a large number of crystal nuclei. In subsequent step (3), the alloy is held partially molten within the insulated vessel 30 (or 30A). In the meantime, fine granular (nondendritic) primary crystals result from the introduced crystal nuclei [step (3)-a] and grow into spherical primary crystals as the fraction solid increases with the decreasing temperature of the melt [steps (3)-b and (3)-c]. Metal M thus obtained which has a specified fraction liquid is inserted into container 82 on an extruding machine 80 and extruded through a die 84 by pushing with a stem 86 under high pressure, yielding a shaped part P.

After the generation of the crystal nuclei, the semisolid metal M in the insulated vessel 30 maybe inserted into the container 82 on the extruding machine 80 by accommodating it into the container 82 in such a way that the part of it which faces the bottom of the insulated vessel 30 and which has a comparatively small portion of the impurities is directed toward the die 84; upon extrusion through the die, one can obtain a shaped part of high quality which has only a small impurity content. Alternatively, the surface (top surface) of the semisolid metal M may be freed of the oxide before it is recovered from the insulated vessel 30 and the thus cleaned semisolid metal is charged into the container 82 on the extruding machine 80.

The semisolid metal forming process of the invention shown in Figs. 1, 2, 68 and 4 have obvious differences from the conventional thixocasting and rheocasting methods.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in Fig. 68, namely, the step of pouring the molten metal on to the cooling jig 20, the step of generating and spheroidizing primary crystals and the forming step are the same as set forth in Example 1.

Table 8 sets forth the conditions for the preparation of semisolid metal samples and the qualities of shaped parts. As Fig. 68 shows, the forming step consisted of inserting the semisolid metal into the container and extruding the same.

The extruding conditions were as follows: extruding machine, 800 t; extruding rate, 80 m/min; billet diameter, 75 mm; extrusion ratio, 20.

In Comparative Sample 1, the temperature of jig 20 with which the melt M was contacted was so high that the number of crystal nuclei generated was insufficient to produce fine spherical primary crystals; instead, coarse unspherical primary crystals formed as shown in Fig. 7.

In Comparative Sample 2, the casting temperature was so high that very few crystal nuclei remained within the ceramic vessel 30, yielding the same result as with Comparative Sample 1.

In Comparative Sample 3, the holding time was so long that the fraction liquid in the metal to be shaped was low, yielding a shaped part of poor appearance. In addition, the size of primary crystals was undesirably large.

In Comparative Sample 4, the holding time within the ceramic vessel 30 was short whereas the fraction liquid in the metal to be shaped was high; hence, only dendritic primary crystals formed. In addition, the high fraction liquid caused many segregations of components within the shaped part.

With Comparative Sample 5 the insulated vessel 30 was a metallic container having a small heat insulating effect, so the dendritic solidified layer forming on the inner surface of the vessel 30 would enter the spherical primary crystals generated in the central part of the vessel, yielding an inhomogeneous structure involving segregations.

Table 8 (continued on next page)

	No.	Alloy	Conditions of the semisolid metal to be shaped						
			Casting temperature (°C)	Cooling jig	Temperature of the cooling jig (°C)	Temperature of the metal within vessel (°C)	Holding time (min)	Fraction of liquid just before shaping (%)	Primary crystal size (μm)
Comparative Sample	1	AC4CH	625	Used	622	615	5	60	260
	2	AC4CH	950	Used	30	728	20	60	440
	3	AC4CH	680	Used	30	621	65	15	180
	4	AC4CH-0.15%Ti-0.005%B	630	Used	30	615	0.04	95	*1
	5	AC4CH	630	Used	30	608	2	60	*2
	6	AC4CH-0.15%Ti-0.005%B	630	Used	30	613	1	92	*2
	7	AC4CH	630	Not used	-	622	5	60	270
Invention Sample	8	AC4CH-0.15%Ti-0.005%B	630	Used	30	611	6.5	55	58
	9	AC4CH	630	Used	30	608	12	45	72
	10	AC4CH-0.15%Ti-0.005%B	630	Used	400	612	5.5	60	90
	11	AC4CH-0.15%Ti-0.010%B	850	Used	25	611	6	60	70
	12	AC4CH-0.15%Ti-0.015%B	630	Not Used	-	620	15	35	110
	13	AC7A	660	Used	30	631	5.7	50	75
	14	7075	650	Used	30	619	1.5	80	85
	15	AZ91	620	Used	30	588	4.2	55	78
	16	AZ91-0.4%Si-0.01%Sr	620	Used	30	588	4.3	55	78
	17	AZ91-0.15%Ca	620	Not used	30	592	4.5	55	118
	18	AC4CH-0.15%Ti-0.015%B	630	Not used	-	620	5	60	98

· AC4CH: Al-7%Si-0.35%Mg m.p. 620°C  
 · 7075: Al-4.5%Zn-1.1%Mg m.p. 640°C

\*1 Dendritic primary crystals

\*2 Spherical primary crystals (with dendritic primary crystals)

\*3 Temperature (°C) of the metal as poured into the vessel from the cooling plate

Segregations: ○, a few; ×, many

Amount of unspherical primary crystals: ○, small; ×, large

Eutectic size: ○, fine; ×, coarse

· AZ91: Mg-9%Al-0.7%Zn m.p. 595°C  
 · AC7A: Al-5%Mg-0.4%Mn m.p. 635°C

Table 8 (continued)

	No.	Alloy	Quality of shaped part			Remarks
			Inter- nal segre- gation	Amount of unspherical primary crystal	Eutec- tic size	
Comparative Sample	1	AC4CH	x	x	○	High jig temperature
	2	AC4CH	x	x	○	High casting temperature
	3	AC4CH	○	○	x	Long holding time
	4	AC4CH-0.15%Ti-0.005%B	x	*1	○	Short holding time, high fraction liquid
	5	AC4CH	x	*2	○	Metallic vessel was used at ordinary temperature
Inven- tion Sample	6	AC4CH-0.15%Ti-0.005%B	x	*2	○	Short holding time, high fraction liquid
	7	AC4CH	x	x	○	No grain refiner was used.
	8	AC4CH-0.15%Ti-0.005%B	○	○	○	
	9	AC4CH	○	○	○	Metallic vessel was used at 580°C.
	10	AC4CH-0.15%Ti-0.005%B	○	○	○	
	11	AC4CH-0.15%Ti-0.010%B	○	○	○	Water-cooled cooling jig was used.
	12	AC4CH-0.15%Ti-0.015%B	○	○	○	No jig was used.
	13	AC7A	○	○	○	
	14	7075	○	○	○	
	15	AZ91	○	○	○	
	16	AZ91-0.4%Si-0.01%Sr	○	○	○	
	17	AZ91-0.15%Ca	○	○	○	No jig was used.
	18	AC4CH-0.15%Ti-0.015%B	○	○	○	Vibrations (100Hz) were applied at amplitude of 0.1mm.

In Comparative Sample 6, the fraction liquid in the metal to be shaped was so high that result was the same as with Comparative Sample 4.

With Comparative Sample 7, the jig 20 was not used; the starting alloy did not contain any grain refiners, so the number of crystal nuclei generated was small enough to yield the same result as with Comparative Sample 1.

In each of invention Samples 8 - 18, a homogeneous microstructure comprising fine ( $< 150 \mu\text{m}$ ) spherical primary crystals was obtained to enable the production of a shaped part having good appearance.

### Example 13

An example of the invention (as recited in claims 36 and 37) will now be described in detail with reference to accompanying Figs.69 - 73, in which Fig. 69 shows two process sequences for the semisolid forming of a hypoeutectic aluminum alloy; Fig.70 shows a process flow starting with the generation of spherical primary crystals and ending with the molding step; Fig.71 shows diagrammatically the metallographic structures obtained in the respective steps shown in Fig.70; Fig.72 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the invention; and Fig.73 is a diagrammatic representation of a micrograph showing the metallographic structure of a shaped part according to the prior art.

The invention concerns a process which starts with either one of the following steps:

- (1) two or more liquid alloys having different melting points that are held superheated to less than  $50^{\circ}\text{C}$  above the liquidus temperature are mixed either directly within an insulated vessel having a heat insulating effect or along a trough in a channel into the insulated vessel, thereby generating crystal nuclei in the alloy solution (see Fig.69); or
- (2) two or more metals to be mixed are preliminarily contacted with respective cooling plates so as to generate crystal nuclei and the metals that have attained temperatures just above or below the liquidus temperature are mixed either directly within an insulated vessel having a heat insulating effect or along a trough in a channel into the insulated vessel, thereby generating more crystal nuclei (see Fig.70).

Either of the metals thus obtained is held within the insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to a molding temperature where a specified fraction liquid is established, whereby the fine grains that have formed within the alloy solution are crystallized out as no dendrites, and the metal is then fed into a mold, where it is subjected to pressure forming.

The "specified fraction liquid" and the "insulated vessel" have the same meanings as defined in Example 1.

According to the invention, semisolid metal forming will proceed by the following specific procedure. In step (1) of the process shown in Figs.70 and 71, two complete liquid forms of metals MA and MB are contained in ladles 10 and poured into a ceramic container 30 (or ceramic-coated metal container 30A) which is an insulated vessel having a heat insulating effect. As a result, an alloy having a large number of crystal nuclei is obtained at a temperature either just below or above the liquidus line. Molten metals MA and MB may be poured either simultaneously or successively with one coming after the other. Alternatively, molten metals MA and MB may be poured into partitioned compartments in the insulated vessel 30 and the partition is removed all of a sudden so as to achieve mutual contact between the two metals. If desired, either molten metal MA or MB or both may be preliminarily contacted with a cooling jig 20 so as to have a number of crystal nuclei generated in the metal or metals and this is effective for the purpose of producing a large number of crystals [step (1A) in Fig.70].

In subsequent step (2), the alloy mixture MC is held partially molten within the insulated vessel 30. In the meantime, extremely fine primary crystals result from the introduced crystal nuclei [step (2)-a] and grow into spherical primary crystals as the fraction solid increases with the decreasing temperature of the alloy mixture MC [steps (2)-b and (2)-c]. Alloy mixture MC thus obtained at a specified fraction liquid is inserted into an injection sleeve 40 [step (2)-d] and, thereafter, pressure formed within a mold cavity 50a on a die casting machine to produce a shaped part [step (3)].

The semisolid metal forming process of the invention shown in Figs.69, 70 and 71 has obvious differences from the conventional thixocasting and rheocasting methods.

The casting, spheroidizing and molding conditions that are respectively set for the steps shown in Fig.69, namely, the step of pouring the molten metal on to the cooling jig 20, the step of generating and spheroidizing primary crystals and the forming step, are set forth below. Also discussed below is the criticality of the numerical limitations set forth in claims 36 and 37.

If the molten (liquid) metals MA and MB to be mixed have been superheated to more than  $50^{\circ}\text{C}$  above the liquidus temperature, the temperature of either metal just after the mixing will neither be just above or below the liquidus temperature of the alloy mixture MC to be eventually formed. If the mixed metals are held within the insulated vessel 30, a microstructure consisting of coarse dendrites will form rather than a structure of uniform, near-spherical nondendritic crystals. To avoid these problems, the temperatures of, molten (liquid) metals MA and MB to be mixed need be superheated to no more than  $50^{\circ}\text{C}$  above the liquidus temperature. The "temperature either just above or below the liquidus temperature of the metal mixture to be eventually formed" means a temperature within the liquidus temperature  $\pm 15^{\circ}\text{C}$ . The liquid metals to be mixed shall include alloys. The insulated vessel 30 for holding the metals the temperature of which have dropped to be within the defined range after the mixing shall have a heat insulating effect in order to ensure that the crystal nuclei generated will grow into nondendritic (near-spherical) primary crystals and have the desired fraction liquid after a specified time. The constituent material of the insulated vessel is in no way limited to metals and those



which have a heat-retaining property and which yet wet with the melt only poorly are preferred. If a gas-permeable ceramic container is to be used as the insulated vessel 30 for holding magnesium alloys which are prone to oxidize and burn, the exterior to the vessel is preferably filled with a specified atmosphere (e. g. an inert or vacuum atmosphere).

If the holding time within the insulated vessel is less than 5 seconds, it is not easy to attain the temperature for the desired fraction liquid and it is also difficult to generate spherical primary crystals. What is more, semisolid metals of a uniform temperature profile cannot be attained. If the holding time exceeds 60 minutes, coarse spherical primary crystals will be generated.

It should also be mentioned that if the fraction liquid in the alloy which is about to be shaped by high-pressure casting is less than 20 %, the resistance to deformation during the shaping is so high that it is not easy to produce shaped parts of good quality. If the fraction liquid exceeds 90 %, shaped parts having a homogeneous structure cannot be obtained. Therefore, as already mentioned, the fraction liquid in the alloy to be shaped is preferably controlled to lie between 20 % and 90 %. More preferably, the fraction liquid should be adjusted to range between 30 % and 70 % in order to ensure that shaped parts of high quality can easily be produced by pressure forming. The means of pressure forming are in no way limited to high-pressure casting processes typified by squeeze casting and die casting and various other method of pressure forming may be adopted, such as extruding and casting operations.

By mixing two or more aluminum alloys having different liquidus temperature and holding the mixture within the insulated vessel 30, one can produce a semisolid metal of a fine spherical structure. If it is desired to generate more crystal nuclei so as to yield uniform and more fine-grained spherical structure in aluminum alloys, Ti and B may be added to the alloys. If the Ti content of the alloy mixture is less than 0.003 %, the intended refining effect of Ti is not attained; beyond 0.30 %, a coarse Ti compound will form to cause deterioration in ductility. Hence, the Ti addition is controlled to lie between 0.003 % and 0.30 %. Boron (B) in the mixed metal MC cooperates with Ti to promote the refining of crystal grains but its refining effect is small if the addition is less than 0.0005 %; on the other hand, the effect of B is saturated at 0.01 % and no further improvement is expected beyond 0.01 %. Hence, the B addition is controlled to lie between 0.0005 % and 0.01 %.

The constituent material of the jig 20 having the cooling zone with which the molten metals MA and MB are to be contacted before they are mixed is not limited to any particular types as long as it is capable of lowering the temperatures of the melts. A jig that is made of a highly heat-conductive metal such as copper, a copper alloy, aluminum or an aluminum alloy and which is controlled to provide a cooling effect for maintaining temperatures below a specified level is particularly preferred since it allows for the generation of many crystal nuclei. In order to ensure that the temperatures of the molten metals MA and MB which have been contacted with the cooling jig 20 are either just above or below the respective liquidus lines, the molten alloys held superheated to less than 300°C above the solidus temperatures are desirably contacted with a surface of the jig at a lower temperature than the melting points of said alloys. Preferably, the degree of superheating above the liquidus temperatures lie less than 100°C, more preferably less than 50°C.

Table 9 sets forth the conditions for the preparation of semisolid samples and the qualities of shaped parts. As shown in Fig. 70, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed, 1.5m/s; mold cavity dimensions, 100 x 150 x 10; mold temperature, 230 °C.

In Comparative Sample 9, the holding time was so long that undesirably large primary crystals formed. In Comparative Sample 10, the temperatures of the alloys to be mixed were high and so was the temperature of the resulting mixture; hence, the number of the crystal nuclei generated was small enough to produce only dendritic primary crystals. In Comparative Sample 11, the holding time was short whereas the liquid fraction in the alloy mixture was high and this caused extensive segregations in the interior of the shaped part.

Table 9 (continued on next page)

		*1				*2	*3	Cool- ing plate
		Compositons and proportions of alloys to be mixed						
		Alloy ①		Alloy ②				
		Composi- tion (%)	Propor- tion (%)	Composi- tion (%)	Propor- tion (%)			
Inven- tion Sample	No.					Alloy ①	Alloy ②	Alloy tem- perture just after mixing (°C)
	1	9Si	50	5Si	50	5	10	1
	2	5Si	50	9Si	50	5	5	0
	3	9Si	50	5Si	50	4	7	2
	4	9Si	70	3Si	30	15	20	5
	5	11Si	30	5Si	70	5	5	3
	6	9Si	50	5Si	50	0	1	-15
Compara- tive Sample	7	9Si	50	5Si	50	5	10	1
	8	11AL	50	7AL	50	10	10	3
	9	9	50	5	50	5	10	1
	10	9	50	5	50	70	60	30
	11	9	50	5	50	10	10	3

\*1 Alloy ① was first inserted into the ceramic vessel; Alloy No.8 was of Mg-Al system and the other alloys were of Al-Si system.

\*2 Expressed in terms of the degree of superheating above the melting point of each alloy.

\*3 Expressed in terms of the degree of superheating above the melting point of the alloy formed by mixing: Al-7%Si had m.p. of 615°C and Mg-9%Al-0.6%Zn had m.p. of 595°C.

Table 9 (continued)

	No.	Compositions and proportions of alloys to be mixed				Addi- tion of Ti and B	Hold- ing time (min)	Crystals in semisolid metal		Internal segrega- tion
		Alloy ①		Alloy ②				Morpho- logy	Size ( $\mu$ m)	
		Composi- tion (%)	Propor- tion (%)	Composi- tion (%)	Propor- tion (%)					
Inven- tion Sample	1	9Si	50	5Si	50	-	8.0	○	100	Absent
	2	5Si	50	9Si	50	-	8.2	○	115	Absent
	3	9Si	50	5Si	50	-	7.7	○	120	Absent
	4	9Si	70	3Si	30	-	8.0	○	150	Absent
	5	11Si	30	5Si	70	-	9.3	○	120	Absent
	6	9Si	50	5Si	50	-	5.9	○	70	Absent
	7	9Si	50	5Si	50	Yes *6	7.9	○	85	Absent
	8	11AL	50	7AL	50	-	3.5	○	80	Absent
Comparative	9	9	50	5	50	-	70	○	280	-
Sample	10	9	50	5	50	-	15.2	×	-	Present
	11	9	50	5	50	-	0.06	○	15	Present

\*4 Time taken for either the alloy (Al-7%Si) to attain 585 $\mu$  or the alloy (AZ91) to attain 580 $\mu$ .

\*5 ○, primary crystals were generally spherical;

×, primary crystals were dendritic

\*6 Ti, 0.15%; B, 0.005%

In each of Invention Samples 1 - 8, a homogeneous microstructure comprising fine (< 150  $\mu$ m) spherical primary crystals was obtained to enable the production of a shaped part having no internal segregations.

Example 14

This is an Example of the invention as recited in claim 38 and it was implemented by the same method as in Example 1, except that at the end of the step of holding the alloy partially molten within the insulated vessel 30 (or 30A), an oxide W forming on the semisolid metal was removed by means of a metallic or nonmetallic jig [step (3)-c in Fig. 74].

As also shown in Fig. 74, the shaping operation consisted of inserting the semisolid metal into an injection sleeve and subsequent forming on a squeeze casting machine. The forming conditions were as follows: pressure, 950 kgf/cm<sup>2</sup>; injection speed, 1.5 m/s; mold cavity dimensions, 100 x 150 x 10; mold temperature, 230°C.

Table 10 shows how the quality of shaped parts was affected by the presence or absence of the oxide. Obviously, Invention Samples 23 - 26 had better results than Comparative Samples 21 and 22.

Table 10 (continued on next page)

		Conditions of the semisolid metal to be shaped						Jig used to remove the top surface of the metal
No.	Alloy	Casting temperature (°C)	Temperature just after pouring (°C)	Temperature just before shaping (°C)	Hold-time (min)	Holding temperature (°C)	Constituent material	
Comparative Sample	21 AC4CH	630	614	585	7.1	50	ceramic	-
	22 AC4CH	630	615	585	14	300	ceramic	-
Invention Sample	23 AC4CH	630	614	585	6.8	50	ceramic	Aluminized iron jig having BN coat
	24 AC4CH	630	616	585	7.2	50	ceramic	Ceramic jig
	25 AC4CH	630	617	585	15	300	ceramic	Aluminized iron jig having BN coat
	26 AC4CH	630	615	585	14	300	ceramic	Ceramic jig

- \* Cooling jig (30°C) was used to induce the generation of crystal nuclei.
- \* Insulated ceramic holding vessel was chiefly made of special calcium silicate.
- \* Oxide pickup was checked by deflection test.
- \* Tensile test was conducted four times under each condition.
- \* Oxide pickup: O, negligible; X, a little

Table 10 (continued)

	No.	Alloy	Quality of shaped part			Tensile strength (MPa)	Elongation at break	
			When the oxide was removed	Oxide pickup			Maximum (%)	Minimum (%)
Comparative Sample	21	AC4CH	-	x		291	16	9
	22	AC4CH	-	x		288	17	11
Invention Sample	23	AC4CH	Just after pouring of the melt	○		315	19	16
	24	AC4CH	Just before the molding temperature was reached	○		322	21	18
	25	AC4CH	Just after pouring of the melt	○		315	20	15
	26	AC4CH	Just before the molding temperature was reached	○		318	22	17

## Claims

1. A method of shaping a semisolid metal, in which a liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is fed into an insulated vessel having a heat insulating effect, held in said insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, thereby crystallizing fine primary crystals in the alloy solution, and the alloy is fed into a forming mold, where it is shaped under pressure.
2. A method according to claim 1, wherein the crystal nuclei are generated by contacting the molten alloy with a surface of a jig at a temperature lower than the melting point of said alloy which has been held superheated to less than 300°C above the liquidus temperature.
3. A method according to claim 2, wherein the jig with which the melt is to be contacted is a metallic or nonmetallic jig, or a metallic jig having a surface coated with a nonmetallic material or semiconductor, or a metallic jig composited with a nonmetallic material or semiconductor, with said jig being adapted to be coolable from either inside or outside.
4. A method according to claim 1 or 2, wherein the crystal nuclei are generated by applying vibrations to the molten metal in contact with either the jig or the insulated vessel or both.
5. A method according to claim 1 or 2, wherein the alloy is an aluminum alloy of a composition within a maximum solubility limit or a hypoeutectic aluminum alloy of a composition at or above a maximum solubility limit.
6. A method according to claim 1 or 2, wherein the alloy is a magnesium alloy of a composition within a maximum solubility limit.
7. A method according to claim 5, wherein the aluminum alloy has 0.001% - 0.01% B and 0.005% - 0.3% Ti added thereto.
8. A method according to claim 6, wherein the magnesium alloy has 0.005% - 0.1% Sr added thereto, or 0.01% - 1.5% Si and 0.005% - 0.1% Sr added thereto, or 0.05% - 0.30% Ca added thereto.
9. A method according to claim 7, wherein a molten aluminum alloy held superheated less than 100°C above the liquidus temperature is directly poured into the insulated vessel without using a jig.
10. A method according to claim 8, wherein a molten magnesium alloy held superheated to less than 100°C above the liquidus temperature is directly poured into the insulated vessel without using a jig.
11. A method of shaping a semisolid metal, in which liquid alloy having crystal nuclei that has been superheated by a degree (X °C) of less than 10°C above the liquidus line is held in an insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to a molding temperature where a specified fraction liquid is established, such that the cooling from the initial temperature at which said alloy is held in said insulated vessel to its liquidus temperature is completed within a time shorter than the time Y (in minutes) calculated by the relation  $Y=10-X$  and that the period of cooling from said initial temperature to a temperature 5°C lower than said liquidus temperature is not longer than 15 minutes, whereby fine primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.
12. A method of shaping a semisolid metal, in which a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is held within an insulated vessel for a period from 5 seconds to 60 minutes as it is cooled to the molding temperature where a specified fraction liquid is established, such that the period of cooling from the initial temperature at which said alloy is held in said insulated vessel to a temperature 5°C lower than its liquidus temperature is not longer than 15 minutes, whereby fine primary crystals are crystallized in the alloy solution, which is then fed into a forming mold, where it is shaped under pressure.
13. A method according to claim 11 or 12, wherein the crystal nuclei are generated by holding the molten alloy superheated to less than 300°C above the liquidus temperature and contacting the melt with a surface of a jig at a lower temperature than its melting point.

14. An apparatus for producing a semisolid forming metal having fine primary crystals dispersed in a liquid phase, which comprises a nucleus generating section that causes a molten metal to contact a cooling jig to generate crystal nuclei in the solution and a crystal generating section having an insulated vessel in which the metal obtained in said nucleus generating section is held as it is cooled to a molding temperature at which said metal is partially solid, partially liquid.
15. An apparatus according to claim 14, wherein the cooling jig in the nucleus generating section is either an inclined flat plate that has an internal channel for a cooling medium and that has a pair of weirs provided on the top surface parallel to the flow of the melt, or a cylindrical or semicylindrical tube.
16. A method of shaping a semisolid metal, in which a liquid alloy having crystal nuclei at a temperature not lower than the liquidus temperature or a partially solid, partially liquid alloy having crystal nuclei at a temperature not lower than a molding temperature is poured into a vessel so that it is cooled to a temperature at which a fraction solid appropriate for shaping is established, said vessel being adapted to be heatable or coolable from either inside or outside, being made of a material having a thermal conductivity of at least  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  (at room temperature) and being held at a temperature not higher than the liquidus temperature of said alloy prior to its pouring, and in which said alloy is poured into said vessel in such a manner that fine, nondendritic primary crystals are crystallized in said alloy solution and that said alloy is cooled rapidly enough to be provided with a uniform temperature profile in said vessel, and said alloy, after being cooled, is fed into a forming mold, where it is shaped under pressure.
17. A method according to claim 16, wherein the step of cooling said alloy is performed with the top and bottom portions of the vessel being heated by a greater degree than the middle portion or heat-retained with a heat-retaining material having a thermal conductivity of less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  or with either the top or bottom portion of the vessel being heated while the remainder is heat-retained.
18. A method according to claim 16, wherein the step of cooling said alloy is performed with the vessel holding said alloy being accommodated in an outer vessel that is capable of accommodating said alloy holding vessel and that has a smaller thermal conductivity than said holding vessel, or that has a thermal conductivity equal to or greater than that of said holding vessel and which has a higher initial temperature than said holding vessel, or that is spaced from said holding vessel by a gas-filled gap, at a sufficiently rapid cooling rate to provide a uniform temperature profile through the alloy in said holding vessel no later than the start of the shaping step.
19. In a method of managing the temperature of a semisolid metal slurry for use in molding equipment in which a molten metal containing a large number of crystal nuclei is poured into a vessel, where it is cooled to produce a semisolid metal slurry containing both a solid and a liquid phase in specified amounts, said slurry being subsequently fed into a molding machine for shaping under pressure, the improvement wherein the vessel for holding said molten metal is temperature-managed such as to establish a preset desired temperature prior to the pouring of said molten metal and such that said molten metal is cooled at an intended rate after said molten metal is poured into said vessel.
20. An apparatus for managing the temperature of a semisolid metal slurry to be used in molding equipment in which a molten metal containing a large number of crystal nuclei is poured from a melt holding furnace into a vessel, where it is cooled to produce a semisolid metal slurry containing both a solid and a liquid phase in specified amounts and in which said slurry is directly fed into a molding machine for shaping under pressure, which apparatus comprising the vessel for comprising the vessel for holding said molten metal, a vessel temperature control section for managing the temperature of said vessel, a semisolid metal cooling section for managing the temperature of the as-poured molten metal such that it is cooled at an intended rate, and a vessel transport mechanism comprising basically a robot for gripping, moving and transporting said vessel and a conveyor for carrying, moving and transporting said vessel.
21. An apparatus according to claim 20, wherein the vessel temperature control section comprises a vessel cooling furnace for cooling the vessel at an ambient temperature not higher than a target temperature for the vessel and a vessel heat-retaining furnace for holding the vessel at an ambient temperature equal to said target temperature.
22. An apparatus according to claim 20, wherein the semisolid metal cooling section comprises a semisolid metal slowly cooling furnace and a semisolid metal slowly cooling furnace for managing the temperature in itself to be higher than the temperature in said semisolid metal cooling furnace.



23. An apparatus according to claim 22, wherein the semisolid metal cooling furnace is such that the area around the vessel carried on the conveyor device moving to pass through said furnace is partitioned into three regions, the upper, middle and lower parts, by means of two pairs of heat insulating plates, one pair consisting of an upper right and an upper left plate and the other pair consisting of a lower right and a lower left plate, with a heater being installed in both said upper and lower parts for heating said two parts at a higher temperature than hot air to be supplied to said central part.
24. An apparatus according to claim 22, wherein a preheating furnace is installed at a stage prior to the semisolid metal cooling furnace to ensure that both a plinth having a lower thermal conductivity than said vessel and which carries said vessel before it is directed to said semisolid metal cooling furnace and a lid having a lower thermal conductivity than said vessel and which is to be placed to cover it after it accommodates said molten metal are preheated by being moved to pass through said preheating furnace in advance.
25. An apparatus according to claim 24, wherein the semisolid metal cooling furnace is equipped with a control unit with which the temperature or the velocity of hot air to be supplied into said semisolid metal cooling furnace is controlled to vary with the lapse of time.
26. An apparatus according to claim 22, wherein the semisolid metal cooling furnace comprises an array of housings each accommodating the vessel as it contains the molten metal and being equipped with an openable cover and hot air feed/exhaust pipes, as well as a mechanism by which a receptacle for carrying said vessel is rotated about a vertical shaft.
27. An apparatus according to claim 26, wherein the housing are each equipped with a vibrator for vibrating the receptacle.
28. An apparatus according to claim 24, wherein the semisolid metal cooling furnace for treating the molten metal as poured into a vessel having a thermal conductivity of at least  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  is supplied with hot air having a temperature in the range from  $150^\circ\text{C}$  to  $350^\circ\text{C}$  for aluminum alloys and from  $200^\circ\text{C}$  to  $450^\circ\text{C}$  for magnesium alloys.
29. An apparatus according to claim 24, wherein the semisolid metal cooling furnace for treating the molten metal as poured into a vessel having a thermal conductivity of less than  $1.0 \text{ kcal/hr} \cdot \text{m} \cdot ^\circ\text{C}$  is supplied with hot air having a temperature in the range from  $50^\circ\text{C}$  to  $200^\circ\text{C}$  for aluminum alloys and from  $100^\circ\text{C}$  to  $250^\circ\text{C}$  for magnesium alloys.
30. A method according to claim 1 or 2, wherein the molten metal as poured into the insulated vessel is isolated from the ambient atmosphere by closing the top surface of said vessel with an insulating lid having a heat insulating effect as long as said molten metal is held within said vessel until the molding temperature is reached.
31. A method according to claim 1 or 2, wherein the alloy is a zinc alloy.
32. A method according to claim 1 or 2, wherein the alloy is a hypereutectic Al-Si alloy having 0.005% - 0.03% P added thereto or a hypereutectic Al-Si alloy containing 0.005% - 0.03% P and having either 0.005% - 0.03% Sr or 0.001% - 0.01% Na or both added thereto.
33. A method according to claim 1 or 2, wherein the alloy is a hypoeutectic Al-Mg alloy containing Mg in an amount not exceeding a maximum solubility limit and which has 0.3% - 2.5% Si added thereto.
34. A method according to claim 1 or 2, wherein the pressure forming is accomplished with the alloy being inserted into a container on an extruding machine.
35. A method according to claim 34, wherein the extruding machine is of either a horizontal or a vertical type or of such a horizontal type in which the container changes position from being vertical to horizontal before shaping and wherein the method of extrusion is either direct or indirect.
36. A method according to claim 1, wherein the crystal nuclei are generated by a method in which two or more liquid alloys having different melting points that are held superheated to less than  $50^\circ\text{C}$  above the liquidus temperature are mixed either directly within the insulated vessel having a heat insulating effect or along a trough in a path into the insulated vessel, such that the temperature of the metal as mixed is either just above or below the liquidus temperature.

37. A method according to claim 36, wherein the two or more metals to be mixed are preliminarily contacted with respective jigs each having a cooling zone such as to produce metals of different melting points that have crystal nuclei and which have attained temperatures just either above or below the liquidus temperature.

5 38. A method according to claim 1, wherein the top surface of the semisolid metal that is held within the insulated vessel and which is to be fed into the forming mold is removed by means of either a metallic or nonmetallic jig during a period from just after the pouring into said vessel but before the molding temperature is reached and, thereafter, said semisolid metal is inserted into an injection sleeve.

10 39. A method according to claim 18, wherein the outer vessel is heated either from inside or outside or by induction heating, with such heating being performed only before or after the insertion of the holding vessel into the outer vessel or continued throughout the period not only before but also after said insertion.

40. A method according to claim 9, wherein the aluminum alloy is replaced by a zinc alloy.

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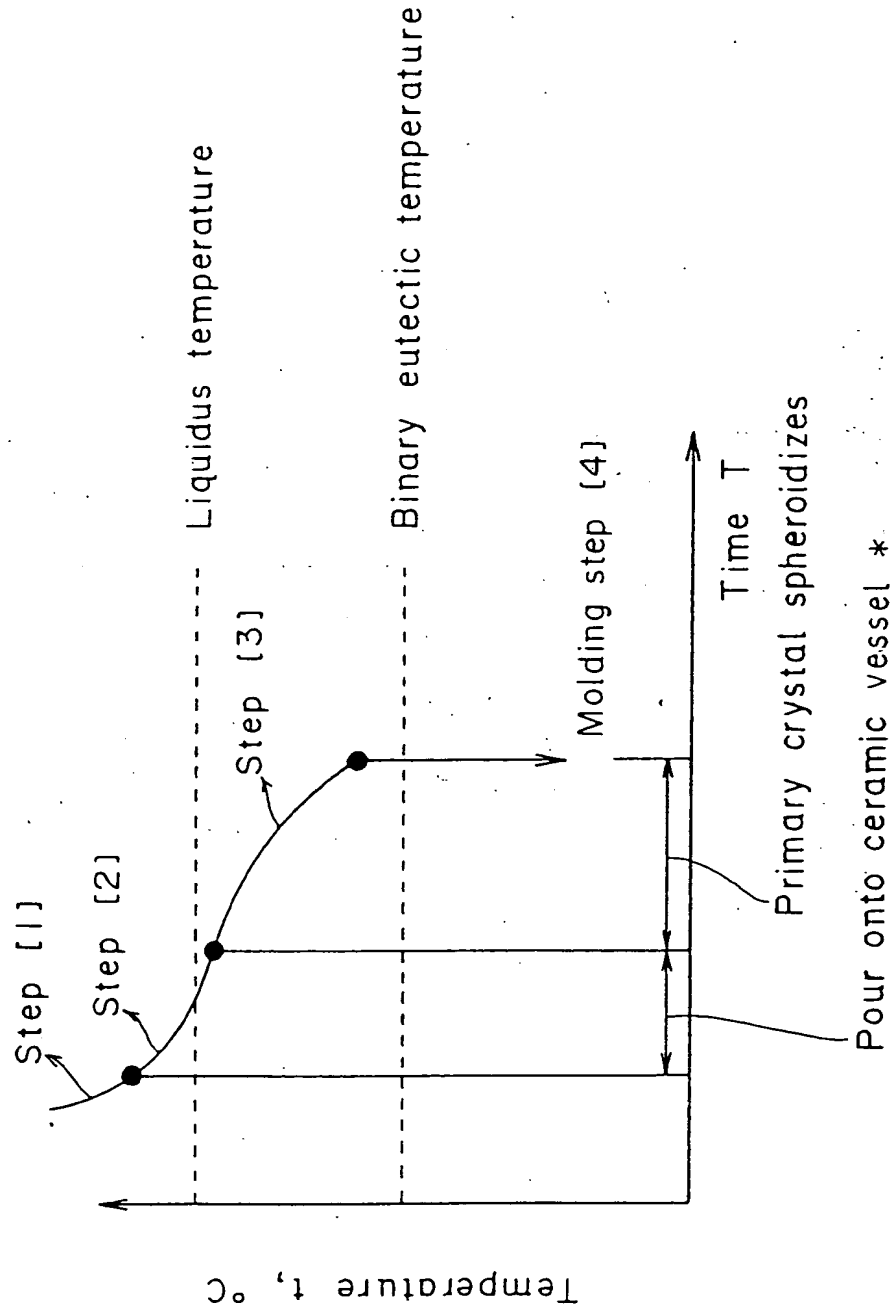
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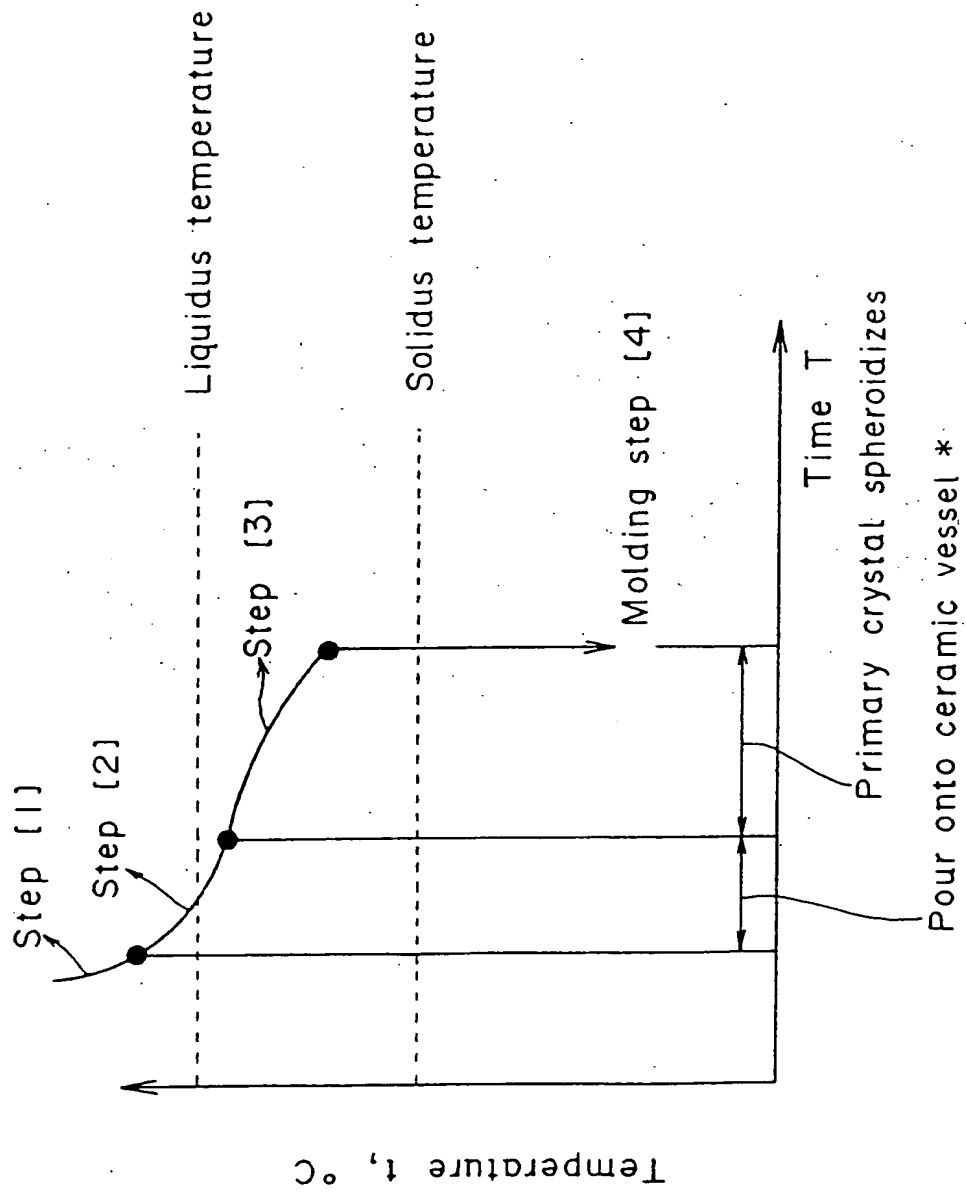
55

FIG. 1



\* With or without cooling jig

FIG. 2



\*With or without cooling jig

FIG. 3

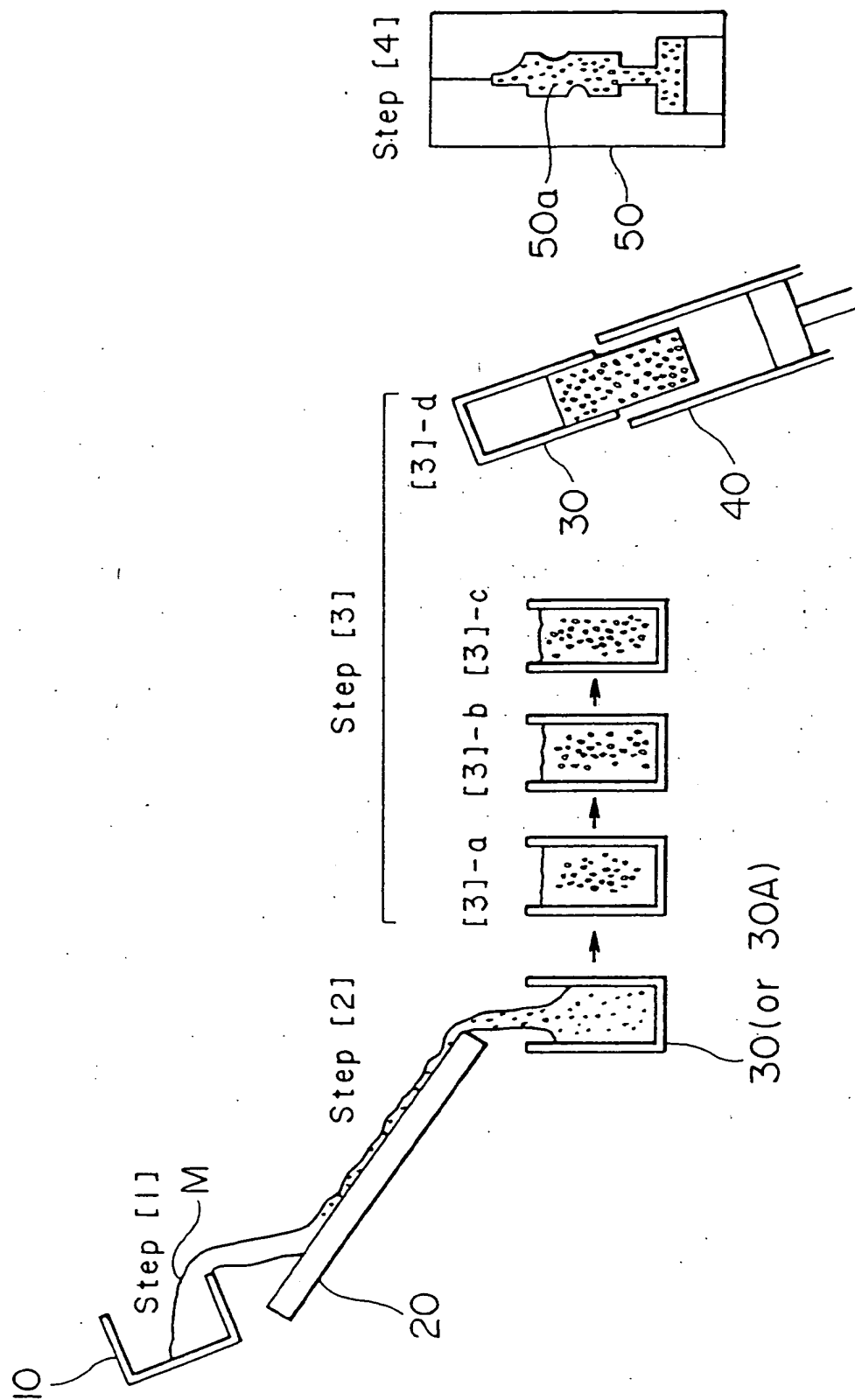


FIG. 4

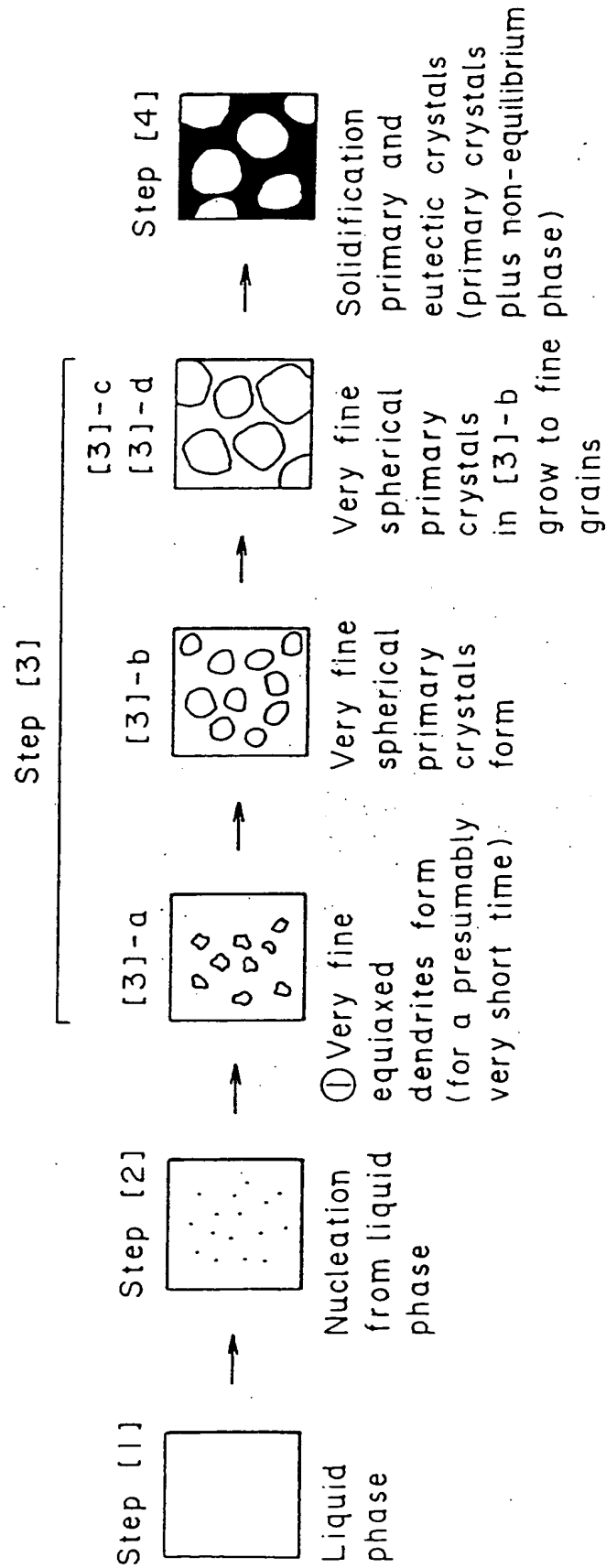


FIG. 5

Superheated to no more than 100°C  
(without cooling jig) or 300°C  
(with cooling jig) above liquidus temperature

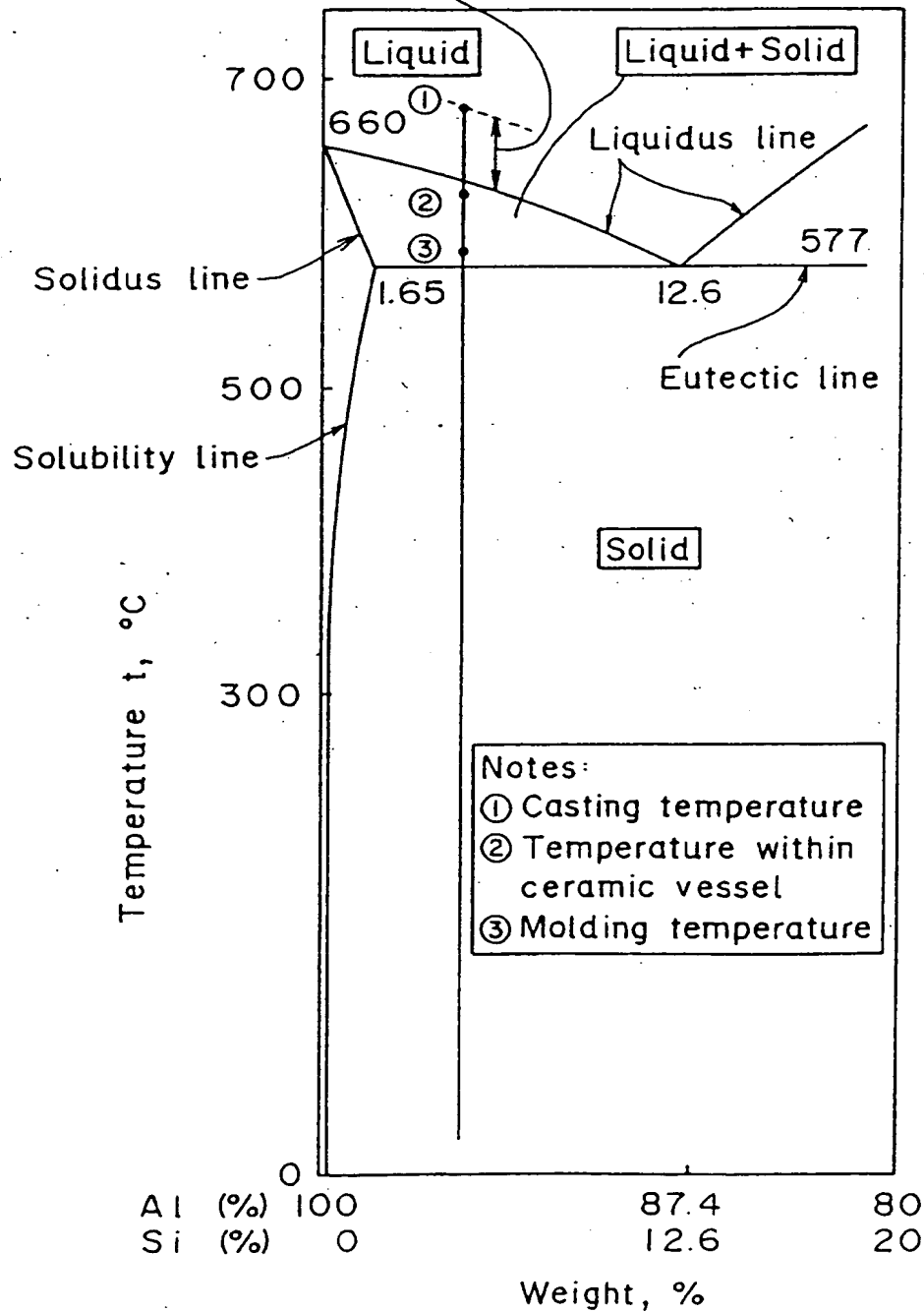


FIG. 6

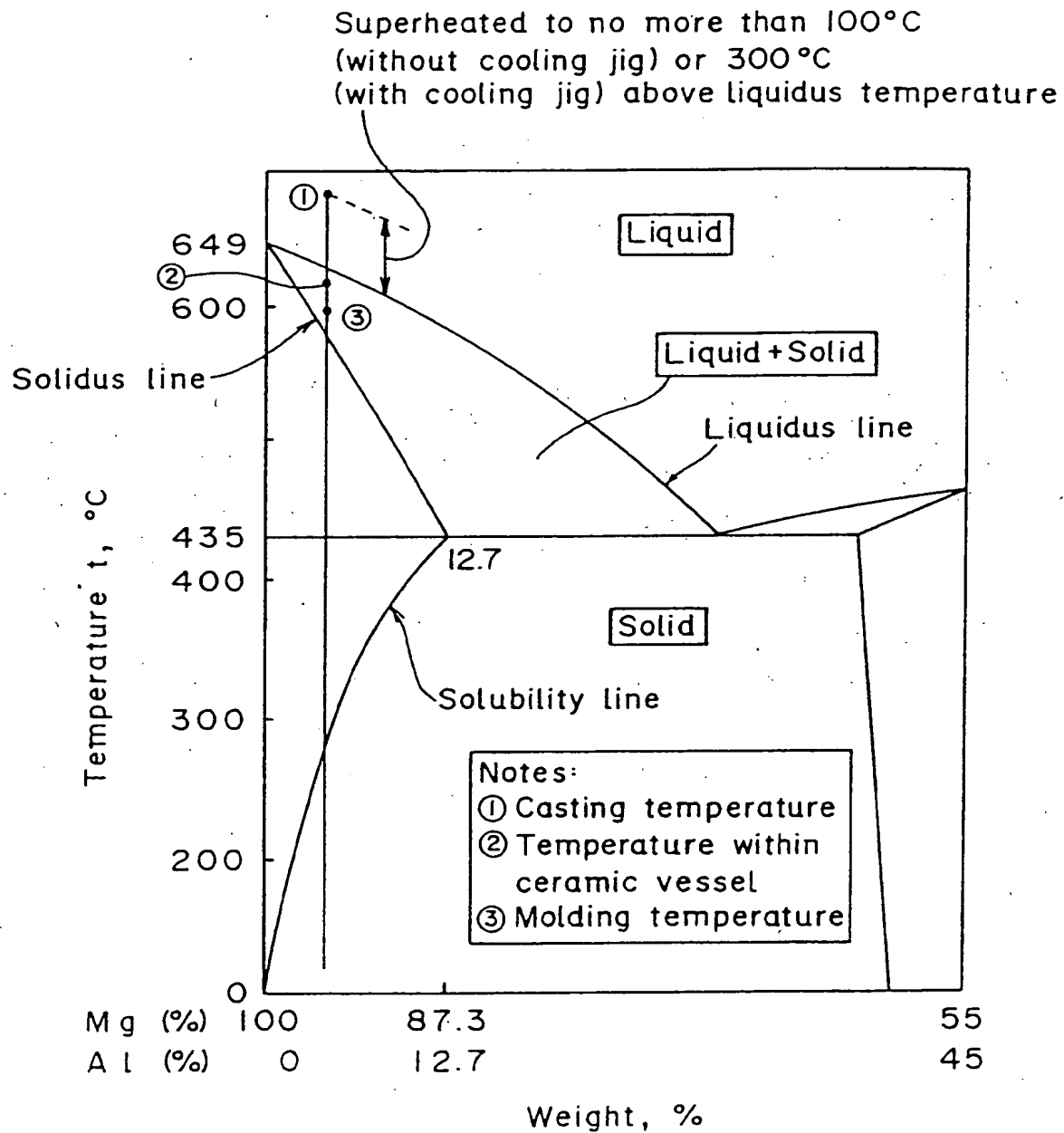




FIG. 7

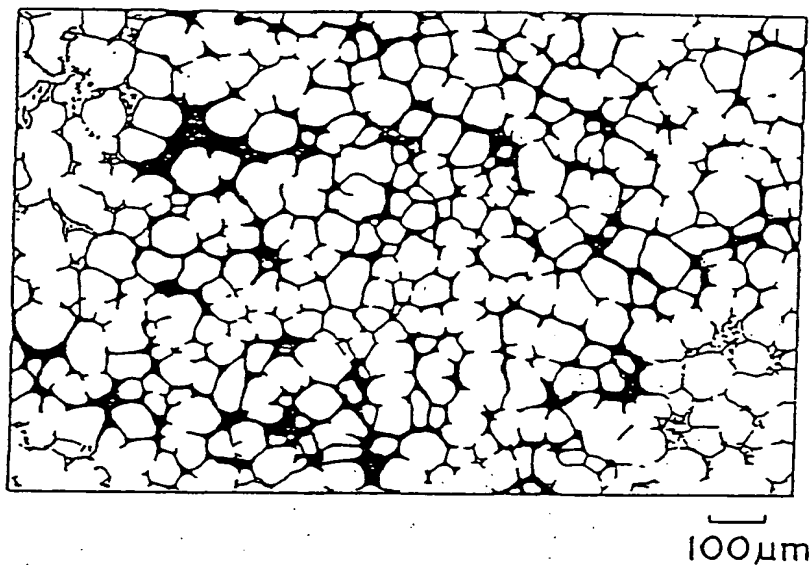


FIG. 8 Prior Art

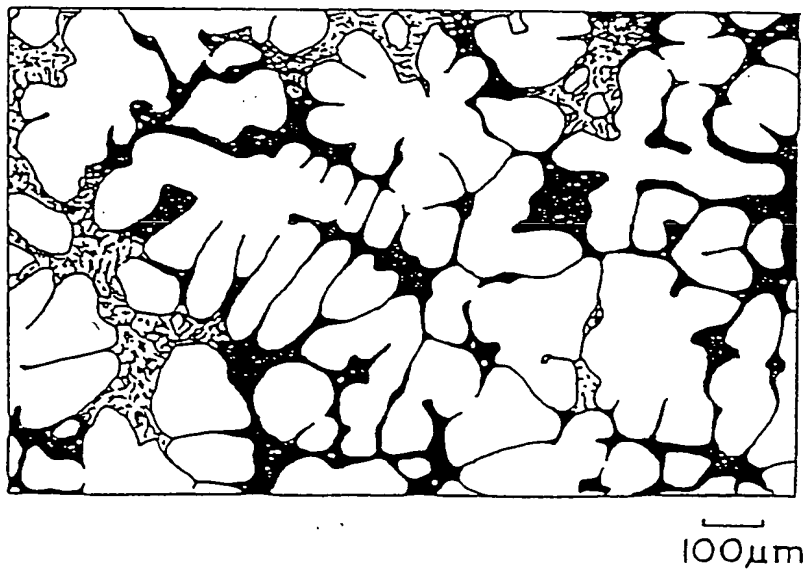
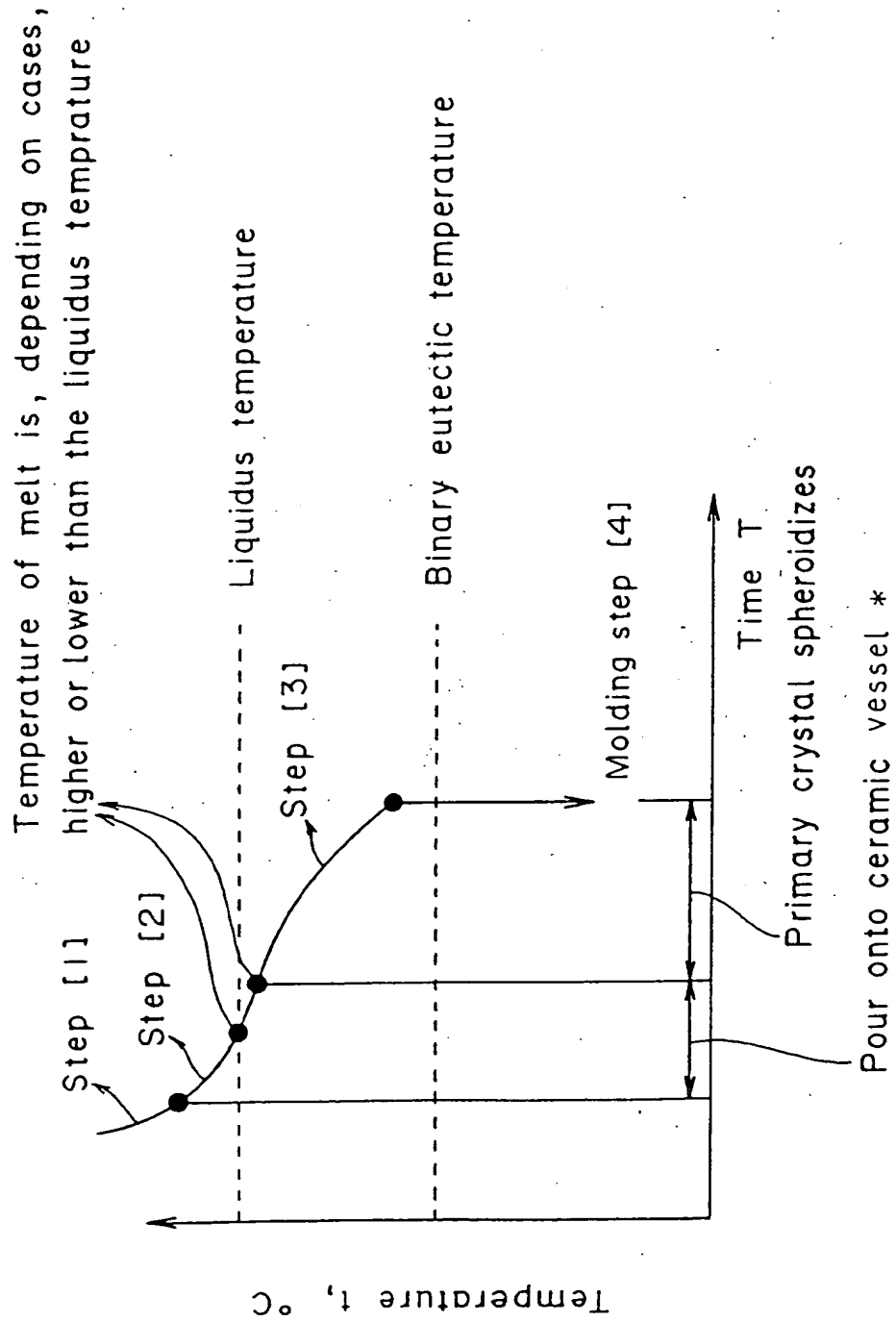


FIG. 9



\* With or without cooling jig

FIG. 10

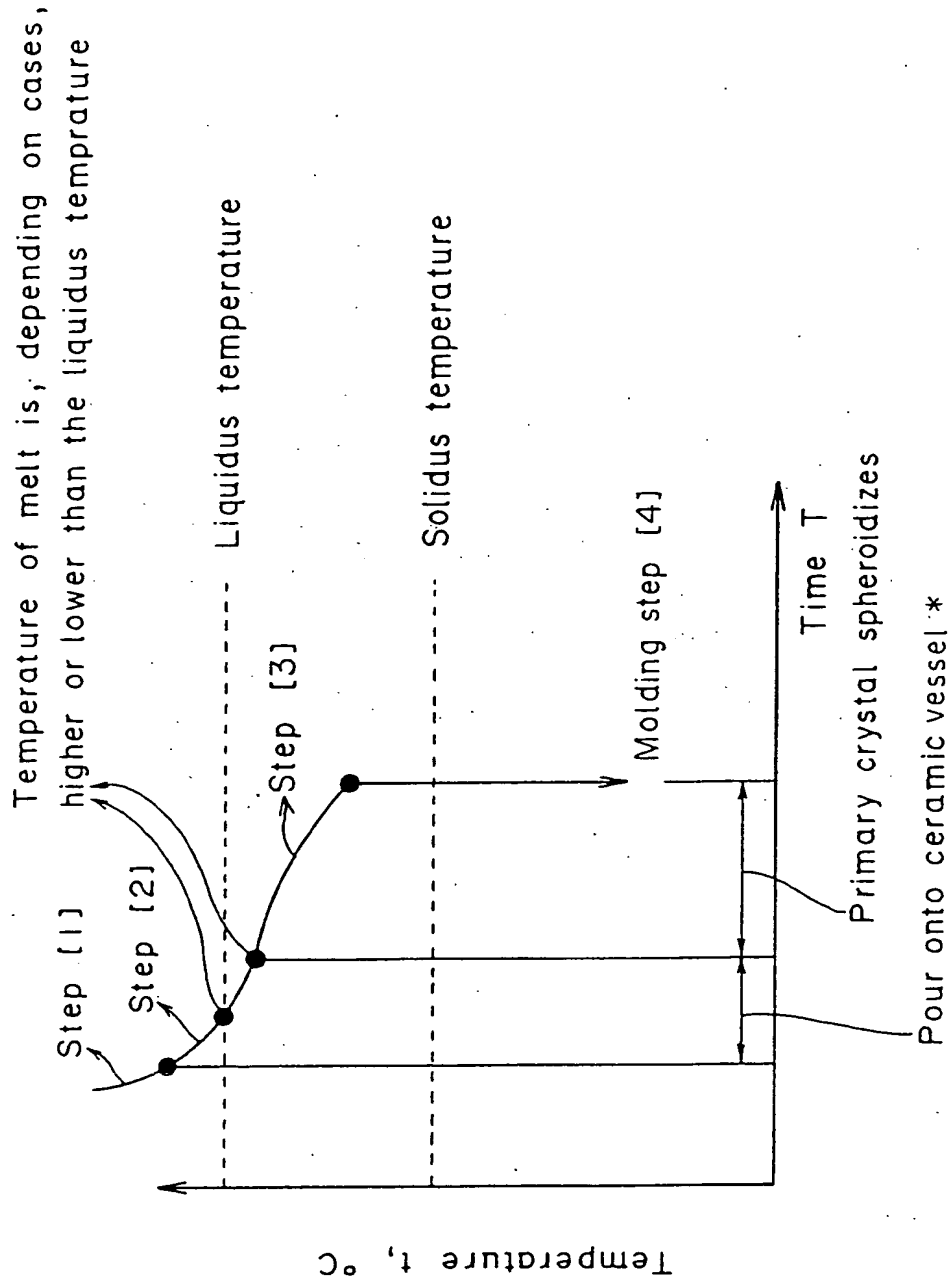


FIG. 11

Temperature of melt is, depending on cases,  
higher or lower than the liquidus temperature

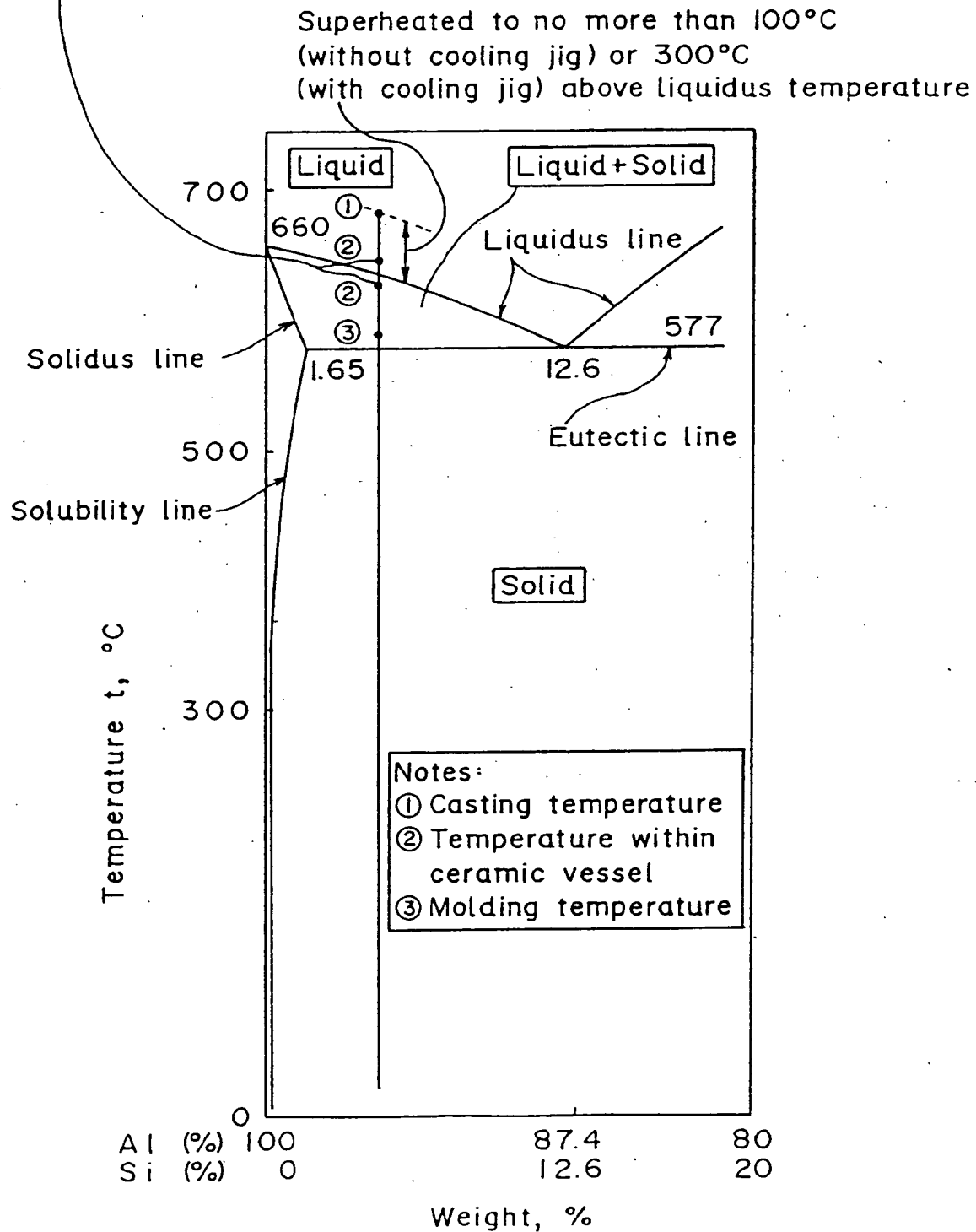


FIG. 12

Temperature of melt is, depending on cases,  
higher or lower than the liquidus temperature

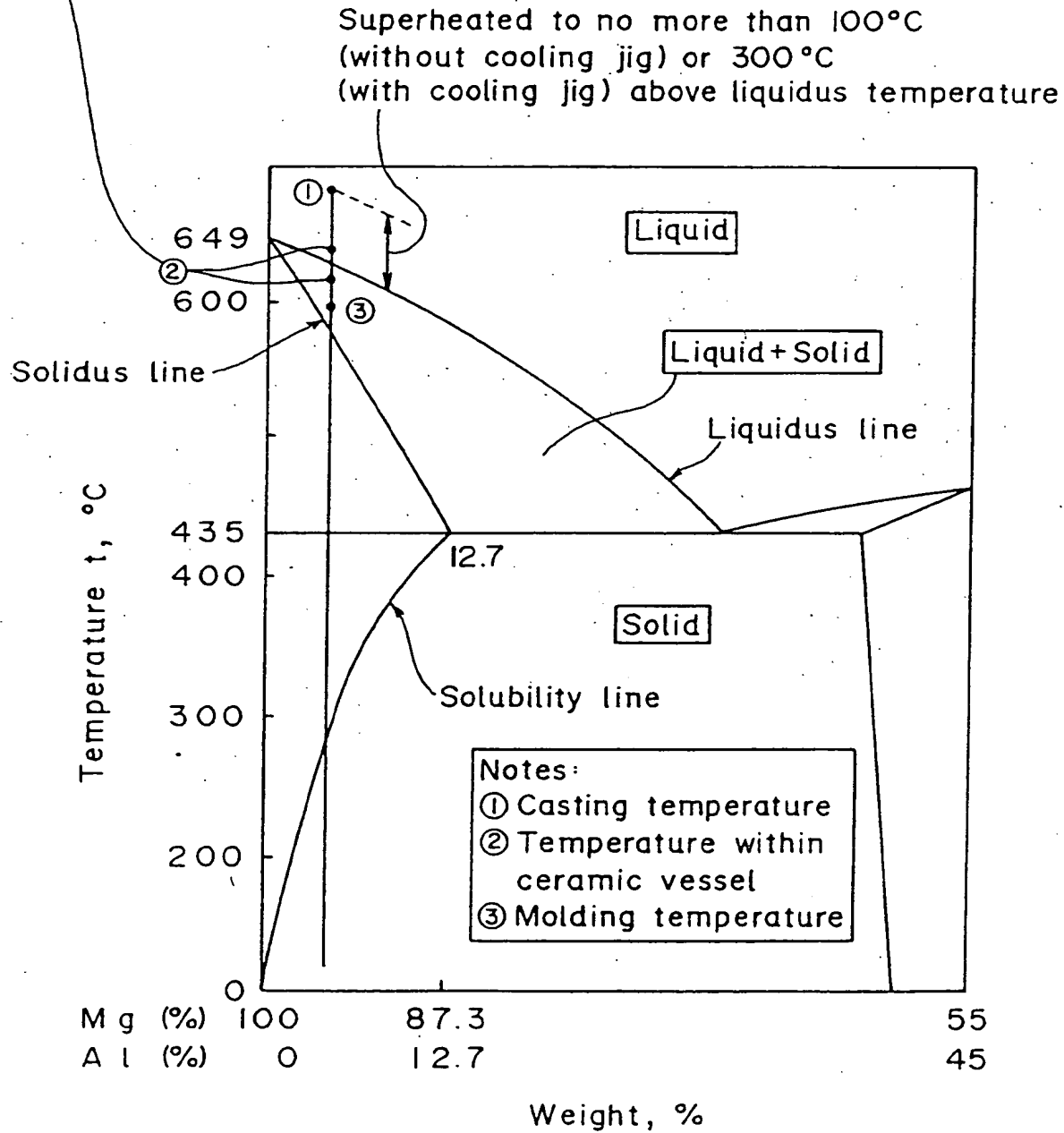


FIG. 13

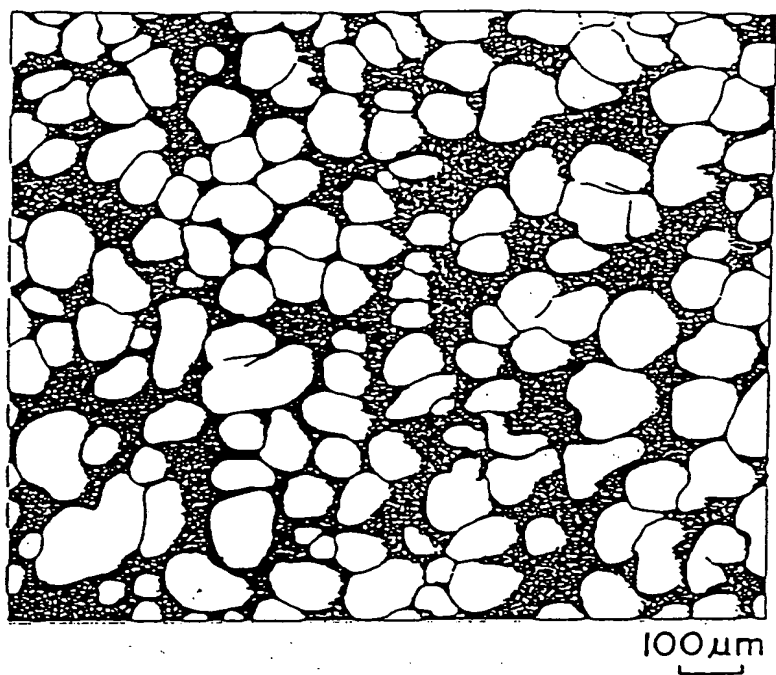


FIG. 14. Prior Art

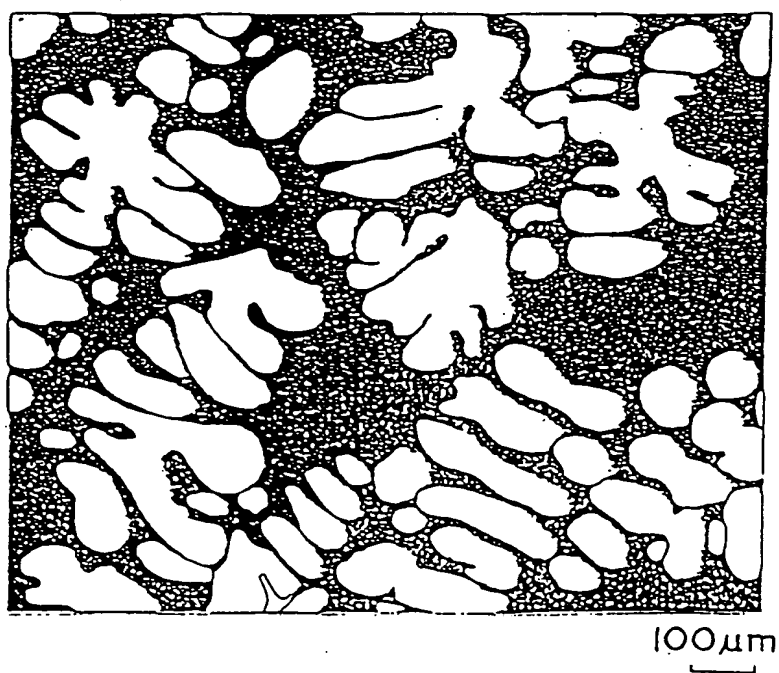


FIG. 15

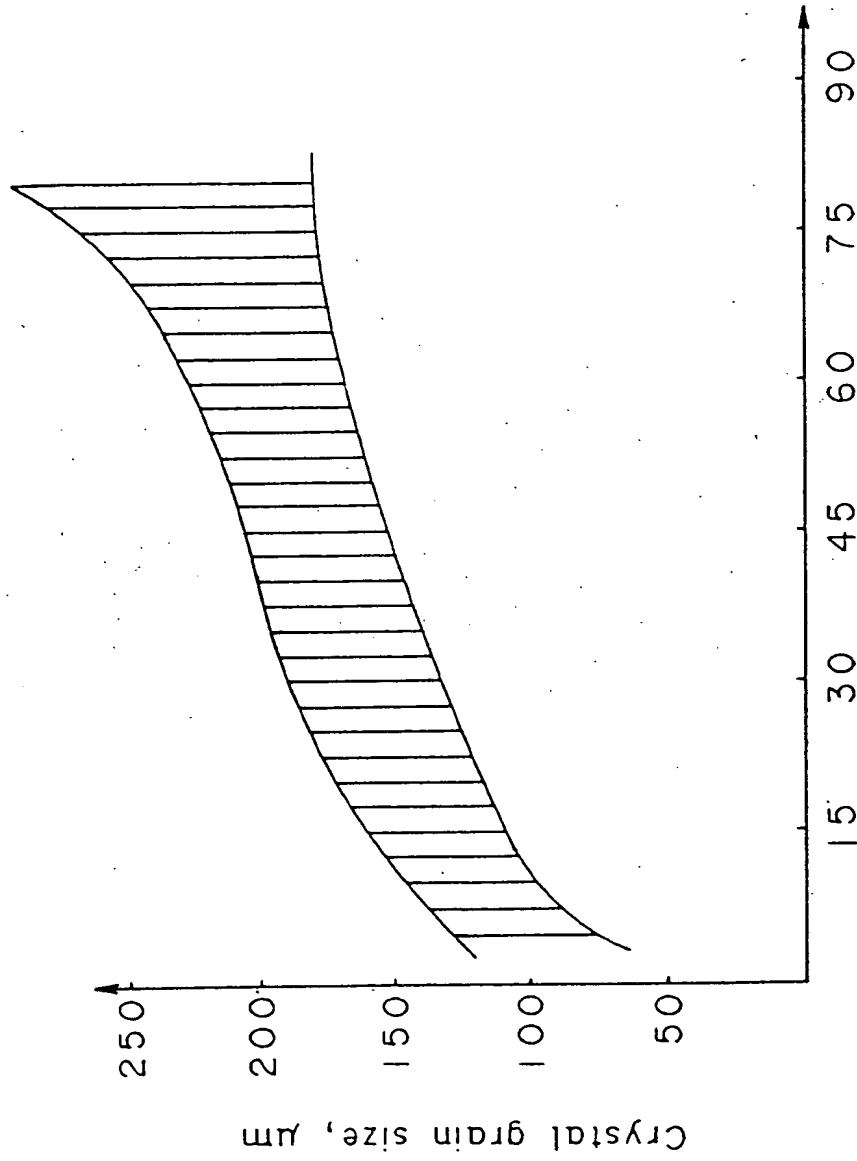


FIG. 16

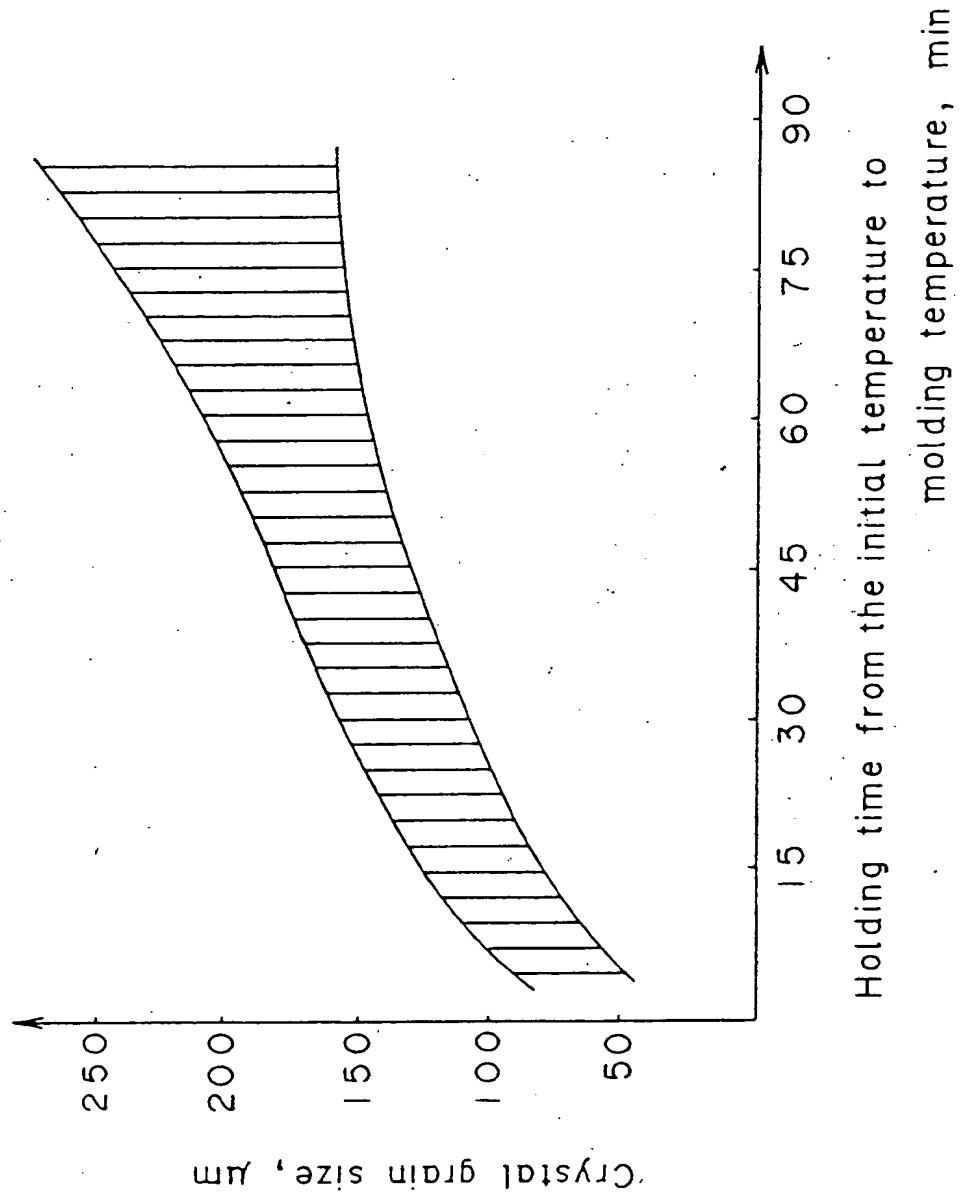




FIG. 17

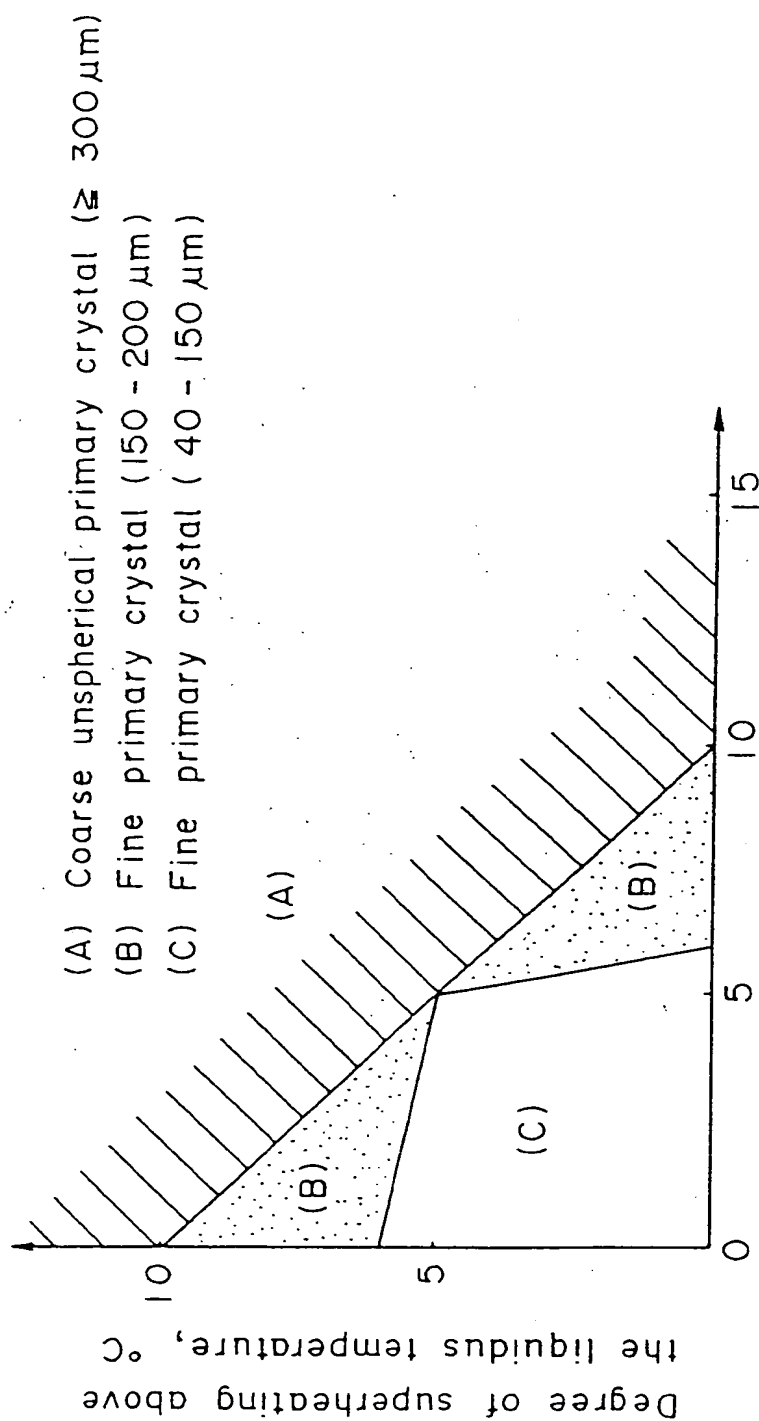
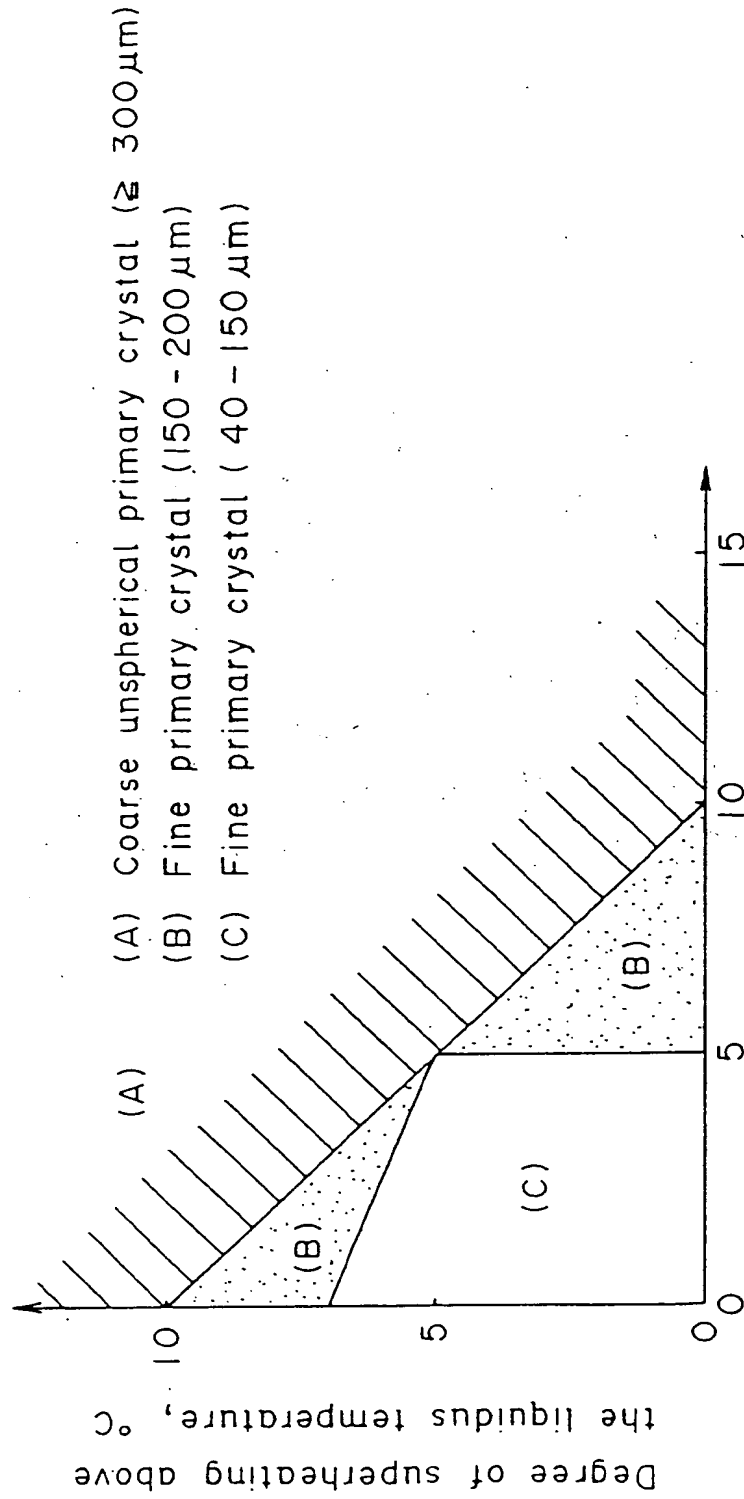
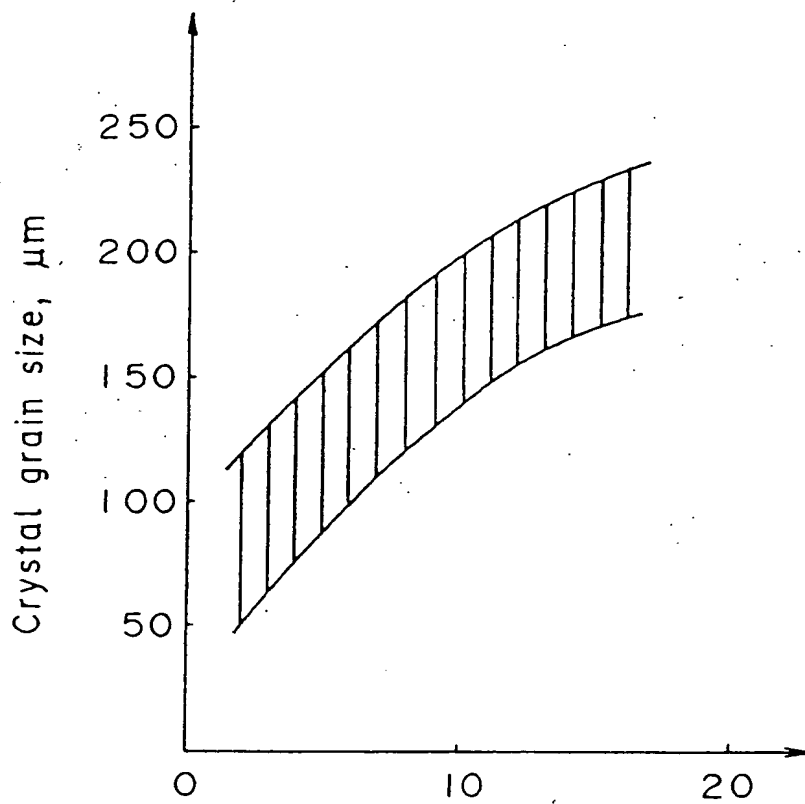


FIG. 18



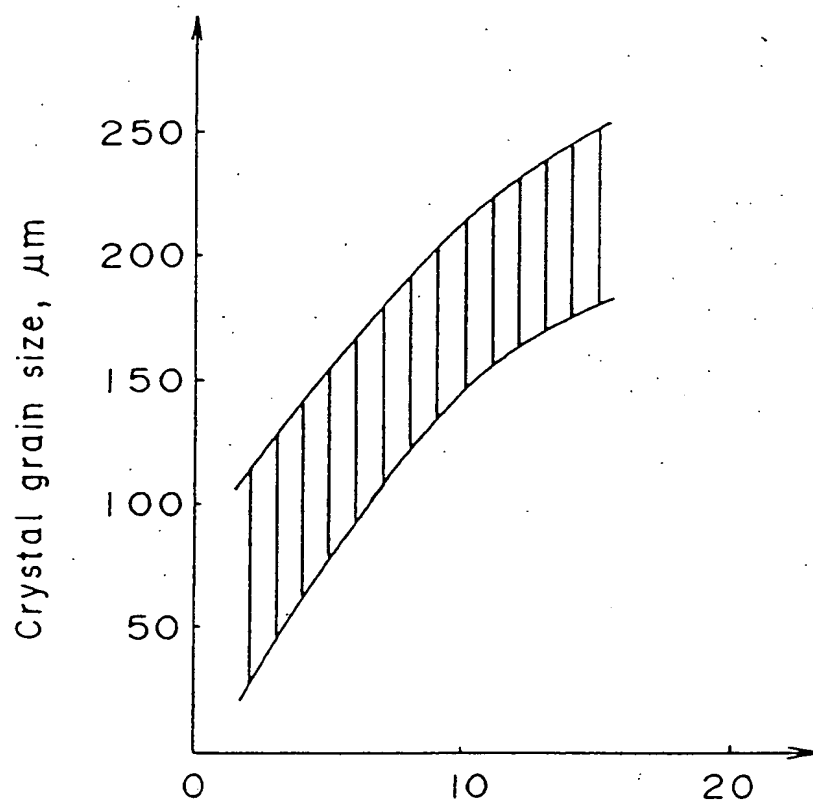
Holding time from the initial temperature  
in insulated vessel to the liquidus temperature, min

FIG. 19



Holding time from the initial temperature  
in insulated vessel to the liquidus  
temperature minus 5°C, min

FIG. 20



Holding time from the initial temperature  
in insulated vessel to the liquidus  
temperature minus 5°C, min

FIG. 21

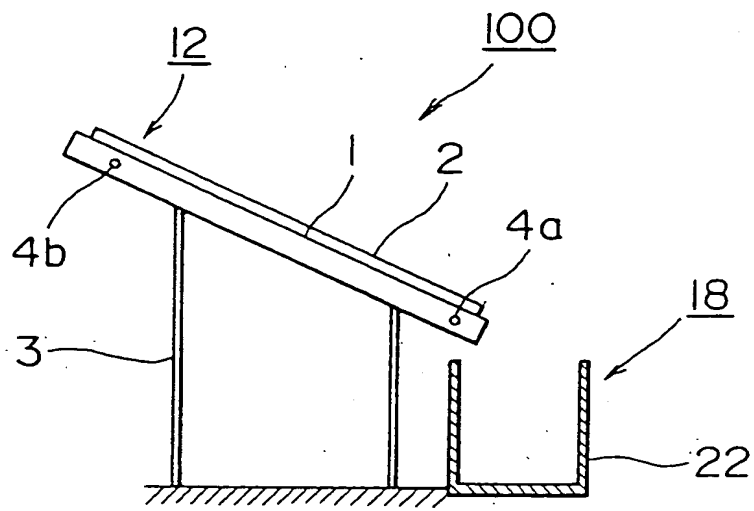


FIG. 22

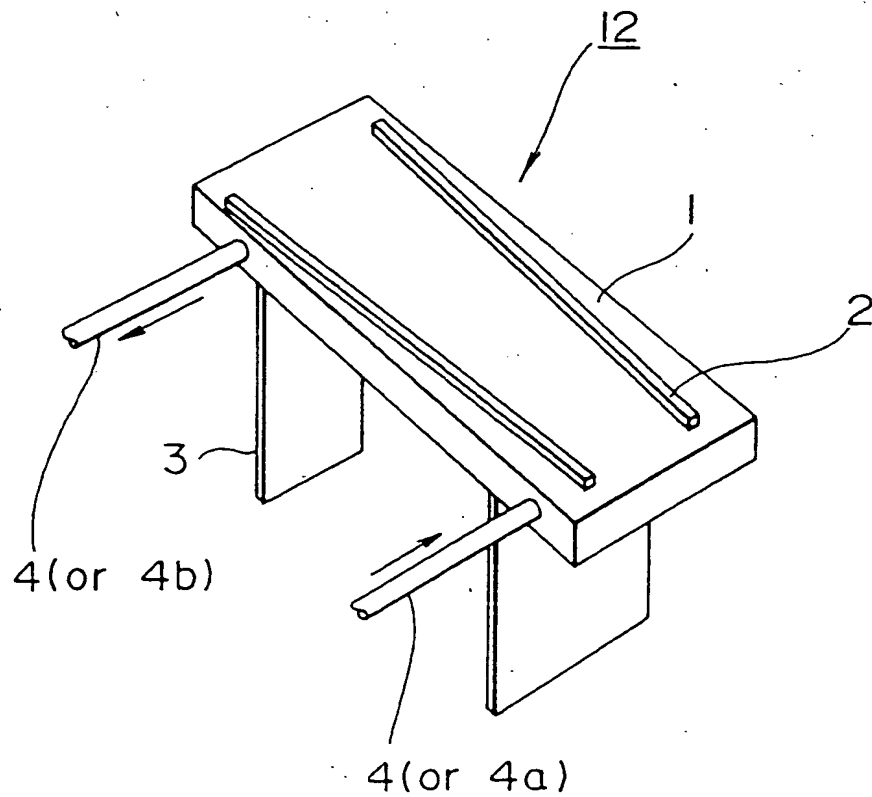


FIG. 23(a)

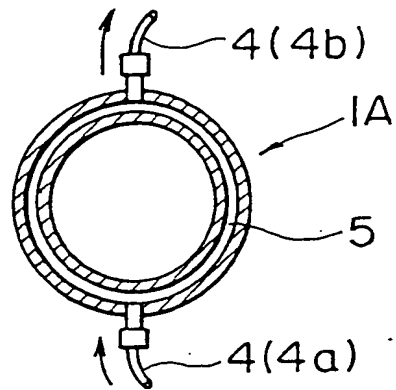


FIG. 23(b)

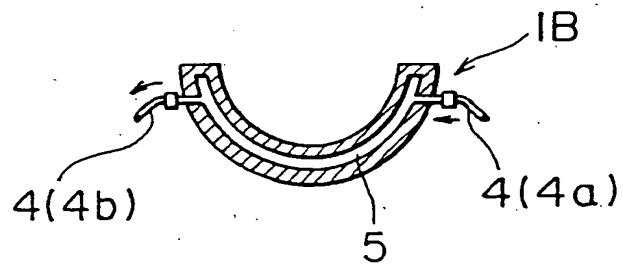


FIG. 24

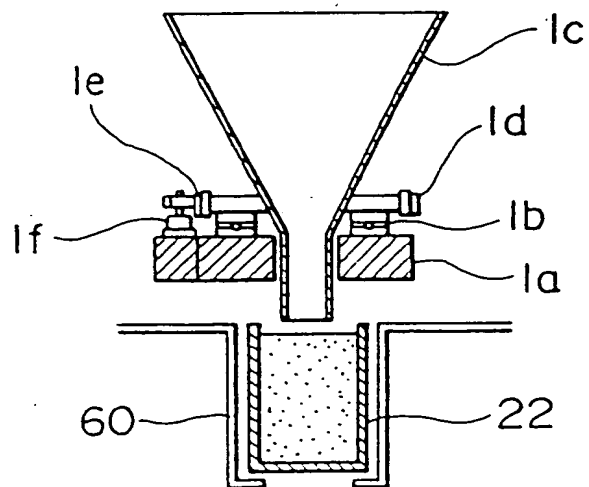


FIG. 25

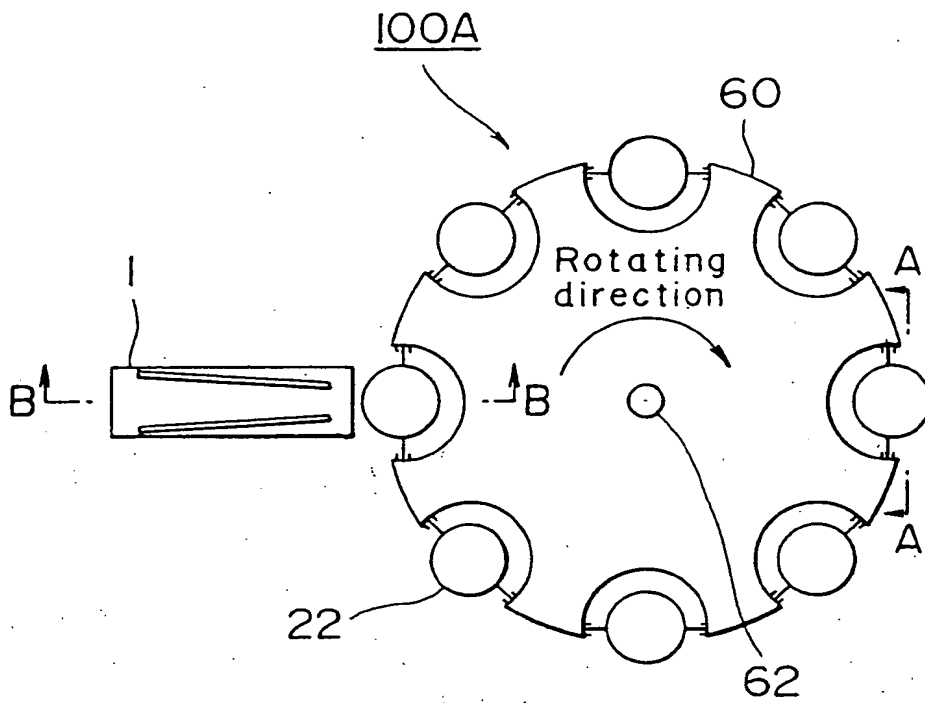


FIG. 26

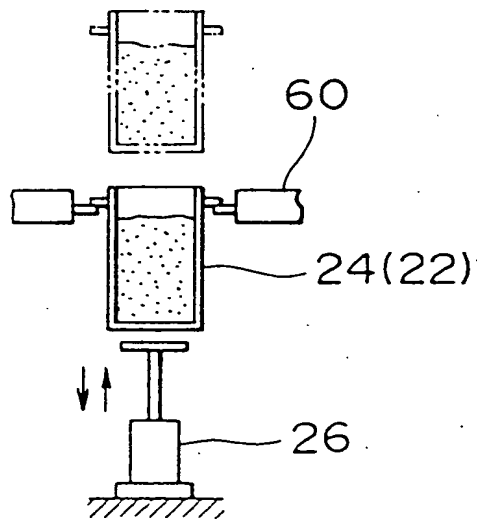


FIG. 27

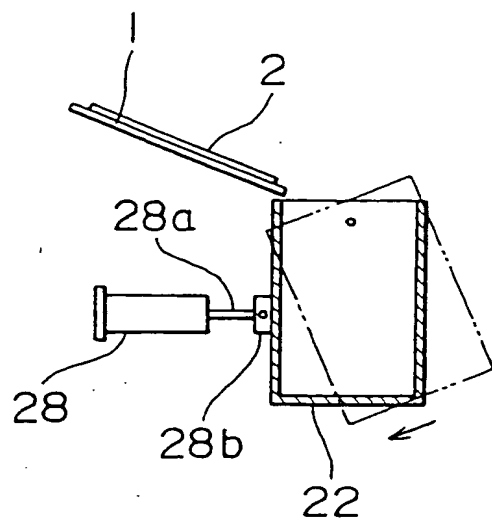


FIG. 28

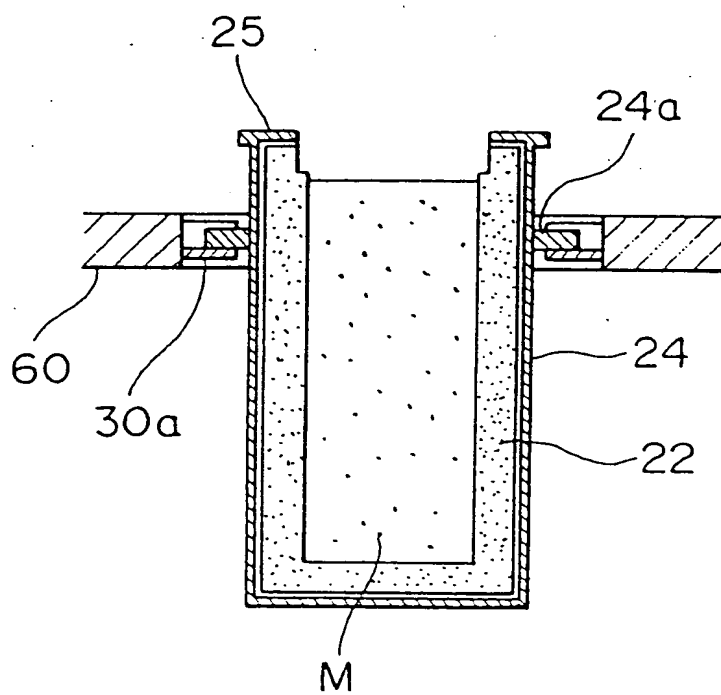




FIG. 29

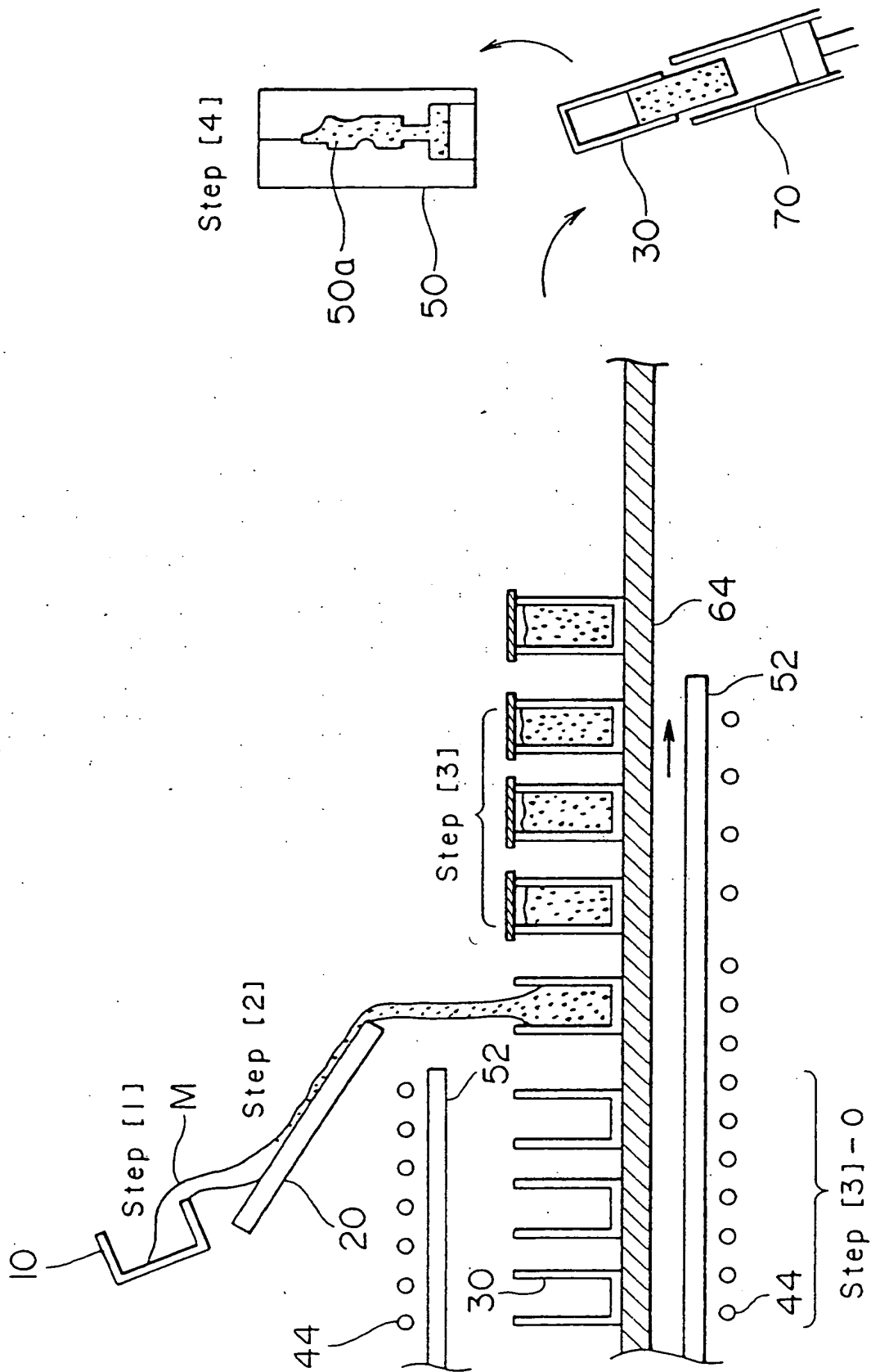


FIG. 30

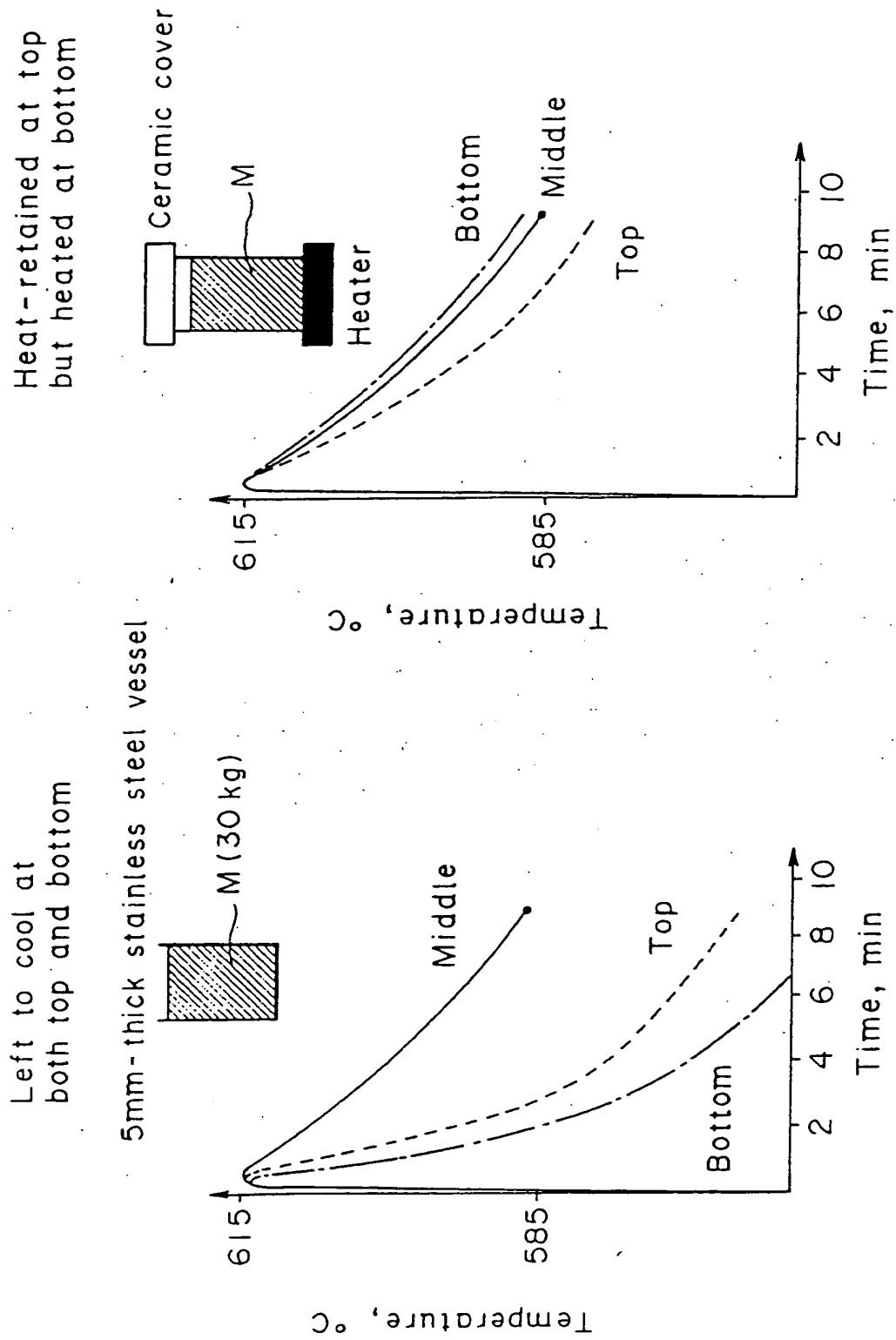
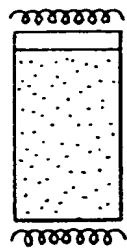


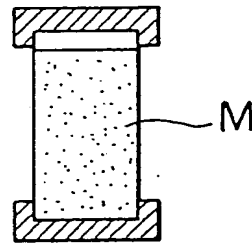
FIG. 31(a)      FIG. 31(b)

Heated



Heated

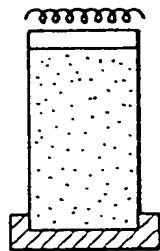
Heat-retained



Heat-retained

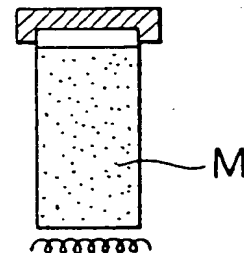
FIG. 31(c)      FIG. 31(d)

Heated



Heat-retained

Heat-retained



Heated

FIG. 32

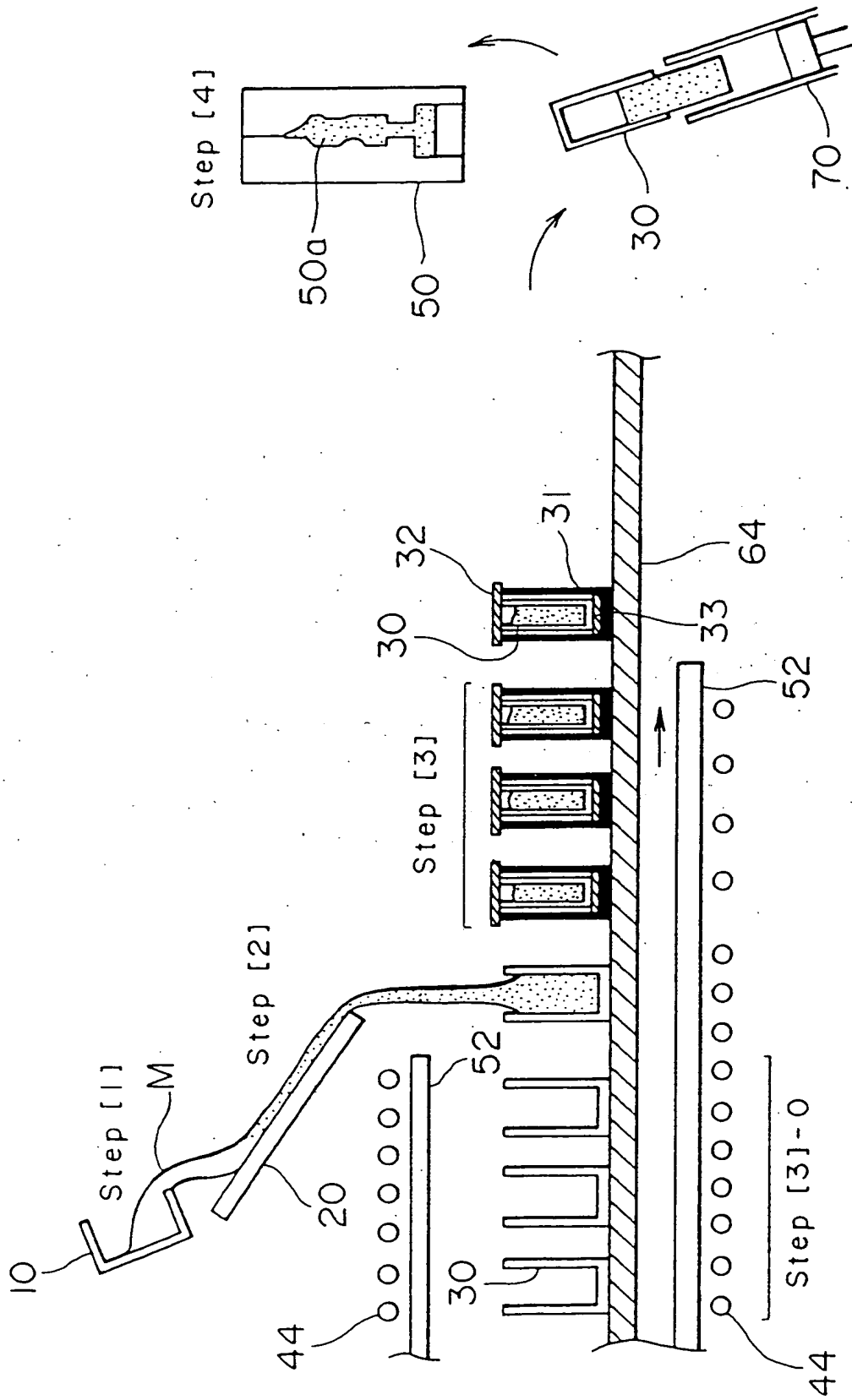


FIG. 33

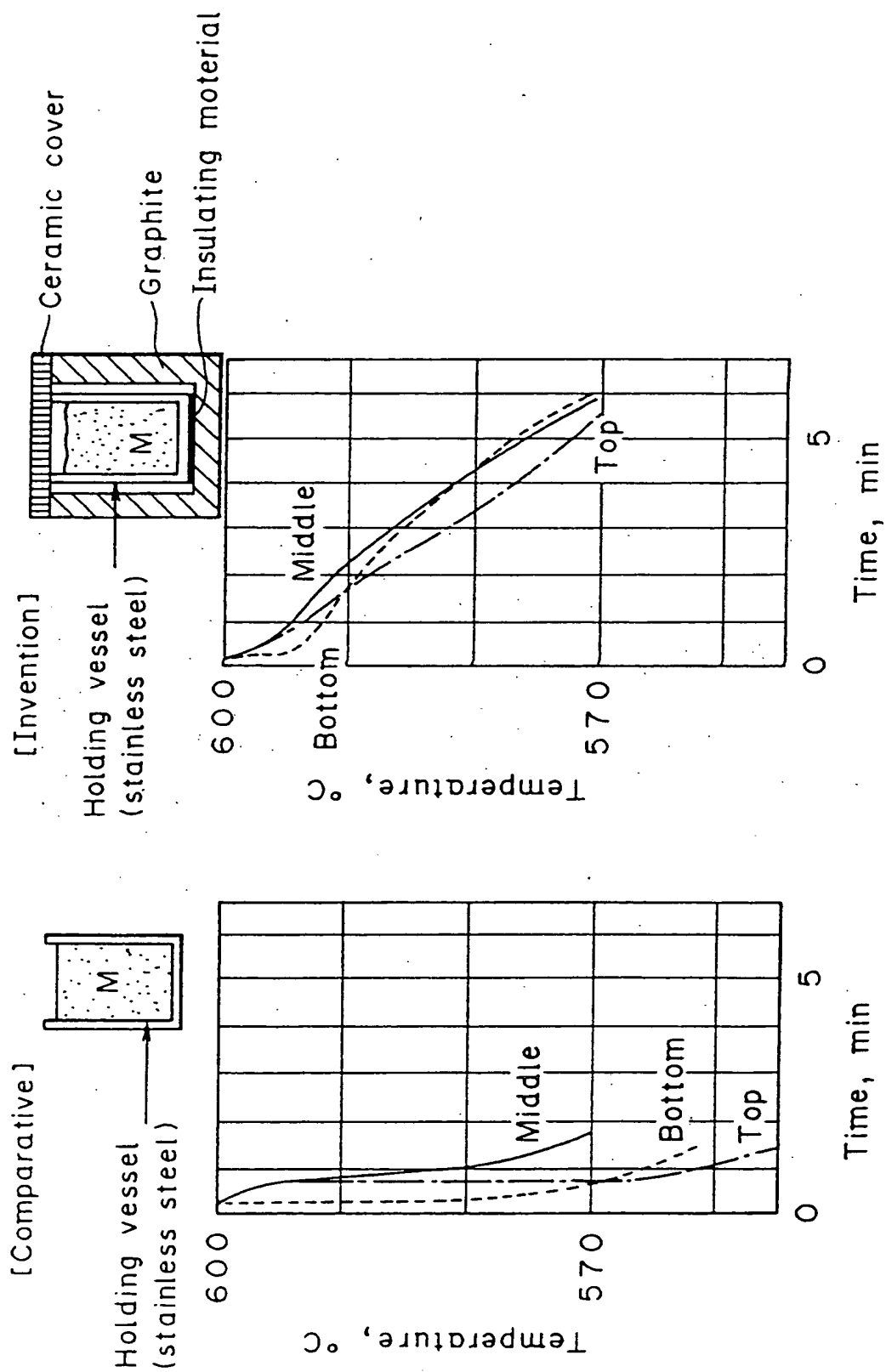
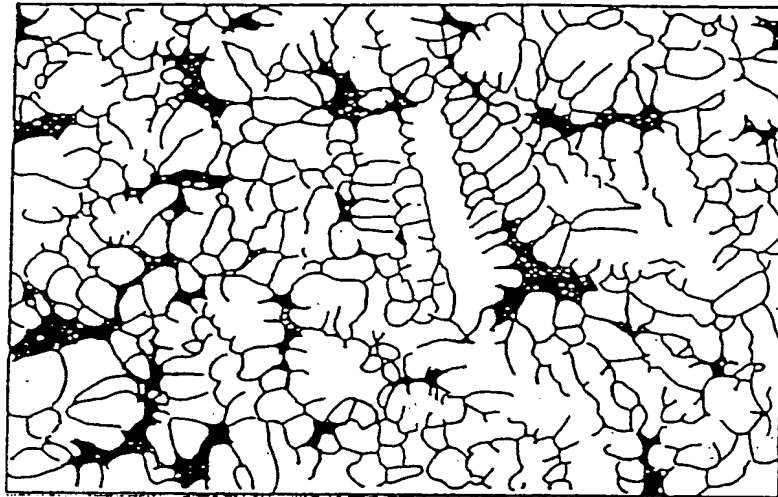


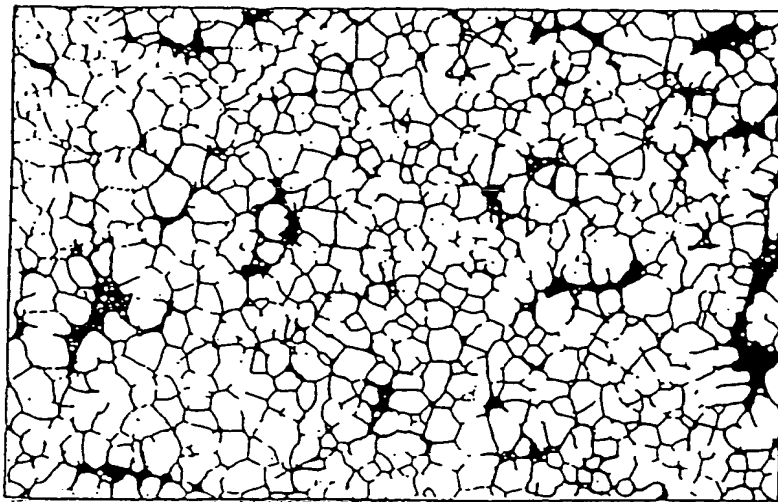
FIG. 34 Prior Art



200  $\mu$ m



FIG. 35



200  $\mu$ m



FIG. 36

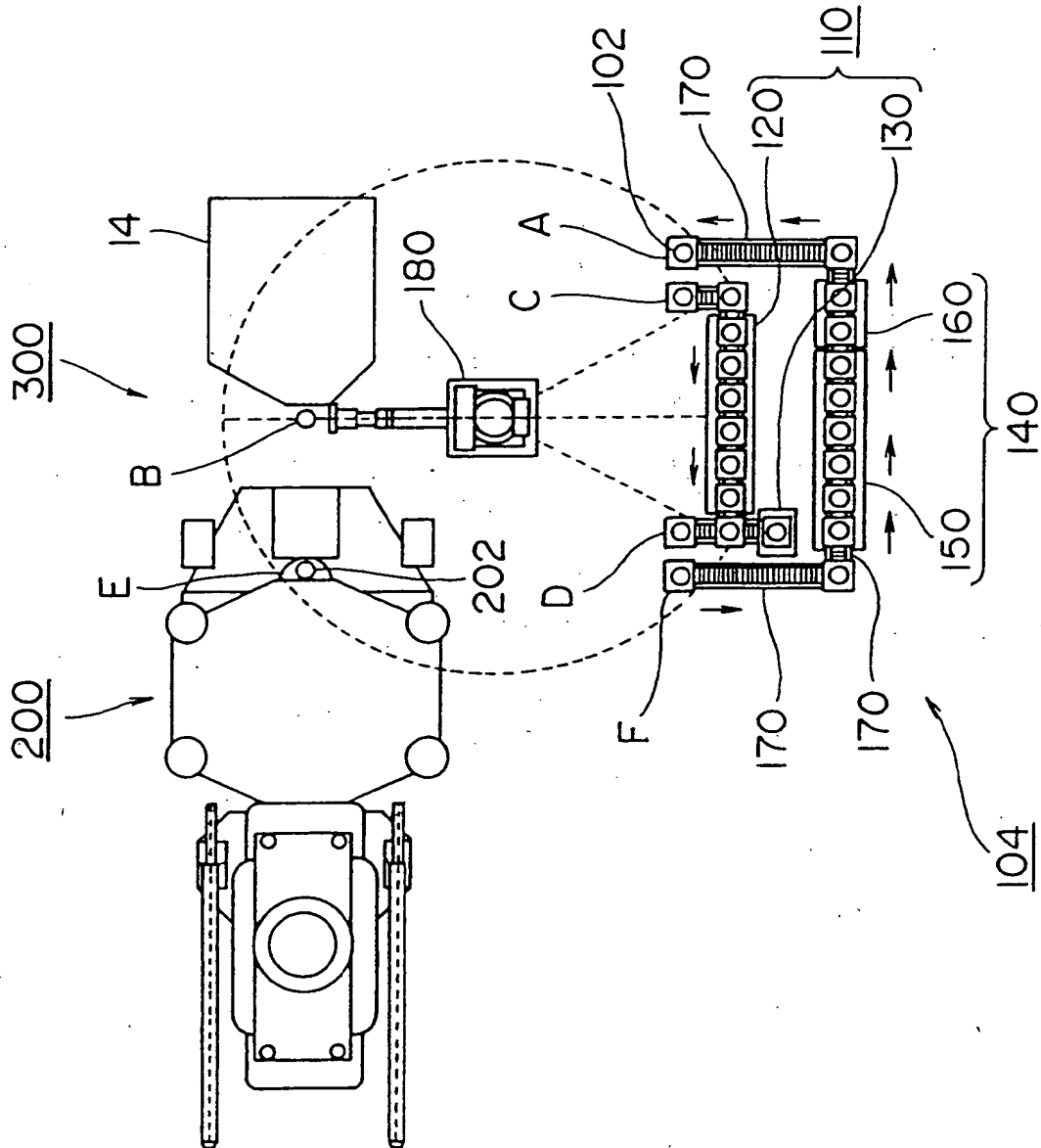


FIG. 37

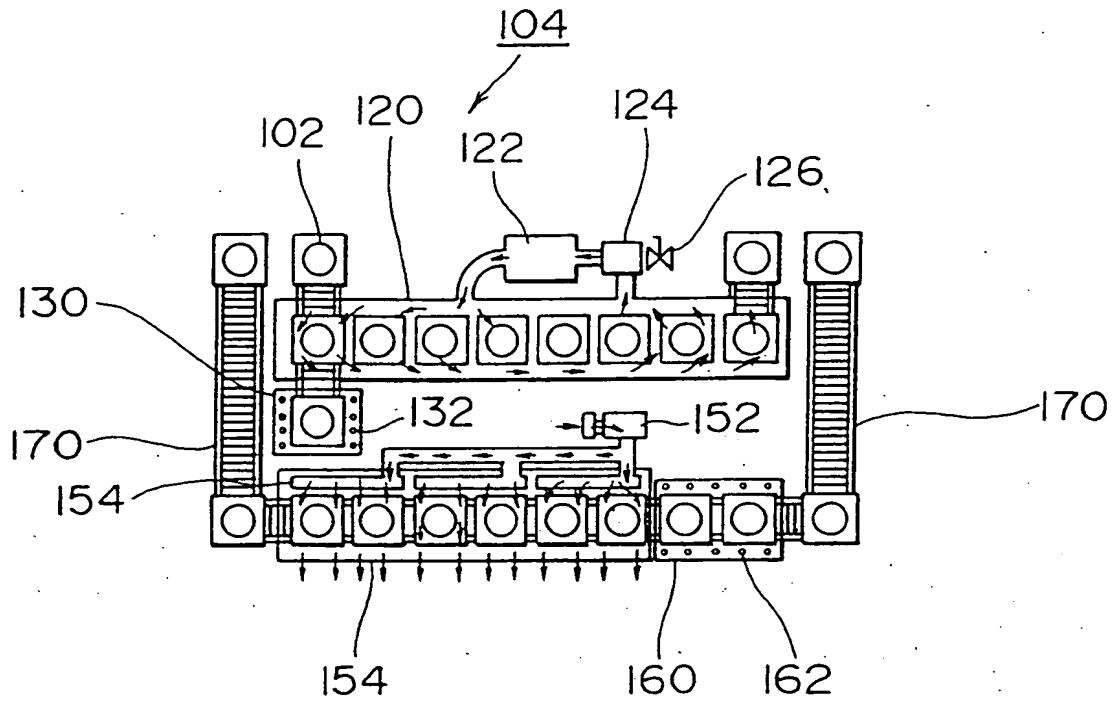


FIG. 38

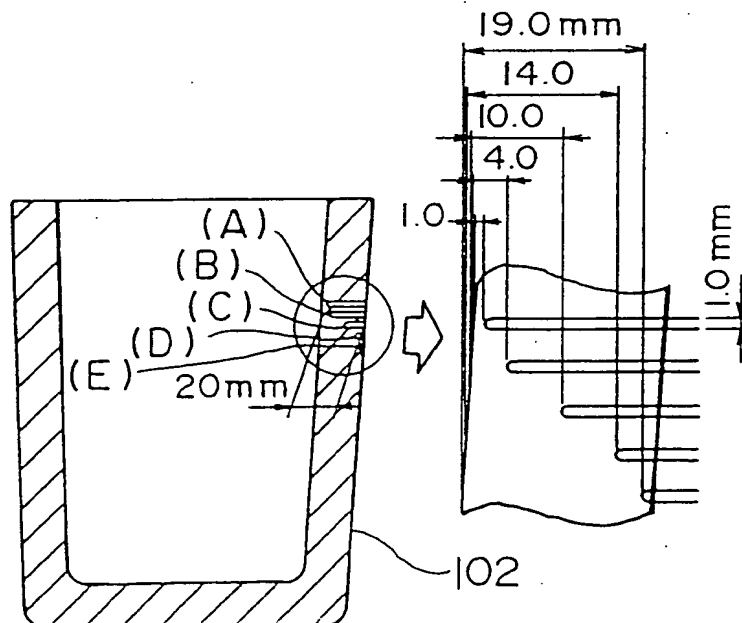




FIG. 39

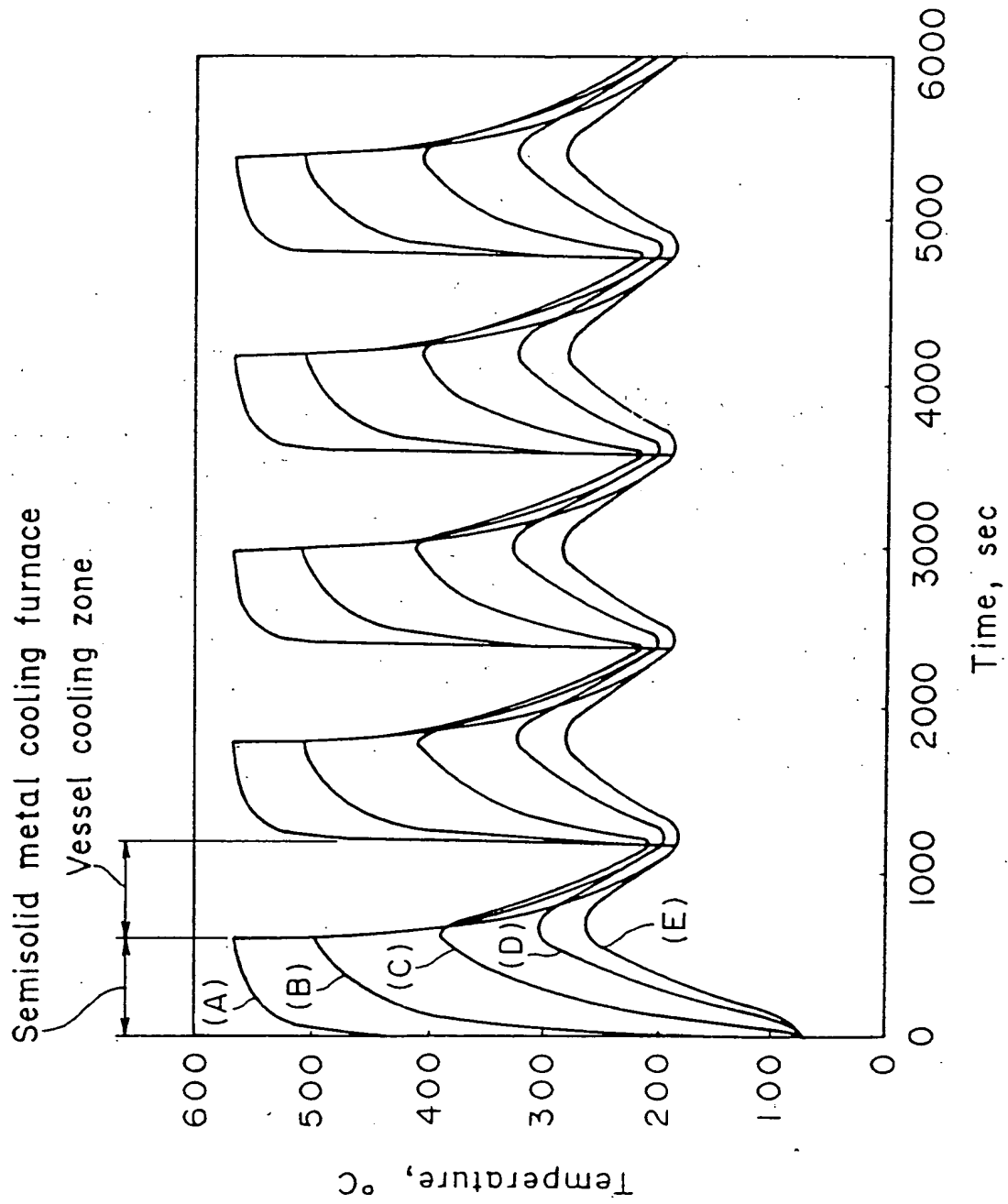


FIG. 40

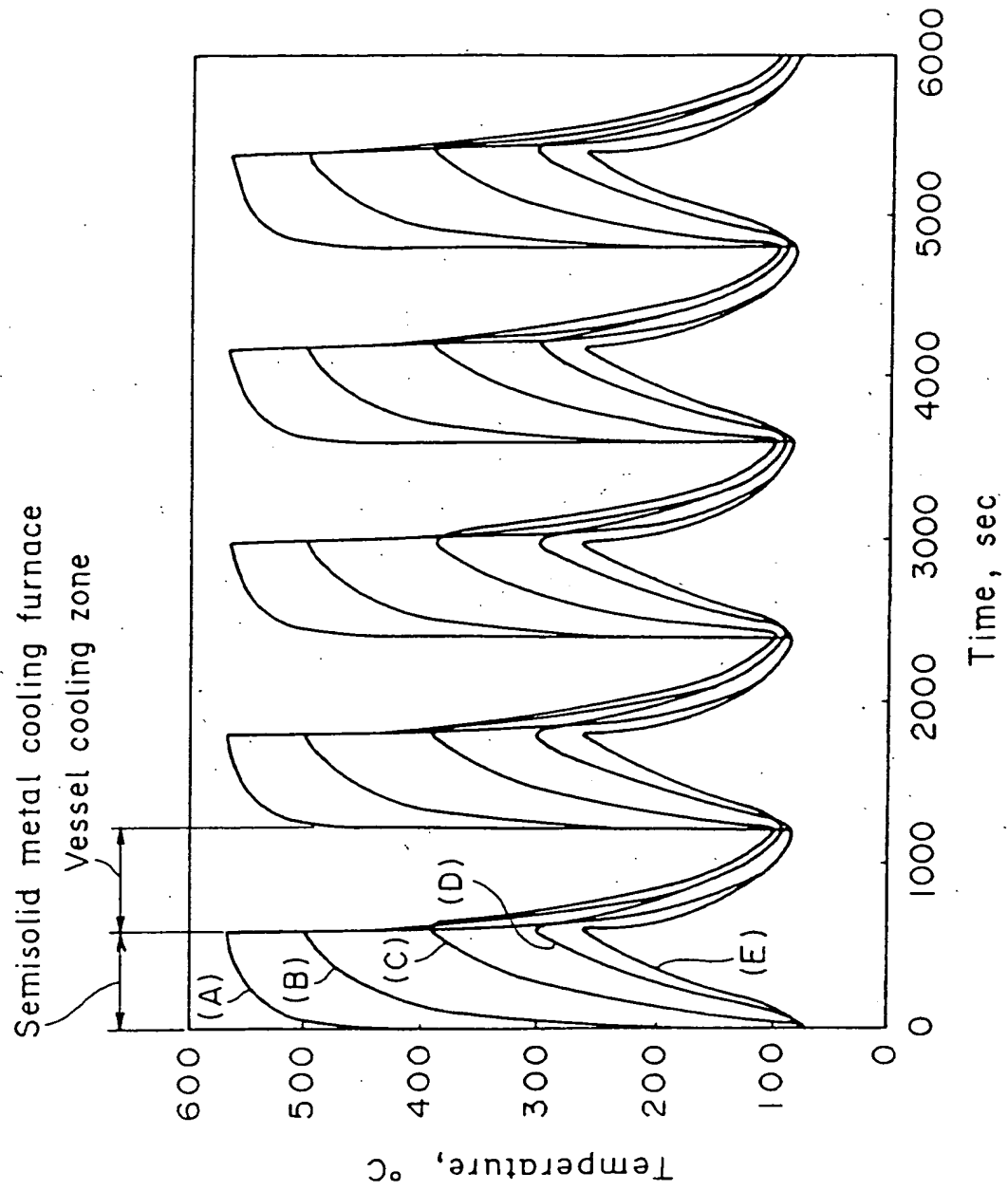


FIG. 41

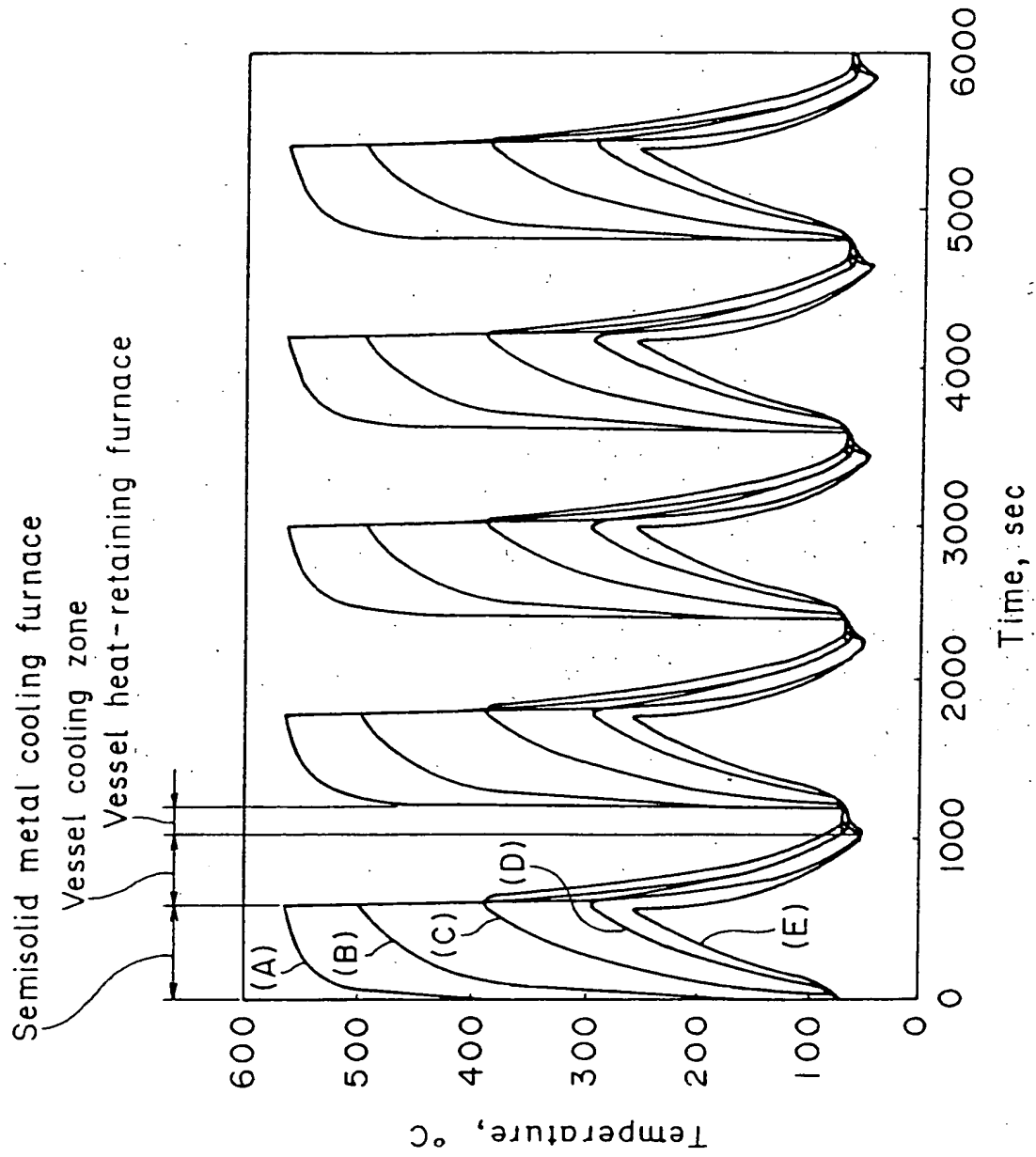


FIG. 42

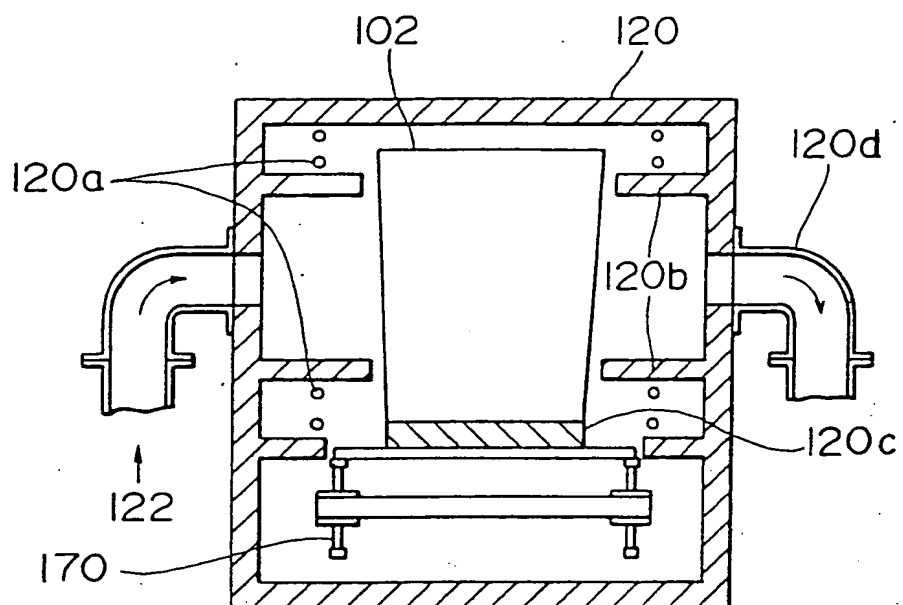


FIG. 43

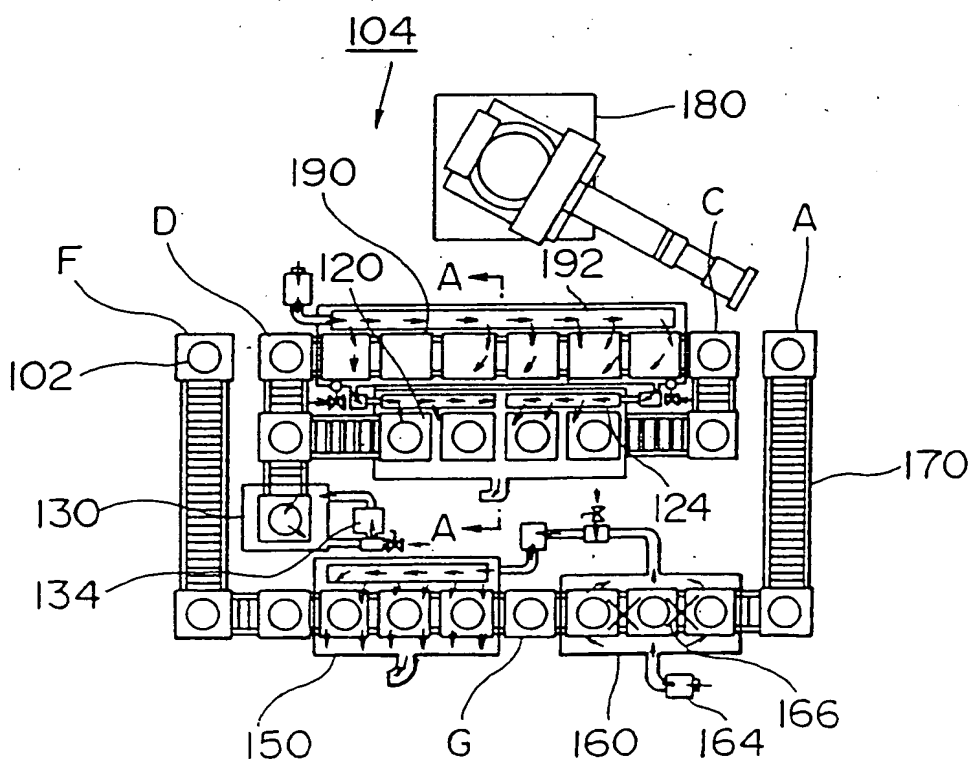


FIG. 44

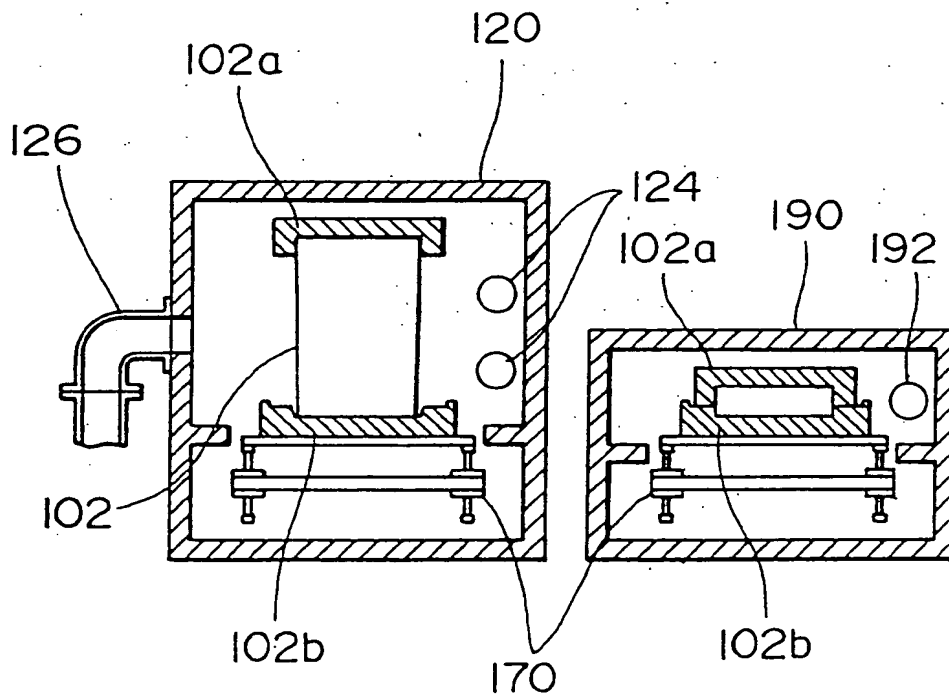


FIG. 45

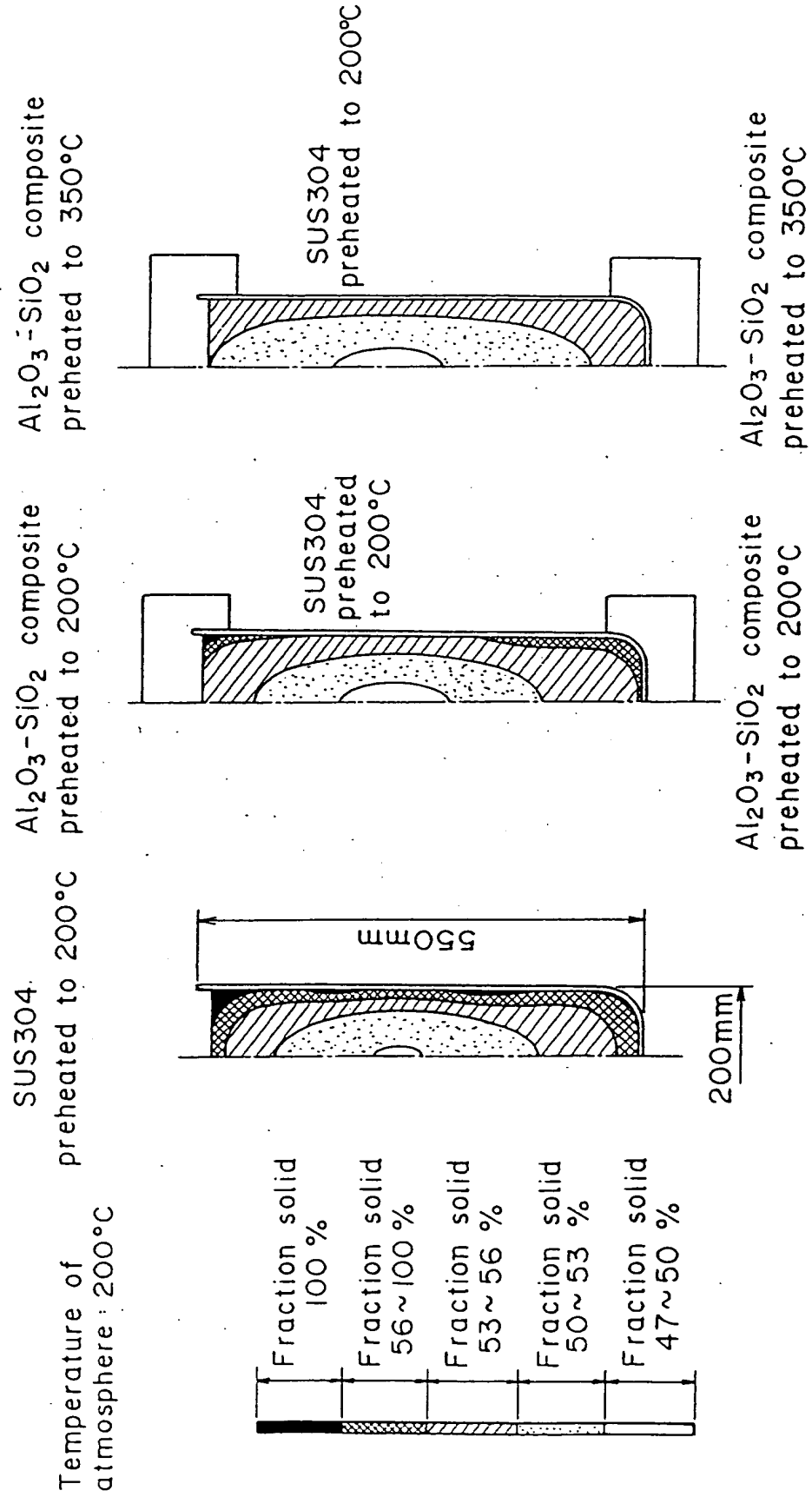


FIG. 46

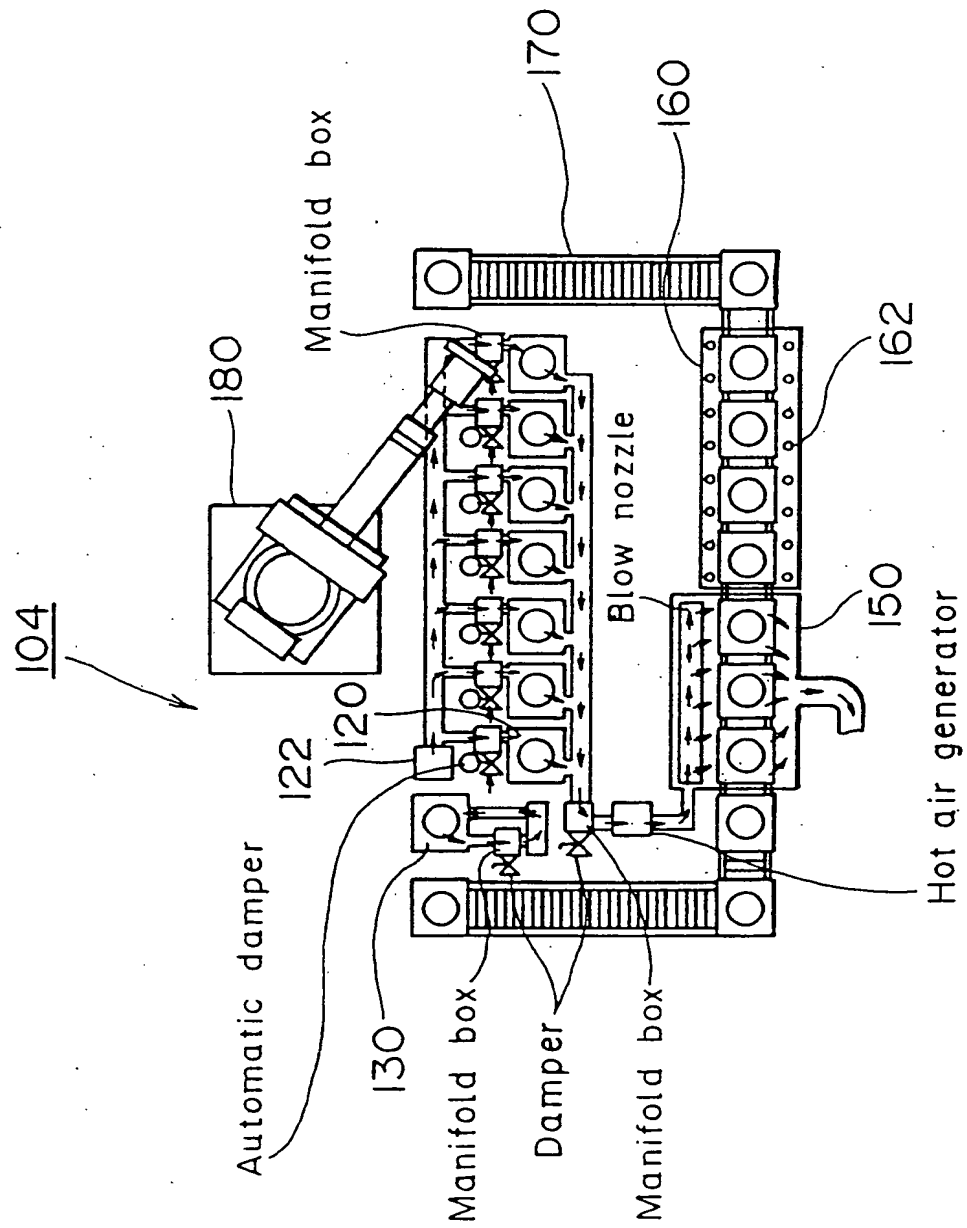


FIG. 47

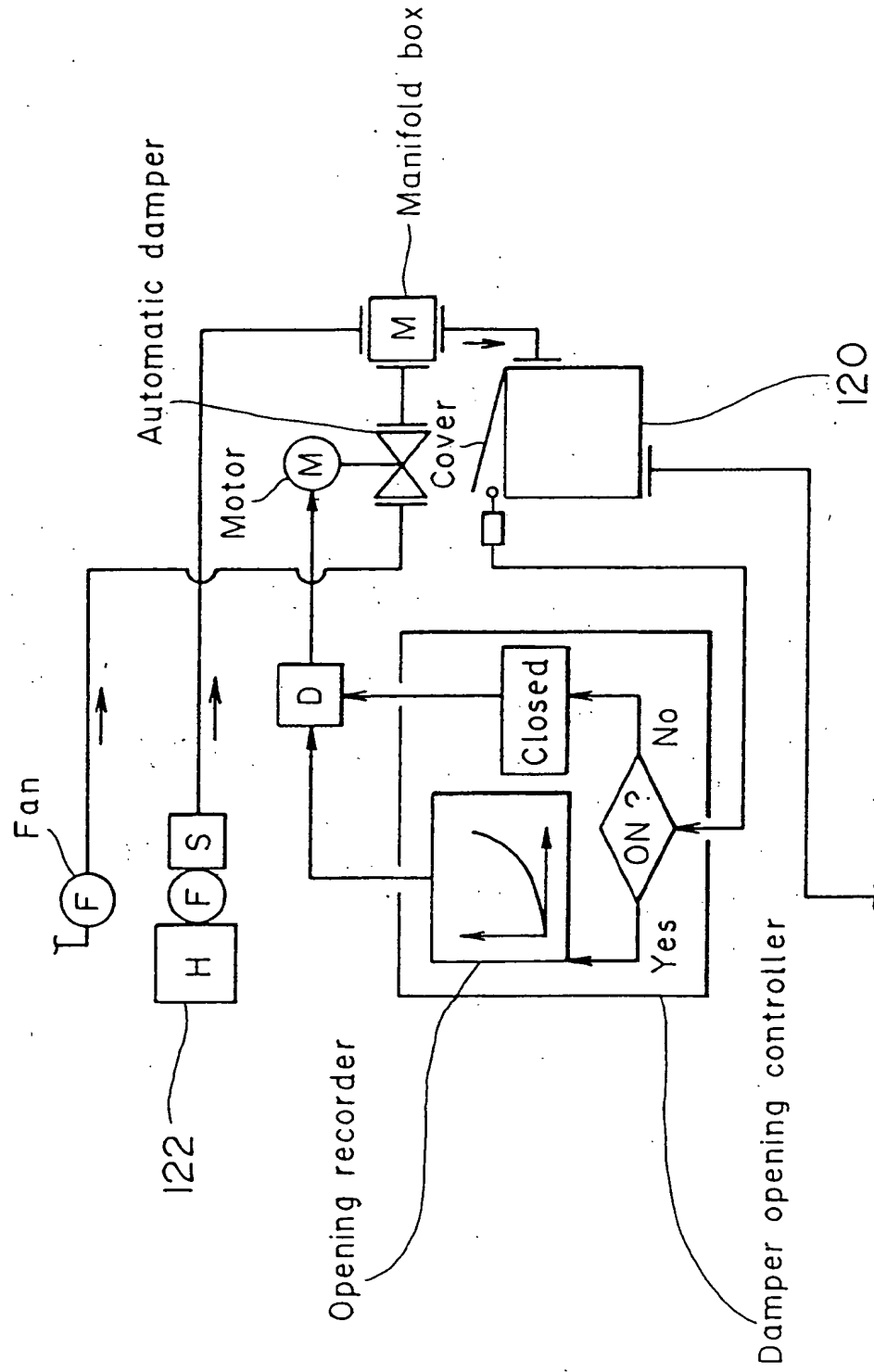




FIG. 48

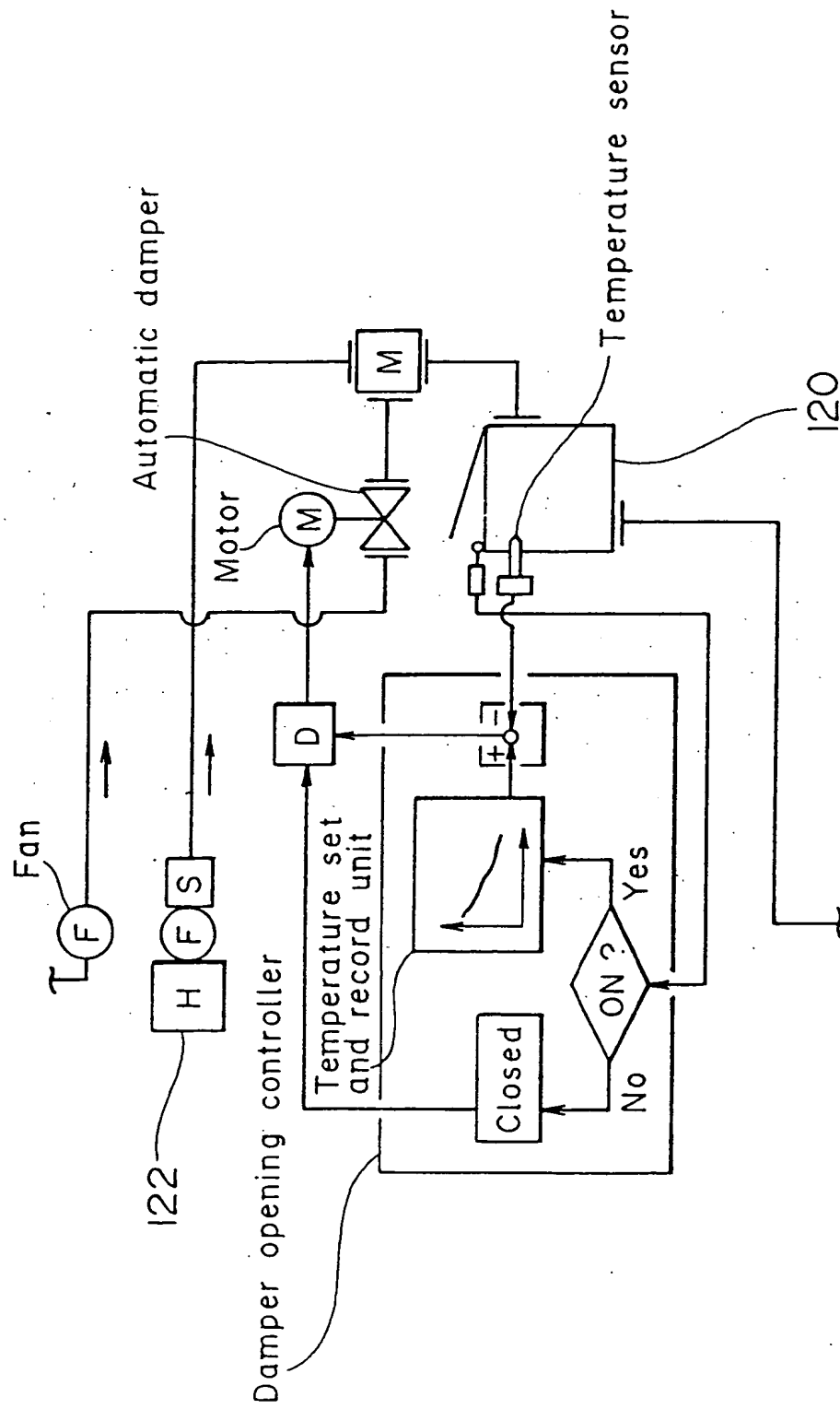
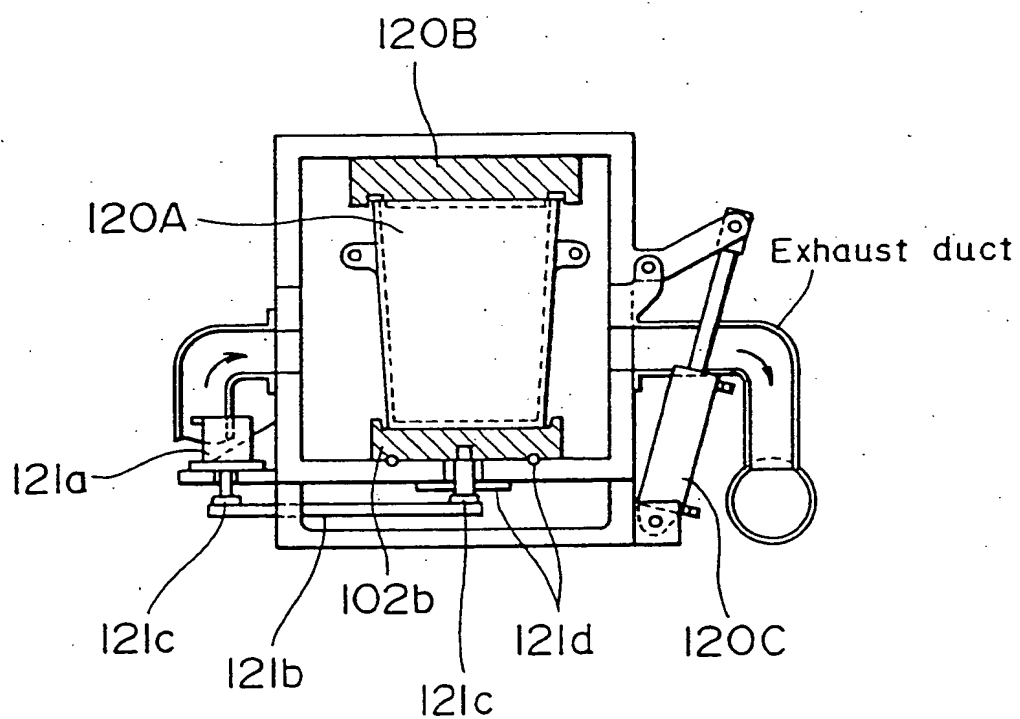


FIG. 49



F/G. 50

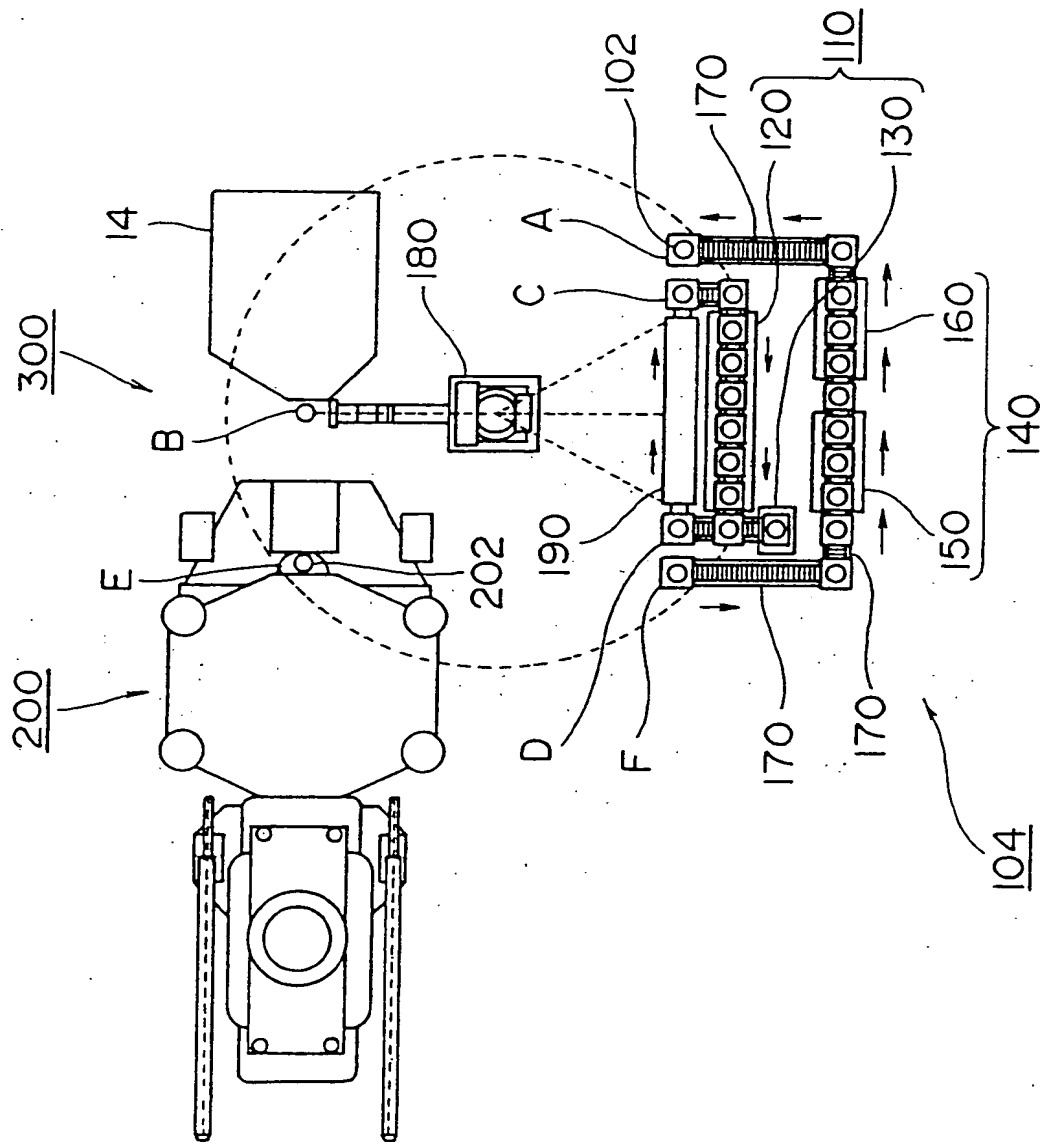


FIG. 5I

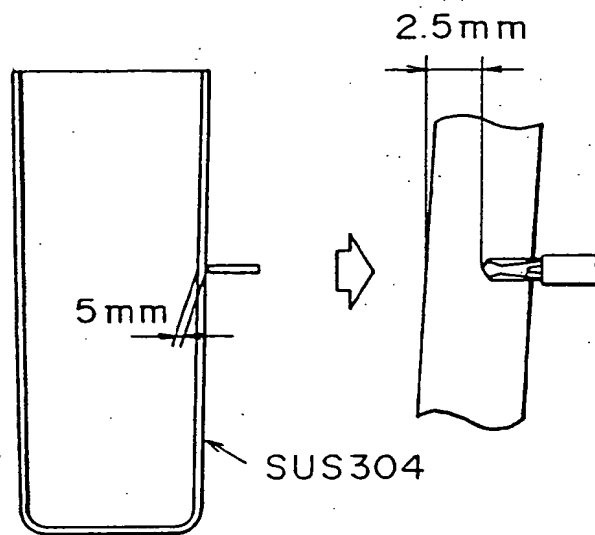


FIG. 52

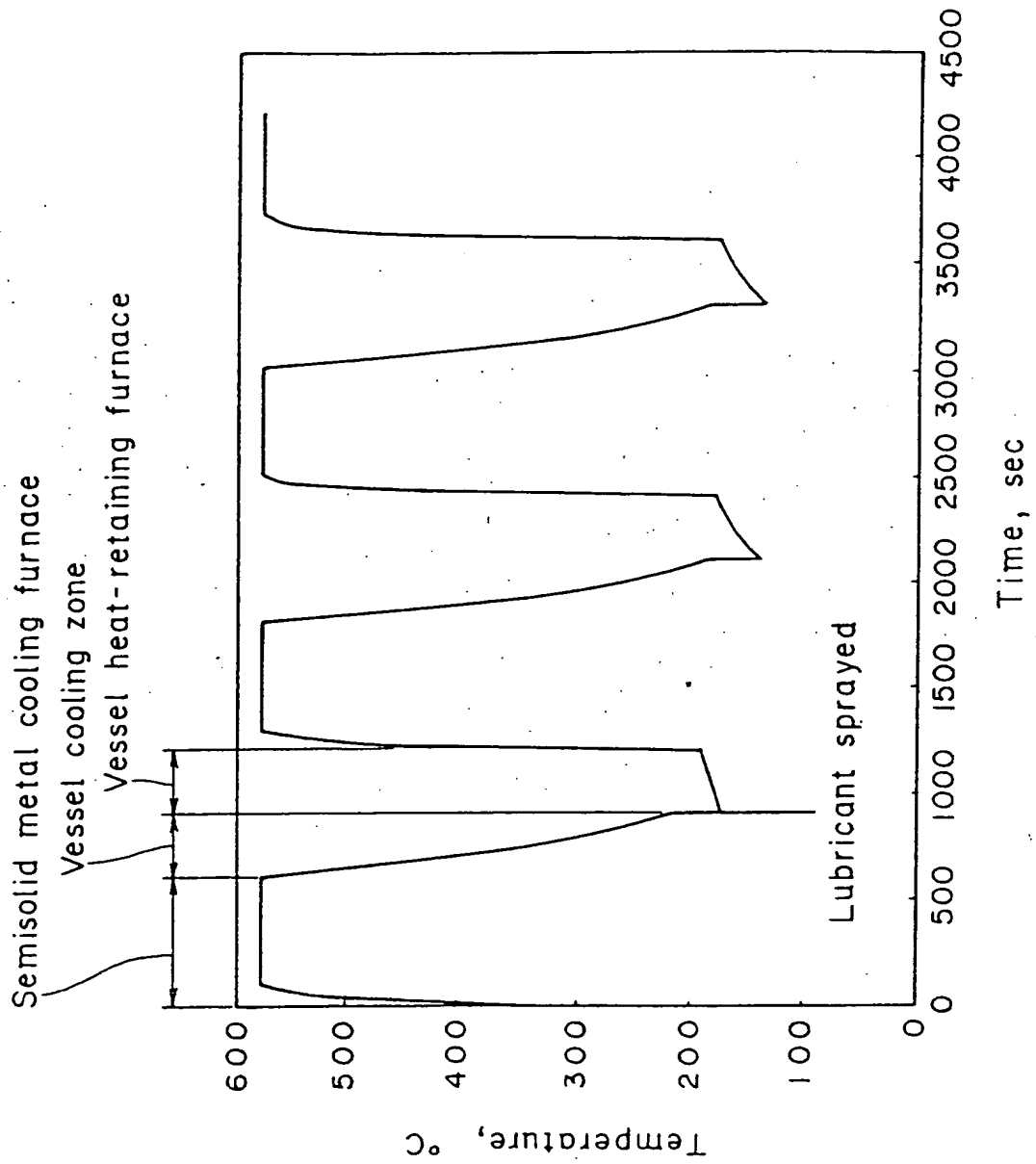


FIG. 53

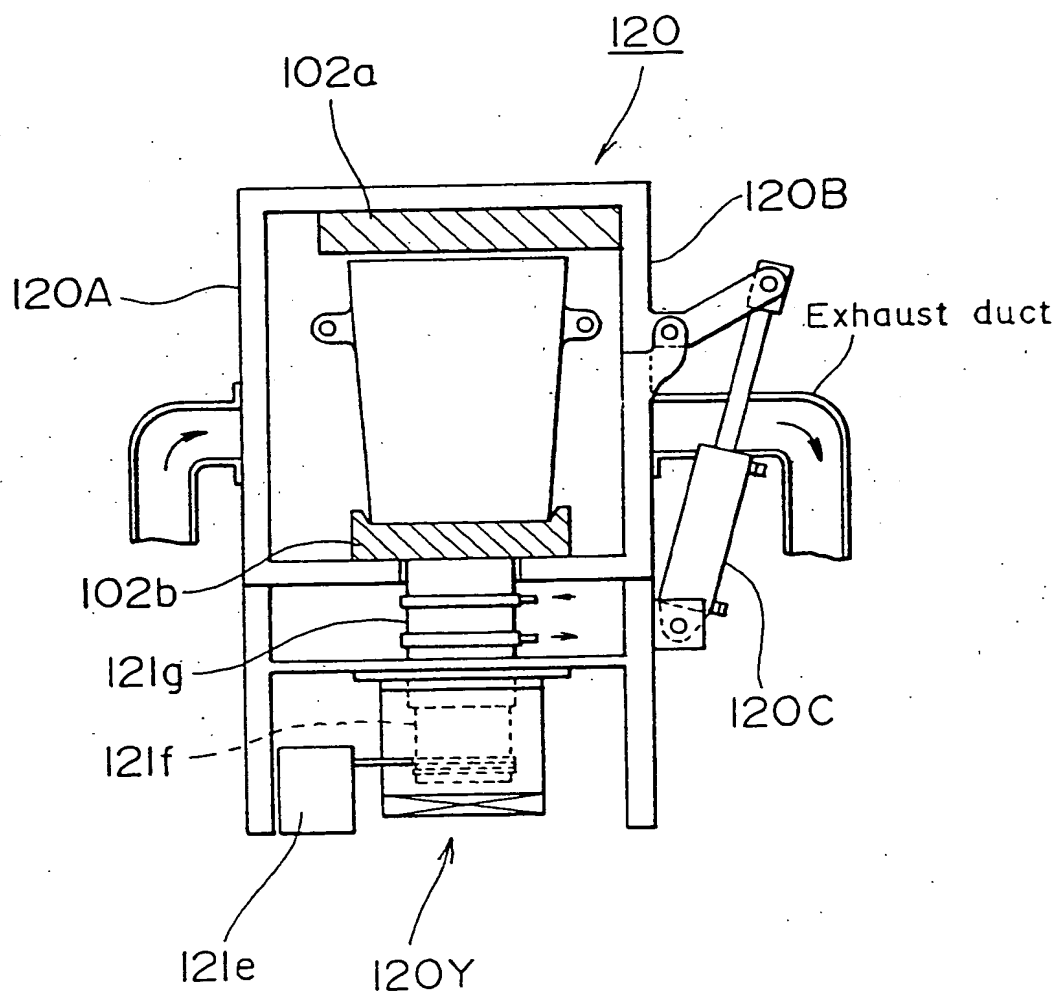


FIG. 54

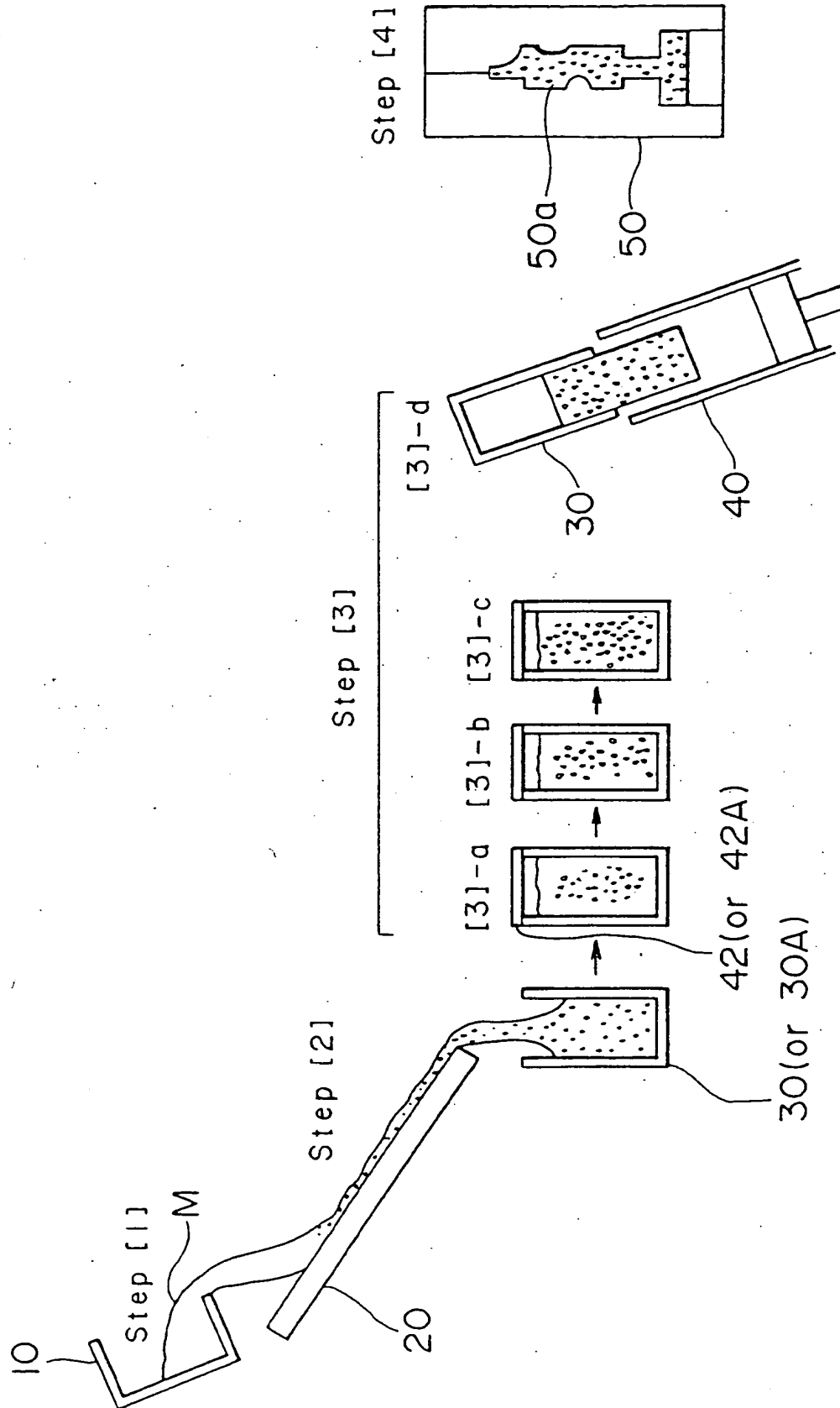


FIG. 55

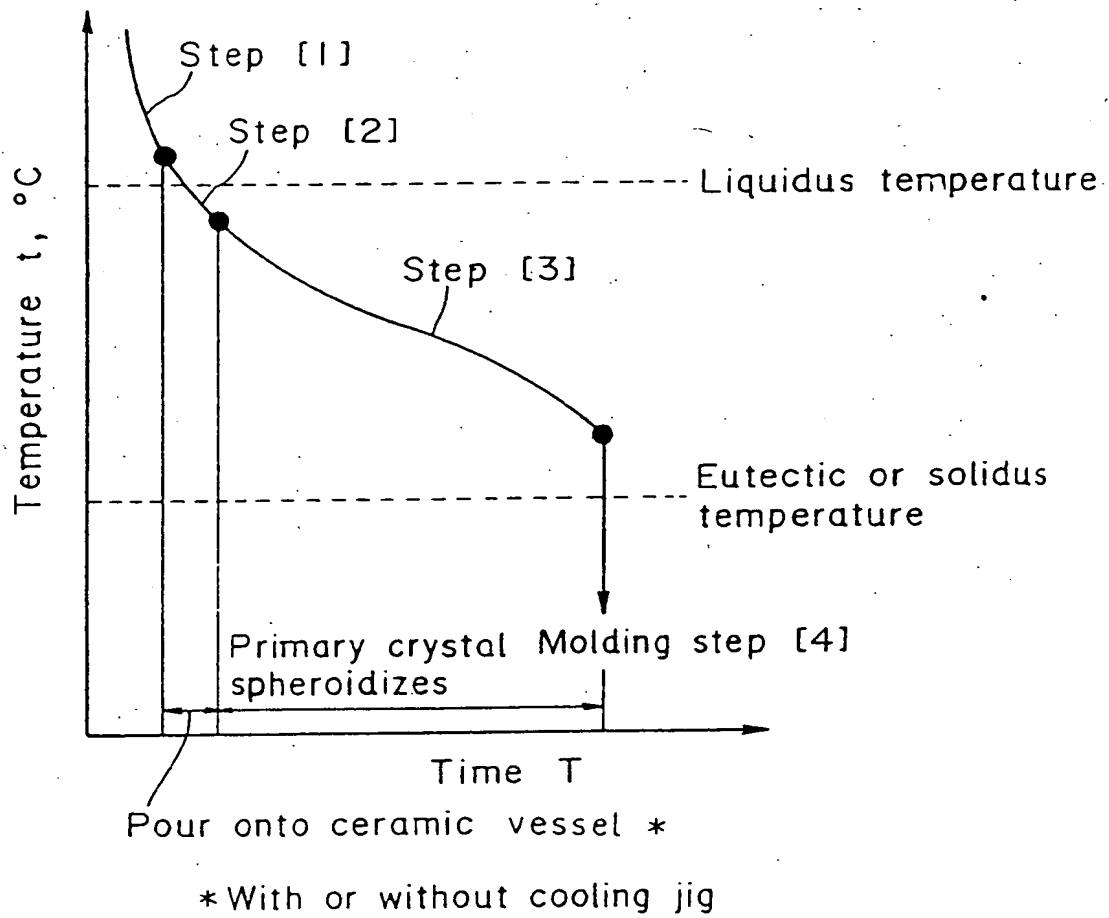




FIG. 56

Superheated to no more than 100°C  
(without cooling jig) or 300°C  
(with cooling jig) above liquidus temperature

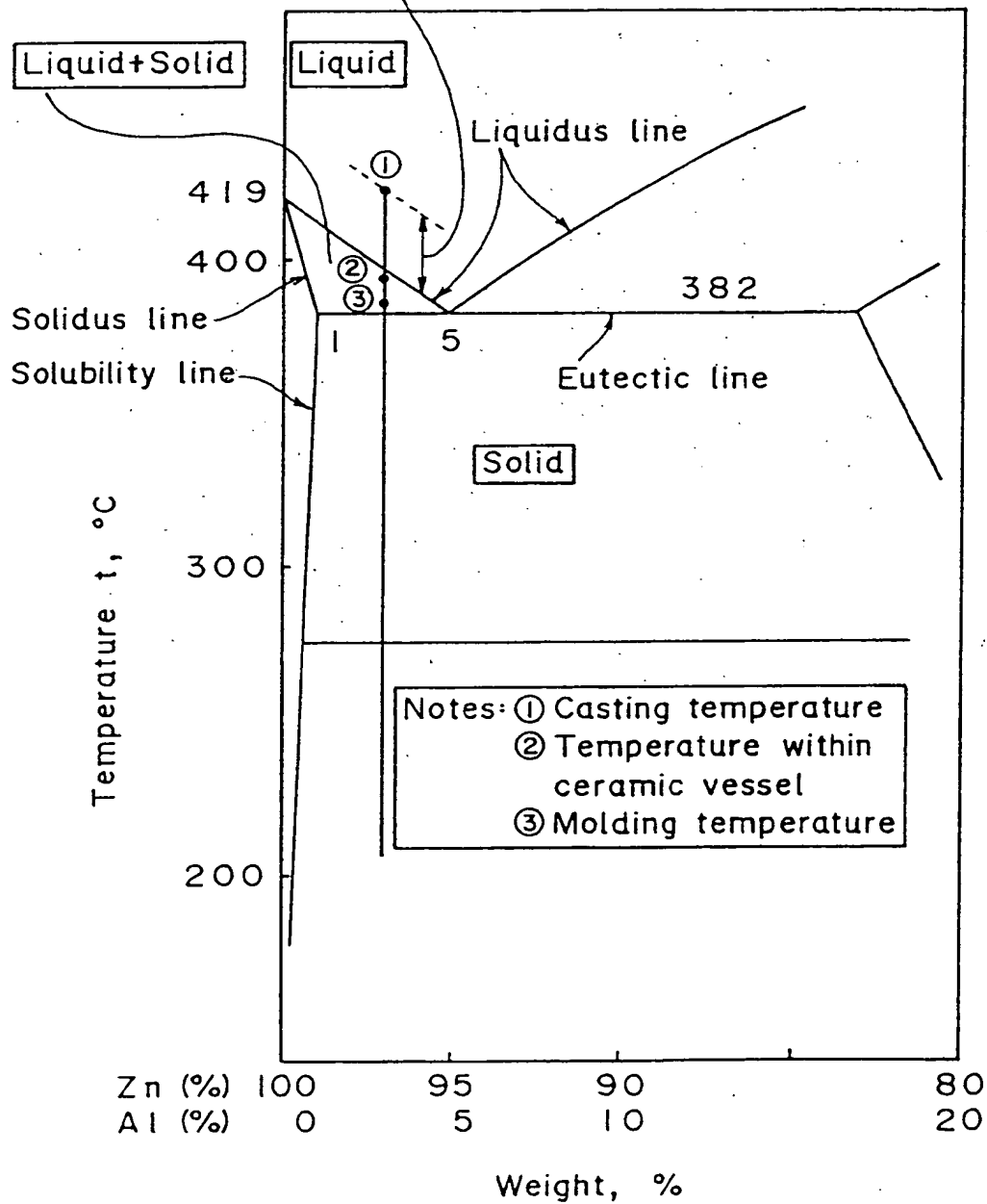


FIG. 57

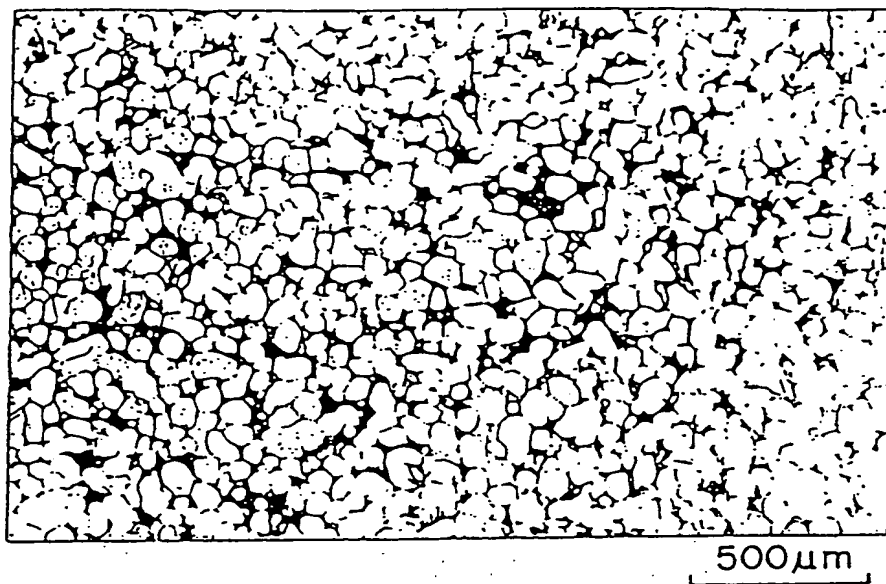
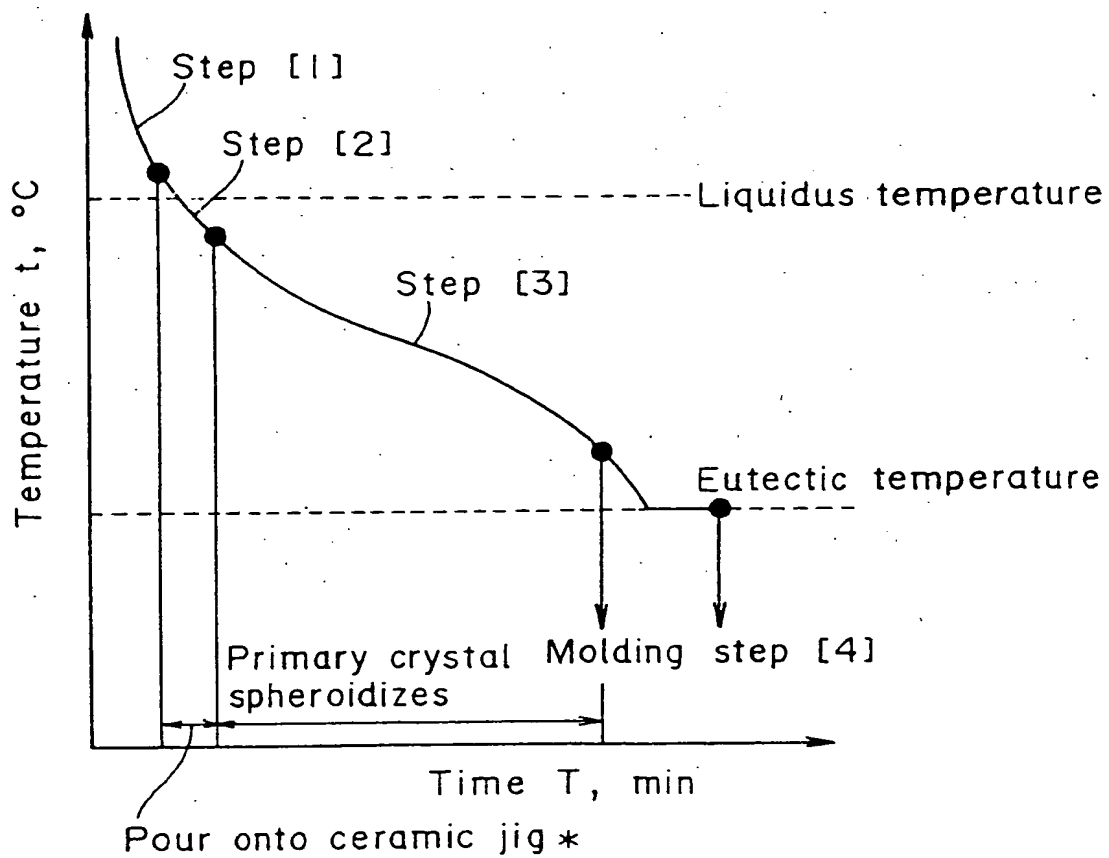


FIG. 58 Prior Art



FIG. 59



\*With or without cooling jig

FIG. 60

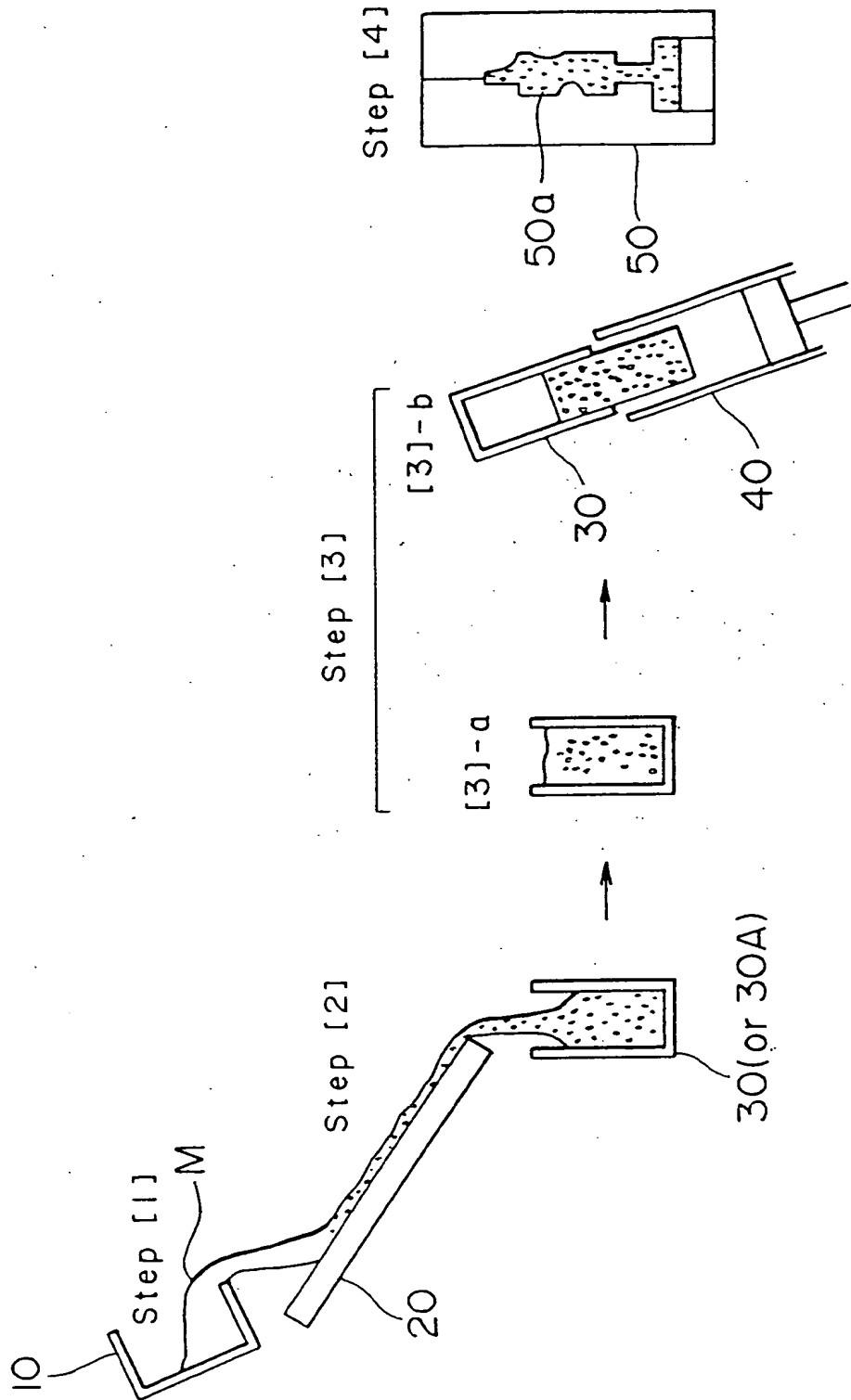


FIG. 61

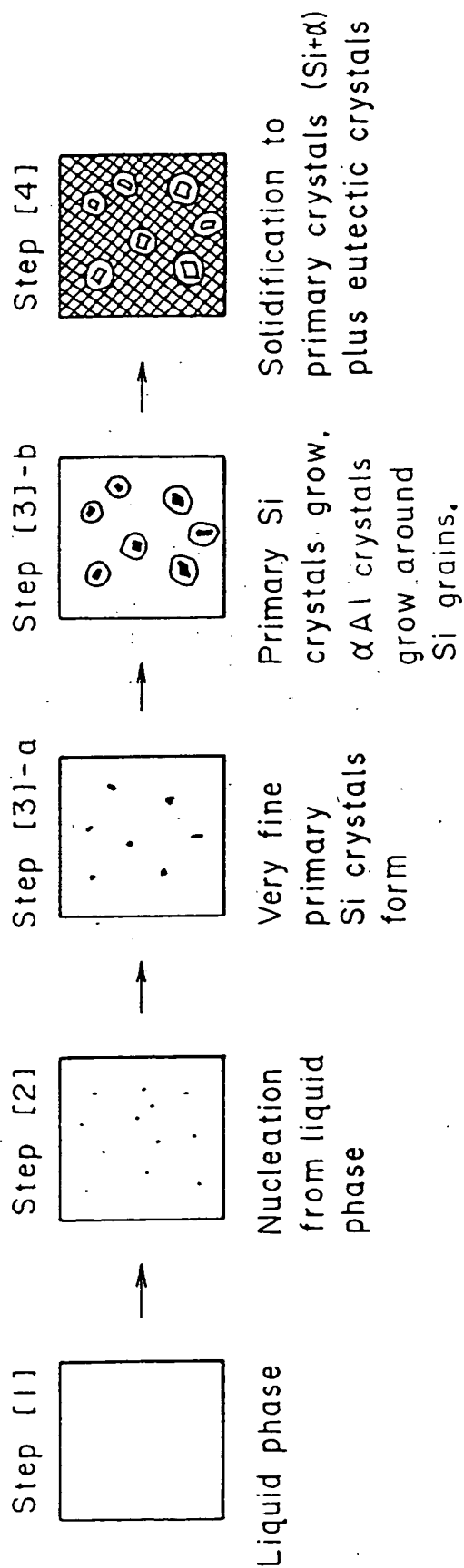


FIG. 62

Superheated to no more than 300°C  
(with cooling jig) above liquidus temperature

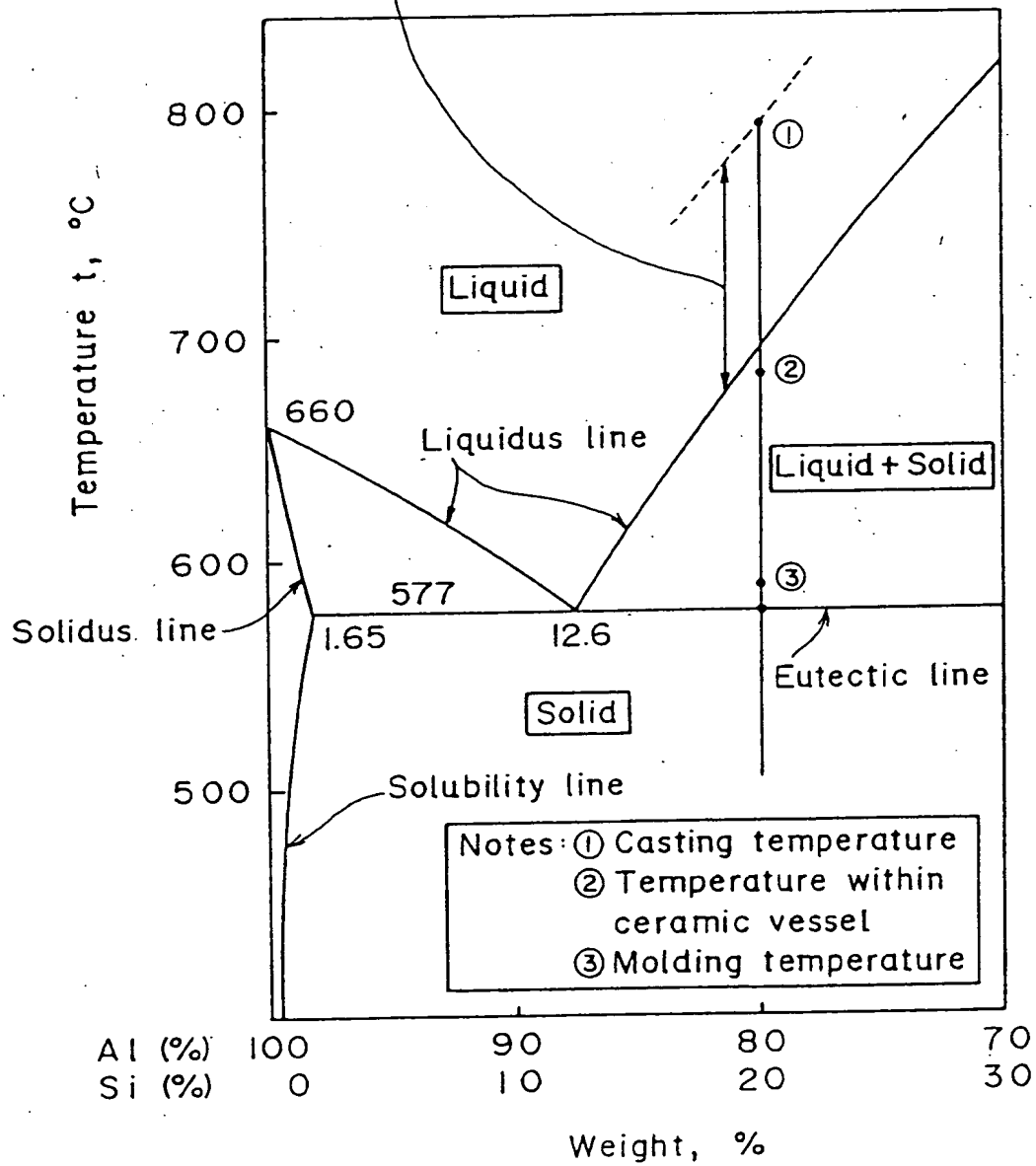


FIG. 63

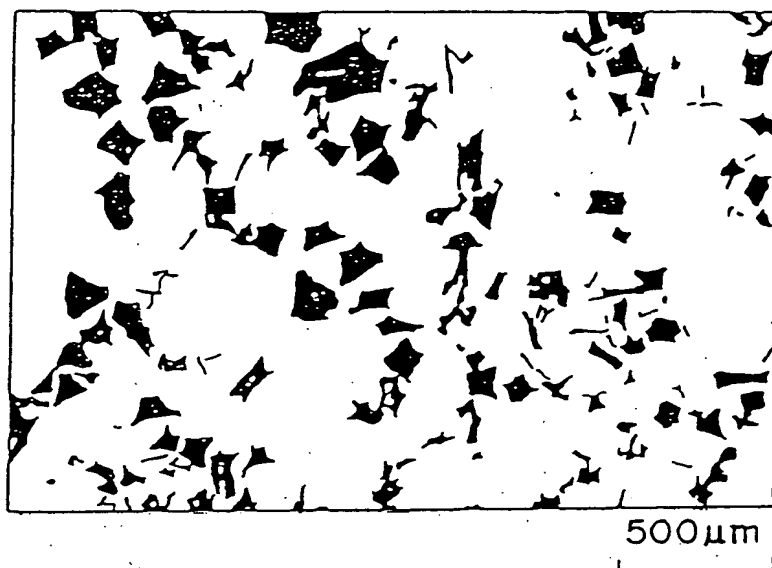


FIG. 64 Prior Art



FIG. 65

Superheated to no more than 100°C  
(without cooling jig) or 300°C  
(with cooling jig) above liquidus temperature

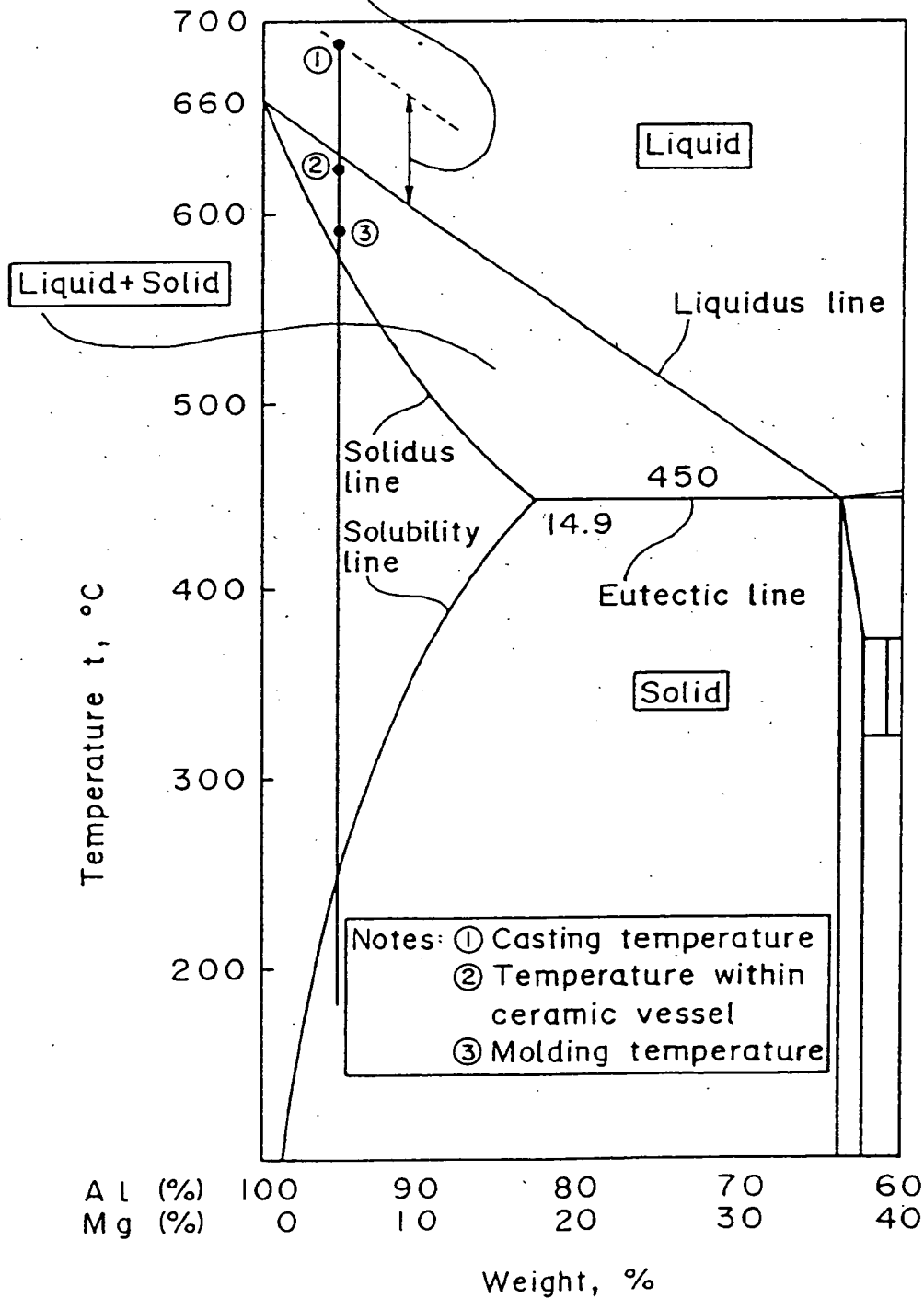




FIG. 66

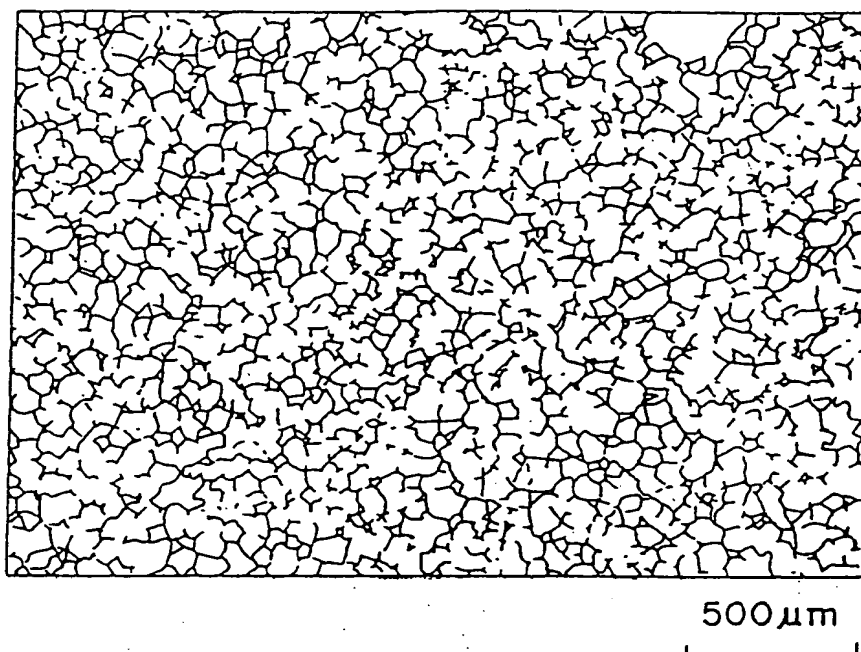


FIG. 67 Prior Art

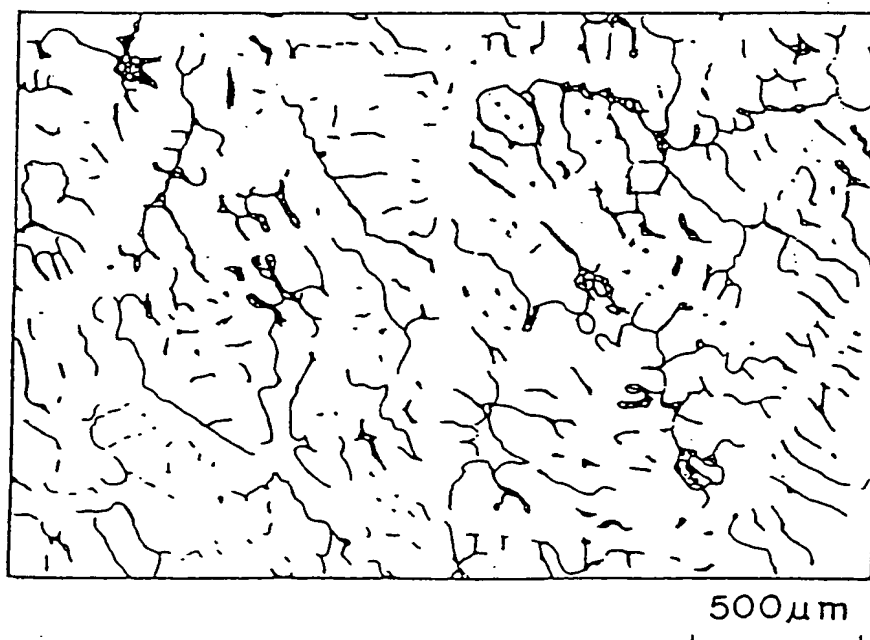


FIG. 68

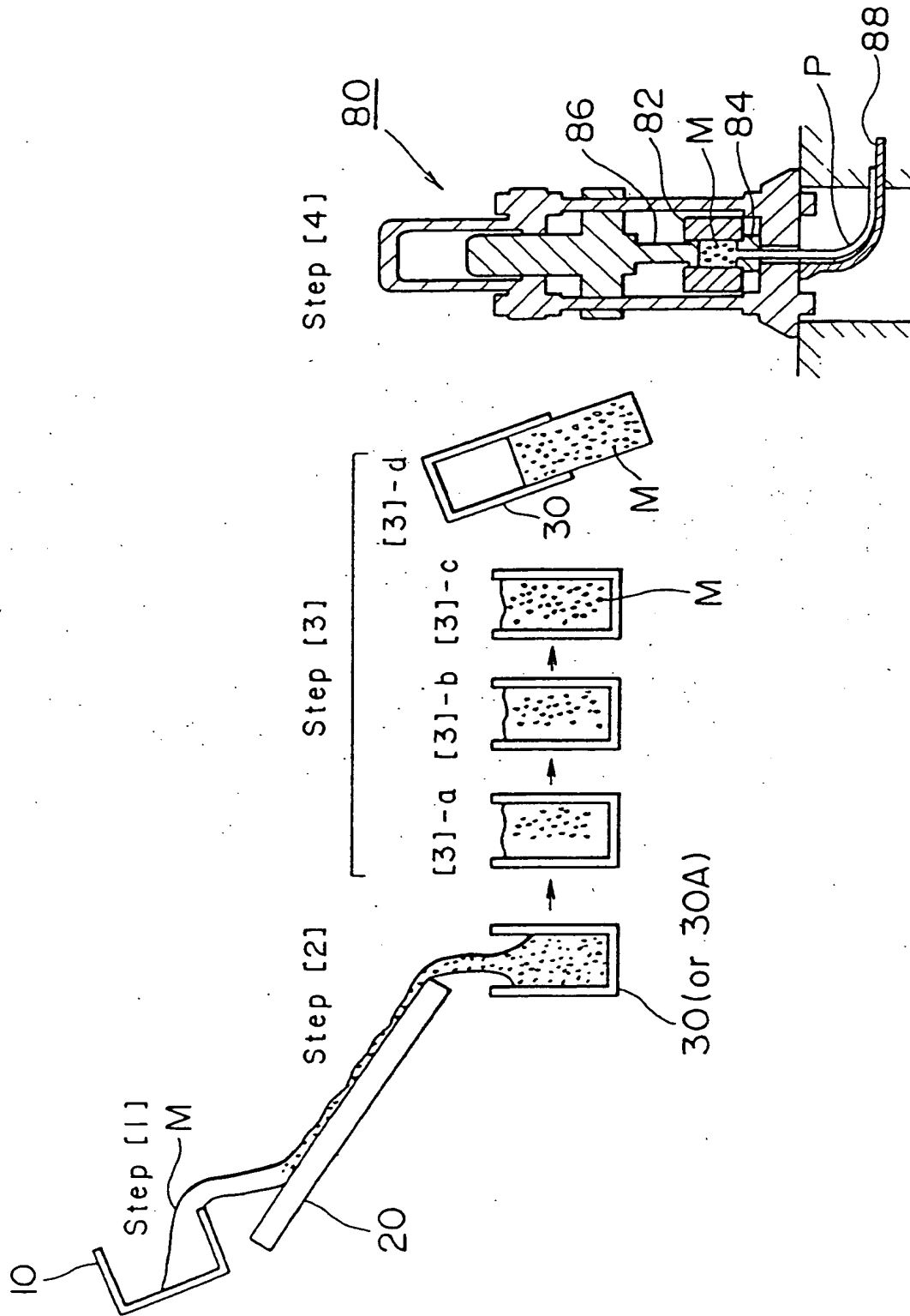
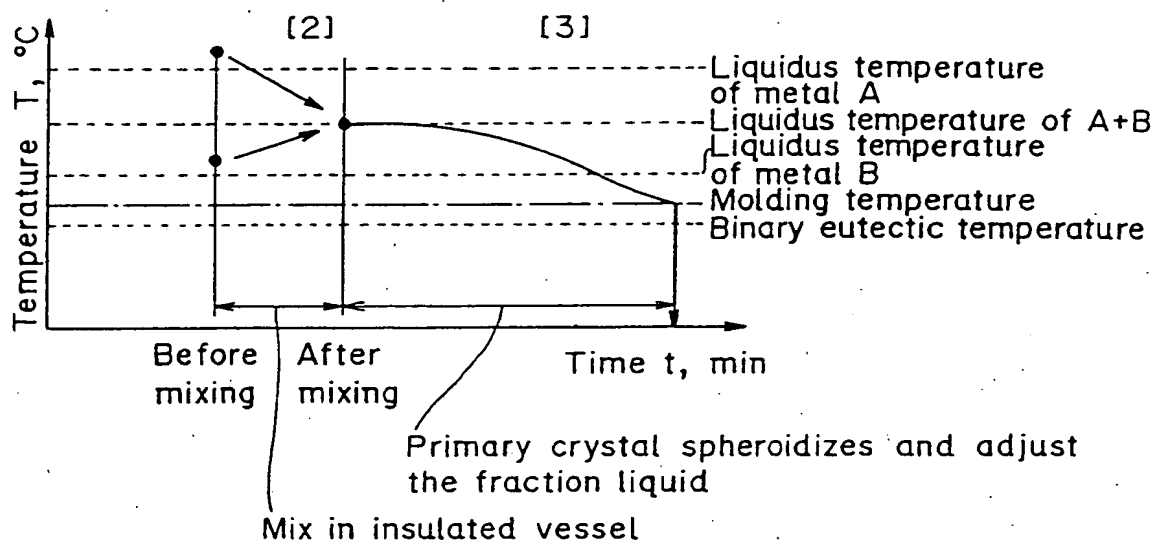


FIG. 69

(a) From a mixture of two molten metals A and B



(b) From two molten metals A and B (including crystal nuclei) that were mixed after cooling with cooling jig

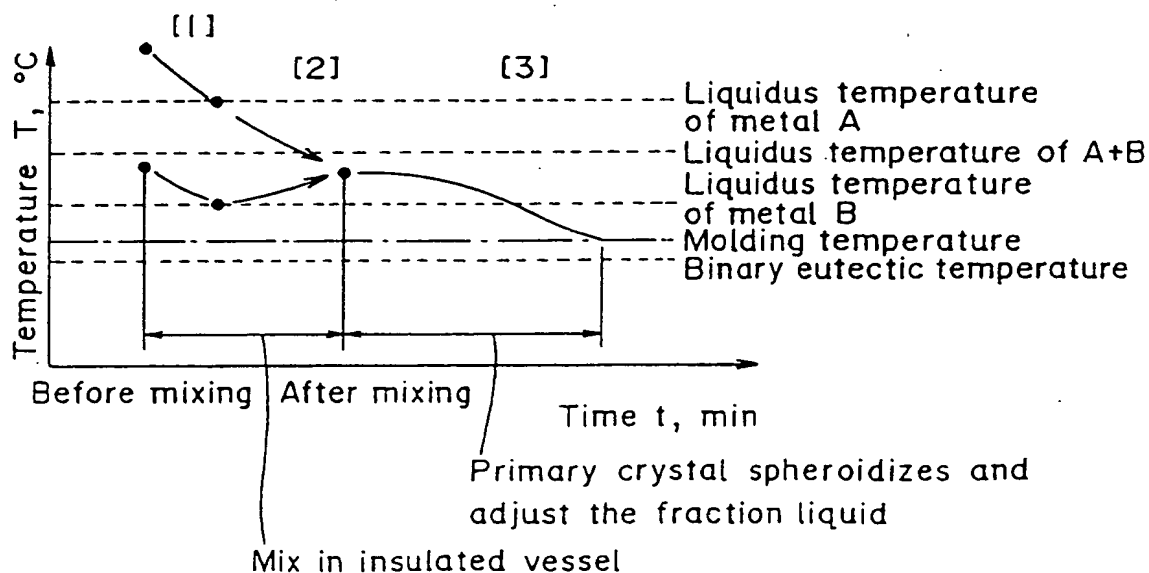


FIG. 70

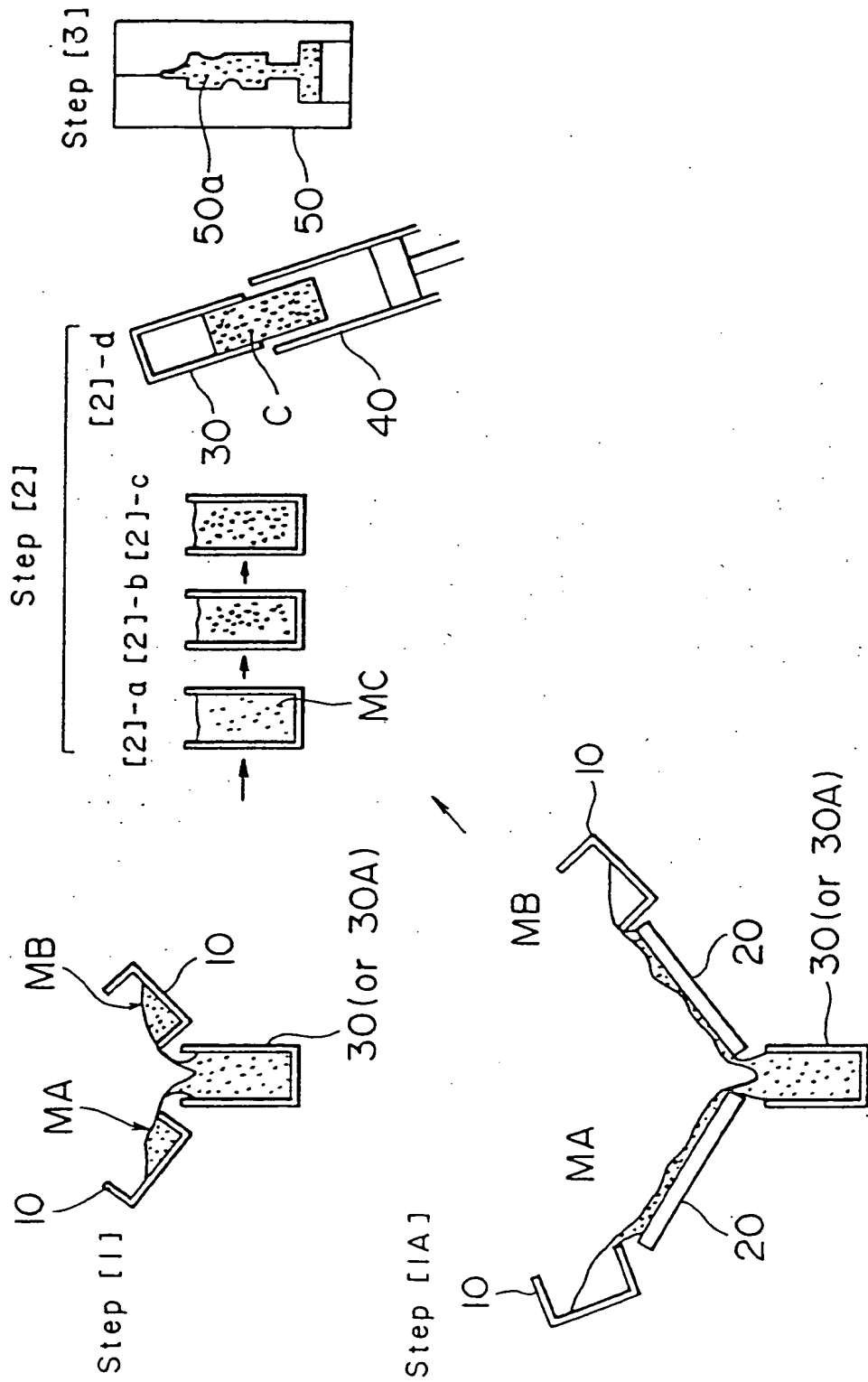


FIG. 71

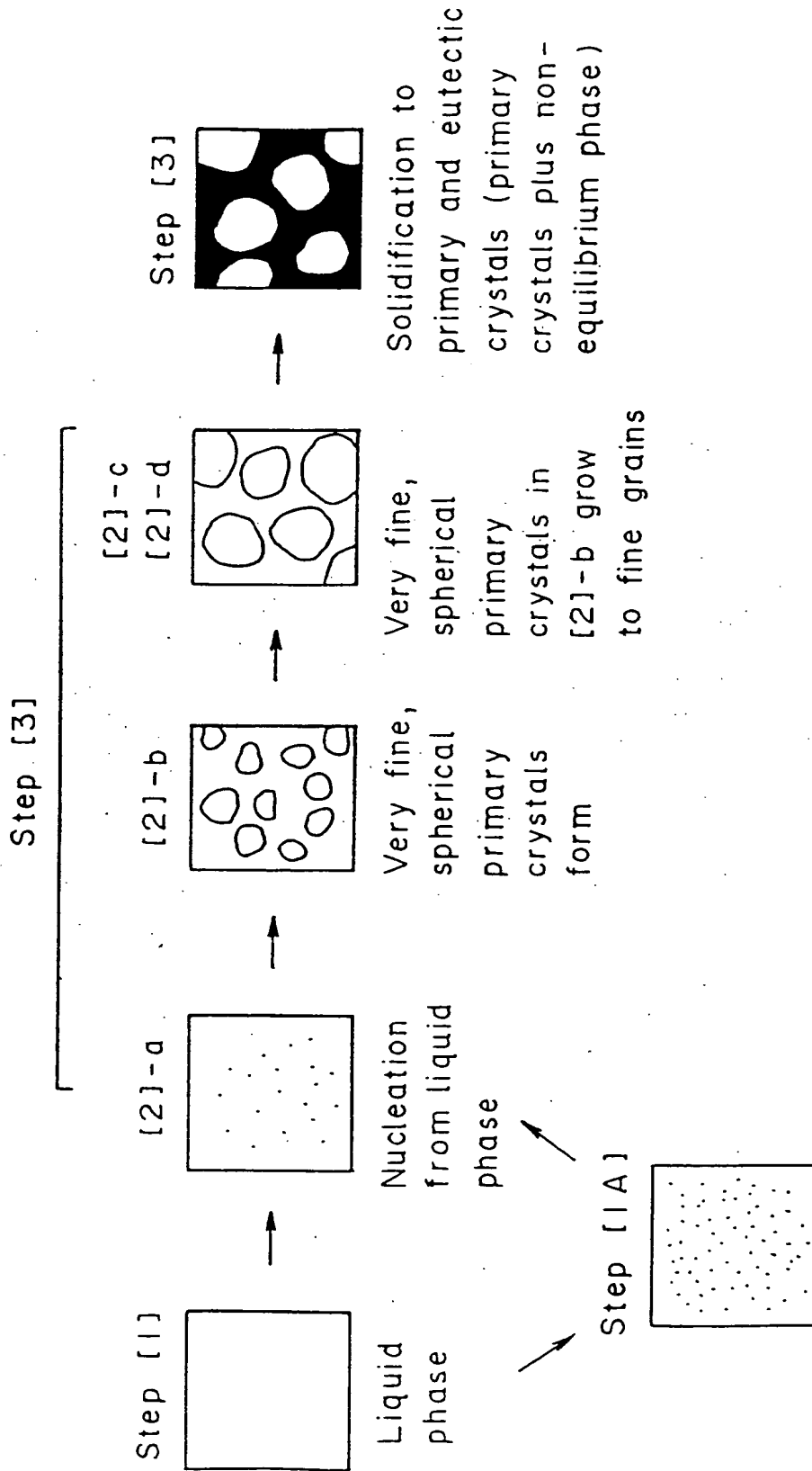


FIG. 72

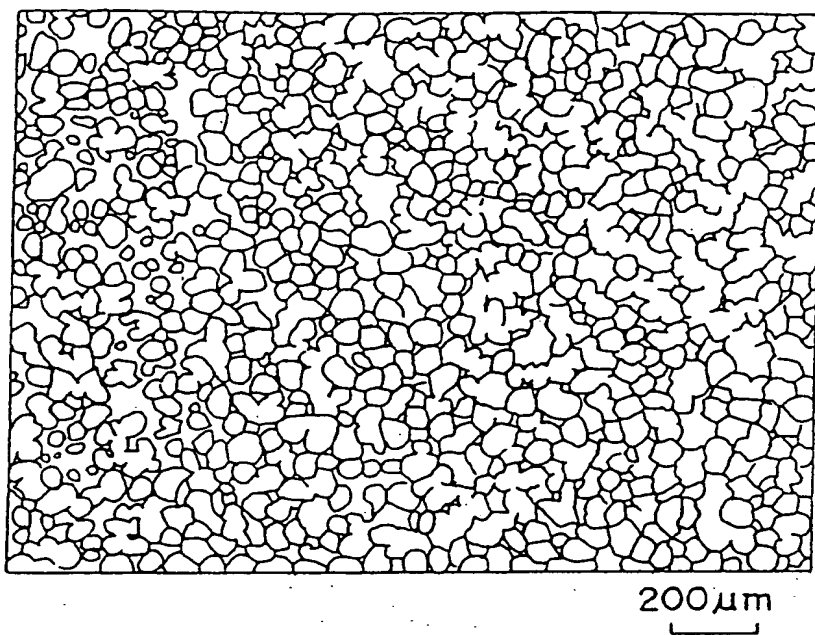


FIG. 73

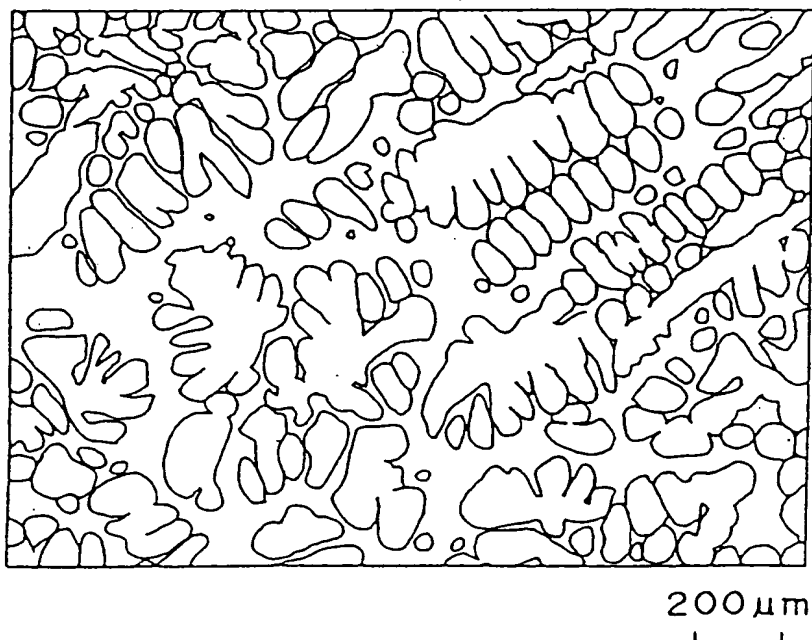
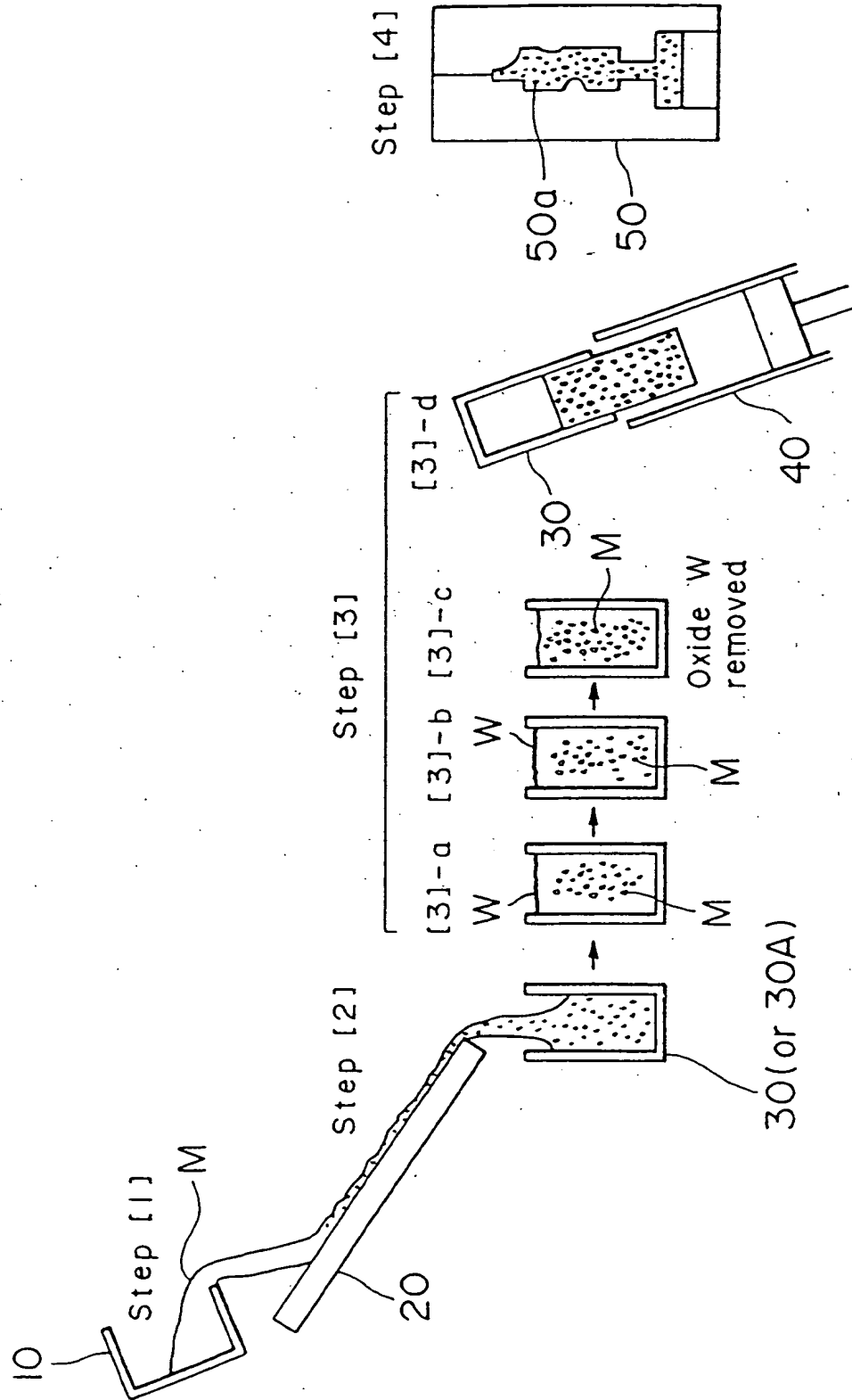


FIG. 74





European Patent  
Office

# EUROPEAN SEARCH REPORT

Application Number  
EP 96 10 8499

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)
E	EP-A-0 719 606 (AHRESTY CORP) 3 July 1996  * the whole document *	1,11,12, 14,16, 19,20	C22C1/00 B22D17/00
A	EP-A-0 392 998 (CROSTI GIOVANNI ;POLVARA MARIA (IT)) 17 October 1990  * the whole document *	1-5,11, 12,14, 16,19,20	
P,A	EP-A-0 701 002 (UBE INDUSTRIES) 13 March 1996  * the whole document *	5-10,28, 29, 31-33,40	
A	PATENT ABSTRACTS OF JAPAN vol. 011, no. 078 (M-570), 10 March 1987 & JP-A-61 235047 (NIPPON KOKAN KK), 20 October 1986, * abstract *	5-10,28, 29, 31-33,40	
A	PATENT ABSTRACTS OF JAPAN vol. 017, no. 574 (M-1498), 19 October 1993 & JP-A-05 169227 (UBE IND LTD), 9 July 1993, * abstract *		TECHNICAL FIELDS SEARCHED (Int.Cl.6)  C22C B22D
A	WO-A-92 13662 (TRANSVALOR SA) 20 August 1992  -----		
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 27 August 1996	Examiner WOUDENBERG, S
<p><b>CATEGORY OF CITED DOCUMENTS</b></p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ----- A : member of the same patent family, corresponding document</p>			

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